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CIVIL ENGINEERING LABORATORY

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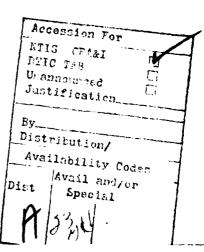
The Navy has initiated a program to improve fleet mooring capability through tests of existing fleet moorings and a range of conventional anchors in use and projected for use. The results of site surveys and of instrumented anchor and mooring tests at San Diego Harbor, Calif., and at Indian Island, Wash., are presented. Emphasis in the tests was on defining the applicability limits of the Navy's primary fleet mooring anchor, the Stockless anchor, through tests of single and tandem anchors. The Navy can use the data immediately for selection and sizing of anchors for sites typical of San Diego sand and Indian Island silty clay seafloors. Other anchors tested included the Navy STATO, BRUCE, Hook, and STEVIN anchors. Test data are presented primarily as plots of anchor penetration, holding capacity, and shank pitch and roll as functions of anchor drag distance. Tandem Stockless anchor arrangements were found that could be easily installed and that resulted in individual anchor efficiencies equal to or exceeding those determined through single-anchor tests. Several anchors were modified to achieve satisfactory performance in the test soils. Guidance for these changes is provided.

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INTRODUCTION

A program has been initiated for improving the Navy's fleet mooring capability through tests of existing fleet moorings and a range of conventional anchors in use and projected for use. These tests by the Civil Engineering Laboratory (CEL) are being performed in seafloors typical of Navy fleet mooring sites in conjunction with Navy Public Works Centers (PWC) where possible. In addition to the gathering of data on mooring and anchor behavior, anchor installation and proofing procedures are being evaluated to determine those most effective within the capabilities of PWC personnel and equipment.

Ultimately, the test data generated can be used: (1) to simplify and refine anchor selection and sizing, (2) to enable stipulation of anchor/mooring installation and proofing procedures, (3) and to improve

the Navy's confidence in its moorings.

This report presents the results of site surveys and of instrumented anchor and mooring tests in the harbor at San Diego, Calif., and at Indian Island, Wash. Test data on Navy Stockless and STATO anchors are presented for immediate use by the Navy for selection and sizing of these anchors for sites typical of San Diego sand and Indian Island silty clay seafloors.

Test data are presented primarily as plots of anchor penetration, holding capacity, shank pitch, and shank roll as functions of anchor drag distance. These data allow complete isolation of anchor behavior from mooring behavior and will ultimately enable the development of an empirical scheme to predict anchor behavior. This task is underway and is scheduled for completion during FY81.

PROGRAM OBJECTIVES

The following are the specific program objectives:

- 1. To determine the capacity of selected existing moorings by proof testing to establish mooring limit.
- 2. To determine more accurately the capacity of the Stockless anchor at typical mooring locations.
- 3. To determine a means for efficiently using Stockless anchors in tandem and thus expand the use of the Navy's current anchor inventory.
- 4. To evaluate the operational practicality of using the Stockless anchor with welded open flukes, since tests have indicated higher capacities for the anchor with this modification.
- 5. To determine the capacities of high efficiency anchors in seafloors typical of Navy sites.

6. To gather site and anchor performance data to enable the development of an empirical procedure to predict the behavior of typical Navy drag embedment anchors.

BACKGROUND

Stockless Anchor

Most of the Navy's existing fleet moorings use the stockless anchor. This anchor was never intended for use as a permanent mooring anchor; its primary purpose was as a ship's bower anchor for temporary mooring. The Stockless anchor was not designed for high efficiency (high holding capacity to weight ratio). It was designed to be easily stowed in a ship's hawse pipe and to be easily recovered after use; deep penetration was not desired. Efficiencies of this anchor type are reported (Ref 1, 2, and 3) as approximately 2 in mud and 4-1/2 in sand after setting. Since the largest Stockless anchor available to the fleet weighed 30,000 pounds, the maximum capacities would be 60,000 pounds in mud after proper setting in sediment deep enough to accommodate expected penetration (20 feet to fluke tips) and 135,000 pounds in sand.

Many of the sites at which the Navy has fleet moorings have a soft mud seafloor to the maximum expected anchor burial depth or soft mud seafloors overlying stiff clay, sand, or coral. This latter condition could cause very poor anchor performance because proper anchor embedment might be prevented by the harder substrata. Embedment into the more competent sediment substrata is unlikely if it is significantly stronger than the surface mud or simply if it is granular, thus requiring a reduced fluke angle for embedment at this interface.

Stockless anchors are currently used in up to class AA moorings. In a mud seafloor a single 30,000-pound Stockless anchor is suitable for mooring class F and marginally suitable for mooring class E. This suitability is contingent upon proper setting and sufficient sediment in addition to the acceptability of a minimum safety factor for mooring class E. Because of equipment and procedural limitations, lack of funds, or lack of personnel training in anchor use, mooring anchors are typically not preset, and the existence of sufficient sediment for proper burial is often marginal or unknown.

The Stockless anchor is in great supply in Navy inventory and replacement funds for new, higher efficiency anchors will come slowly; thus, it is important to make use of the inventory. To do this, however, some operational complexities will necessarily be introduced. Tests (Ref 1) of the Stockless anchor in mud with flukes free-swinging and with flukes welded open show significant increases in efficiency for the latter condition, 4 versus 2, indicating that the anchor flukes did not open completely or at all for the free swinging (usual) condition. Towne (Ref 1) briefly experimented with Stockless anchors in parallel (side-by-side, attached to a single pulling point through a length of chain). Results showed that the anchors tended to come together, and that load equalization was of concern. Once the anchors come together, they will not re-embed, thus losing the safety advantage of this basic anchor type. Use of anchors in tandem (series) is an alternative to enable more effective use of the Stockless anchor. However, unless the anchors are properly rigged, the capacity of two anchors can be less

than that for a single anchor. Laboratory experiments (Ref 4) have been performed to determine an appropriate rigging technique for tandem anchors. The laboratory tests suggest rigging methods for tandem fixed and movable fluked anchors that appear feasible in practice. Both possibilities, welded open flukes and tandem anchors, would introduce additional installation complexity but could expand the use of the existing Stockless anchor inventory.

STATO Anchor

Limitations in the use of the Stockless anchor may still exist even if the approaches suggested previously can be successfully utilized. For some mooring classes other higher efficiency anchors may be required. One such anchor, the STATO anchor, was developed by the Navy to efficiently fulfill a variety of Navy anchoring needs. The STATO is recognized as the forerunner of a new breed of high efficiency anchors. During its development, it was tested exclusively in two types of sediment, San Francisco mud and Port Hueneme sand (Ref 3). Its design and rated capacities (20 to 1 in sand and 13 to 1 in mud at 50 feet of drag) were established for these two seafloors. The behavior of the STATO in other seafloors will be different; the differences for the Naval sites of interest could be slight, but without verification higher factors of safety would have to be employed at "unknown" sites.

High Efficiency Anchors

Many new high efficiency anchors have been developed and are available; however, performance data are limited to advertising claims. Advertised data suggest extremely high anchor efficiencies. If these data can be verified then these new anchors have the potential for significant cost savings to the Navy.

TEST PROGRAM

To resolve uncertainties in mooring capacity, anchor selection, sizing, configuration, and installation procedure, prototype testing at Navy sites with typical seafloor conditions is underway. In addition to the prototype tests, development of a predictive technique which depends on those engineering properties of the soil that govern soil reaction to loading by the embedded anchor and chain will be needed. Engineering properties are not a factor in presently used prediction schemes; capacity is always stated in terms of holding capacity to weight ratios and is usually based on a few tests in idealized soils (a sand or a clay). Relating capacity to engineering properties has the potential of enabling more accurate sizing of different or larger anchors or anchors used in seafloors in which they have not been tested.

Locations

After a lengthy pre-selection process which evaluated such things as available site boring logs, geologic charts, and site support, three sites were selected for detailed site surveys: San Diego Harbor, Calif., Indian Island, Wash.; and Subic Bay, Phillipines. Indications were that

these sites would provide a cross section of seafloor types typical of Navy fleet mooring sites as well as very uniform soil deposits to avoid confusion in data analysis. The surveys verified the suitability of San Diego and Indian Island sites; the Subic Bay survey results were inconclusive. Fortunately, a survey of Apra Harbor, Guam was being performed by Chesapeake Division Naval Facilities Engineering Command. These data were provided to CEL, and they indicated that Guam would be a suitable third test site. Anchor tests at Guam have been completed and results will be published in a subsequent report.

The locations of the anchor tests and cores at San Diego and Indian Island are shown in Figures 1, 2, and 3. For reference, the typical orientation of the test barge (shown to scale) during tests of anchors and moorings at San Diego is shown. The lay of the mooring legs is also shown for San Diego moorings.

Site Survey

The site survey at each test location consisted of underway acoustic subbottom profiling using a 5-kHz sound source and a hydrophone array and recorder, and coring using a 10-foot piston corer and an Alpine vibracorer for cores typically to 20 feet. One 40-foot core was attempted at Indian Island; 28 feet of core were recovered. The acoustic survey was performed to rapidly assess vertical and areal uniformity to aid the site selection process. The profile did not prove effective at the shallow water (10 to 15 feet) fine sand site at San Diego or at Indian Island where gassy sediments caused confused records. Fortunately, the vibracorer provided a rapid and easy alternative means to assess soil properties at probable test locations.

Each core was cut into 5-foot sections and transported to CEL for determination of the engineering properties. Usable soil strength data were not obtained from the cores taken at San Diego and Indian Island due to significant sample disturbance. It is planned to return to both sites with an in situ test device with cone penetrometer and vane shear capability. Twelve vibracores were taken at San Diego and six were taken at Indian Island. Not all these cores were completely analyzed; this can be done at a later date if need arises. A few cores were thoroughly analyzed with spot checks made on other cores to determine similarities. For example, the cores at Indian Island were extremely similar; thus, only one was analyzed in detail from that location.

Briefly, the primary test site (location 1) at San Diego (Figure 1), is a very uniform fine sand both areally and vertically. Figures 4 and 5 illustrate this with grain size curves of cores taken several hundred feet apart. Indications are that the seafloor is very dense, based on frequent extraordinarily high chain resistance during testing. As mentioned, this will be determined at a later date to enable eventual development of a predictive scheme. Additional data for San Diego Harbor are provided in Appendix A. Figure 2 shows a second site (location 2) described as a dense clayey sand. It is a very dense fissured seafloor in which only six tests were performed to evaluate the behavior of two particular anchors in a very hard seafloor.

The Indian Island site shown in Figure 3 consists of a gassy, soft silty clay with shell fragments. Table 1 lists of soil properties for core 3 at Indian Island. The gas in the soil caused soil expansion upon

core recovery, disturbing the samples and making undisturbed shear strength data meaningless.* Typically, the Indian Island mud was almost evenly distributed between silt and clay sized particles. Figures 6 and 7 show the grain size distributions for core 3V. The curves are almost identical with depth to 10 feet; spot checks showed minimal areal variability. Indian Island soil is classified as an organic silty clay of high plasticity. The liquid limit and water content values are relatively high and approximately equal, varying little with depth to 28 feet. Values range from 110 to 160 for water content and 117 to 142 for the liquid limit. The liquidity index (ratio of the difference between natural water content and plastic limit and the plasticity index) for the mud varies between 0.88 and 1.65 which can indicate either a comparatively soft or firm but sensitive soil. For liquidity indices in the above range, soil sensitivities could vary from 5 to 25. Anchor and chain performance suggests that the soil is quite sensitive; in situ strength measurements will be made for verification.

Test Anchors

A variety of test anchors were gathered from the Navy and private industry and are listed below:

Anchor	Nominal Weight, lb (kg)
Stockless	5,000
Stockless	9,000
STATO	1,000
STATO	3,000
STATO	6,000
BRUCE (twin shank)	748 (340)
BRUCE	1,320 (600)
BRUCE	2,200 (1,000)
STEVMUD	1,100 (500)
STEVMUD	2,200 (1,000)
STEVDIG	2,200 (1,000)
STEVFIX (sand)	1,408 (640)
STEVFIX (mud)	2,068 (940)
Hook	1,232 (560)

^{*}Immediately prior to printing this document, shear strength data for Indian Island mud became available. The seafloor is normally consolidated and shear strength measures almost linearly from zero at the surface to 1-1/2 psi at 21 feet. See Figure A-11 in Appendix A for the data.

These anchors are all shown on the deck of the Army National Guard barge (Figure 8) used at Indian Island. Dimensions of all anchors tested are provided in Appendix B.

The Stockless anchor is depicted in Figures 9, 10, and 11. It can be modified by the addition of stabilizers to slightly increase capacity and improve roll stability. The Stockless anchor typically has a 45-to 48-degree fluke angle which is appropriate for mud seafloors. In sand, the angle should be reduced to 32 to 35 degrees for maximum performance. The Stockless anchor was also tested with welded-open flukes to evaluate speculated performance improvement and operational difficulties and advantages. The welded-open Stockless anchor was also used in tests of anchors in tandem (also called piggy-back).

Three sizes of the STATO anchor were tested to evaluate individual anchor behavior as well as to provide data on size effects. The STATO is shown schematically in its sand (34 degree fluke angle) and mud (50 degree fluke angle) configurations (Figure 12). Figure 13 shows the 6K STATO ready for testing.

Two types of BRUCE anchors were made available to the Navy. Figure 14 depicts the standard cast BRUCE anchor, which is designed to be lowered or dropped to the seafloor without concern for its attitude upon contact. Upon dragging (setting), the anchor rotates to its fluke-down orientation. A new welded version of the BRUCE anchor (Figure 15) was provided for tests at Indian Island. It was not fabricated in time for San Diego sand tests. The welded BRUCE anchor looks like the cast anchor but employs a twin plate shank and a hollow fluke section to allow increased fluke area. In fact, the 340-kg welded anchor had about the same fluke area as the 1,000-kg cast anchor. BRUCE cable depressors (either singly or multiple) are designed to attach to the shank (see Figure 16) between the anchor and chain to "depress" the chain, cause increased anchor penetration, and produce higher anchor holding capacity. Nominally, a depressor adds 20% to total system weight.

Four other types of high efficiency anchor were provided for testing, the STEVDIG, STEVMUD, STEVFIX, and Hook. The STEVDIG (Figure 17) is typically used for competent seafloors. Note the "claws" at the tips of the anchor flukes; they were placed to aid in digging into the dense sand and overconsolidated clay-type seafloors of the North Sea. The STEVMUD (Figure 18) is a single-purpose anchor developed for anchoring in mud. The STEVFIX, however, was designed to be used in sand and mud seafloors. Figure 19 shows the STEVFIX without bolt-on plate and stabilizer extensions for mud application. Fluke angle is adjusted for sand (50 degrees) and mud (32 degrees) by the removal (burnout) or addition (welded) of a small insert in the anchor crown.

A movable fluke, pick-type anchor, called the Hook anchor (Figures 20 and 21), was also tested. This anchor is designed primarily for mud, but is usable in sand by restricting the fluke angle to 32 degrees. The Hook is shown with and without auxiliary flukes on the shank and was tested in both configurations.

TEST PROCEDURES AND EQUIPMENT

The basic test setup showing component layout and instrumentation locations is shown schematically in Figure 22. The layout for the tandem Stockless anchor tests is identical except that the instrument package is located on the outboard anchor. The inboard anchor is uninstrumented.

For this test effort, an instrumentation system was devised to isolate anchor behavior from test mooring behavior. It was felt that isolation of anchor behavior was critical to the eventual development of a scheme to predict anchor size effects on capacity and to understand and predict the behavior of conventional anchors as a function of seafloor engineering properties.

Measurement System

Data gathered for all single and tandem anchor tests included load at the test vessel, load at the anchor, anchor depth, anchor longitudinal rotation (shank pitch), transverse rotation (shank roll), mooring line angle at the test platform, and barge displacement. By knowing barge displacement and accounting for test mooring line catenary changes, anchor drag distance is readily calculated.

Spar Marker. Initially, barge position was to be recorded primarily by means of a portable range-range navigation system with a spar buoy reference system used as a backup. The spar marker system proved to be much simpler, more accurate, and more reliable than the navigation system; thus, it was used exclusively during the test effort. The deck of the YC test platform was marked off in 2-foot increments for 100 feet. At the beginning of each test (identified by test anchor movement) a spar buoy (Figure 23) was placed on the bottom at the corner of the barge. Barge motion was recorded in 2-foot increments directly on the oscillograph and digitape-papertape records. At San Diego, a 20- to 35-foot length of gasoline-filled plastic pipe (depended upon test site) was weighted at its base and used as the spar marker. At Indian Island, water depth approached 100 feet; thus, the spar marker was modified to be less sensitive to current. A 30-foot segment of tube was attached to a subsurface taut mooring comprised of a 1-1/2-ft diam float, 85 feet of 1/8-inch wire rope, and an anchor clump.

Instrumentation System. Figure 22 is to be referred to for the overall measurement system layout. The underwater portion of the system is shown in Figure 24 for San Diego and Indian Island. The instrument pack was further streamlined for Indian Island. The load cell is the slender object attached directly between the anchor shank and chain; it measures load at the anchor only. Included in the instrument pack shown strapped to the anchor shank is a pressure transducer to measure water depth from anchor to surface, two inclinometers to measure shank angle and shank/anchor rotation, all signal conditioning equipment, and amplifiers for the load cell. The load cell was connected to the package

by an 8-foot electrical cable. A hose connected to the pressure transducer at the package was connected to a buoy (shown in Figure 24) to ensure that the bitter end remained out of the seafloor. The underwater system was connected to the surface barge by a 1,300-ft-long, six-conductor, underwater electrical cable.

The surface system consists of a deck load cell to measure load between pulling barge and test anchor, a cable inclinometer to measure cable angle at the barge, signal conditioning equipment, biasing and voltage calibrator unit, and recording equipment. Two methods were used to record the data: (1) an analog-to-digital recorder recorded data every 10 seconds and (2) an analog oscillograph was used to record continuously during test.

All transducers (load cells, inclinometers, and pressure transducers) were calibrated before each series of tests and rechecked afterward and found to be within specification of calibrations.

All load cells used for measurements on anchor tests were calibrated at the CEL on a Baldwin load machine with an accuracy of 0.303% of full scale.

Repeatability of the load cells was:

No. 1 underwater cell - 0.4%

No. 2 underwater cell - 0.4%

No. 1 deck load cell - 0.35%

No. 2 deck load cell - 0.35%

The underwater load cells were checked for temperature drift and found to change 0.019/° or 38 lb/deg; this is a positive temperature coefficient.

Pressure cells used for depth measurement were calibrated with a deadweight tester and have a built-in signal conditioner and amplifier. Repeatability of pressure transducers was:

No. 1 pressure transducer - 0.005%

No. 2 pressure transducer - 0.0045%

The pressure transducers were checked for temperature drift and found to change 0.139 ft/°; this is a negative temperature coefficient. This change occurred within 60 seconds; therefore, relative changes in depth were correct during testing. Actual recorded depth could be as much as 1-1/2 feet too high, considering the temperature difference between deck and water. Inclinometers were calibrated and found to have an accuracy of 0.2-degree resolution.

Single Anchor Test

The test procedure was the same at San Diego and Indian Island; however, equipment did differ somewhat. A YC barge about 120 feet long served as the anchor pulling and data recovery platform. Photographs of the actual deck layout are given by Figures 25 and 26. A 100-ton-capacity, hydraulic cable puller was provided by the Supervisor of Salvage for the test effort. The cable puller basically consists of a fixed and a movable 2-inch cable gripper controlled through a remote console. The

grippers are alternately actuated and deactuated to haul-in or pay-out the 2-inch hauling line. About 4 feet of movement occurs at each cycle at rates from 0 to 17 ft/min. Each anchor was pulled at about 2 ft/min primarily to agree with previous controlled anchor tests. The cable puller operates as a load-controlled, rather than a strain-controlled, system; it is felt that, even though loading is briefly interrupted during a puller reset cycle, the loading is realistic. The cable puller pulled the anchor and its fixed-length mooring line toward a restraint mooring comprised of one preset 9,000-pound STATO anchor, 2-1/2-inch chain, and a peg-top buoy.

The YC barge was not heavily loaded during mooring or anchor testing; load was transferred from the restraint mooring through the cable puller (which simply rests on the deck) to the test anchor and mooring by a heavy duty padeye fixed to the YC. The padeye-deck attachment had to withstand only the environmental forces on the barge. Barge orientation was maintained during testing because both test and restraint lines passed through open chocks welded at opposite ends of the barge.

A crane barge was used to install and recover all test anchors at each site. The orientation of test barge and crane barge for Indian Island tests is shown in Figure 27. The crane barge was attached to the test barge by a 5/8-inch wire from an 8-ton salvage winch. At San Diego, wind proved to be a formidable problem in controlling crane barge location. Two pusher boats and an LCM-8 were barely able to control crane barge position. During the latter phase of San Diego tests, a stern anchor was placed to help control position in addition to helping restretch the test mooring after completion of a test series. The Figure 27 setup was a further refinement of the test procedure. This setup allowed the crane barge to move back and forth between its stern anchor and the test barge with help from its pusher boats.

For each test location, an attempt was made to minimize the number of times the restraint and test moorings had to be readied and deployed. The barge was layed out as shown in Figure 28. The 400 feet of 2-inch hauling wire was attached to the preinstalled restraint mooring buoy, and the wire was stretched out. The test mooring wire was subsequently stretched out using the crane barge. Two to three shots of chain were then attached to the test line and stretched. This configuration was typical for the beginning of each test day. At this point the LCM-8 would pull the 5/8-inch wire to the test barge and then return to the barge crane with the floated electrical line which would then be connected to the test anchor attached to the test mooring chain.

At San Diego the test anchor was lifted and lowered directly to the seafloor through the crown wire. The tug was released and the anchor pulled. After at least 50 feet of anchor drag the anchor was lifted, hosed off and relowered for another test. Three to four tests could be performed sequentially in a single line before the 2-inch haul line had to be pulled back through the cable puller while the test mooring was restretched. The test mooring was then layed 50 to 75 feet counterclockwise for the next series.

At Indian Island, crane lift height was not sufficient to lower the anchor directly to the seafloor (about 100-foot depth); therefore, a large sheave was connected to the no. 1 hook. A 160-foot crownwire shackled to the deck at one end and attached to the anchor at the other was then placed in the sheave. With only a 50-foot crane lift, the

anchor was easily lowered to 100 feet through the two-part line. This approach was simple and should be useful to the PWC's where controlled anchor lowering in water depths between 80 and 180 feet is required.

Tandem Anchor Tests

Three tandem anchor arrangements with the Navy Stockless anchor were evaluated. The first method, referred to as the shank-to-shackle technique, and described by Figure 29, proved effective during a brief model study performed in Holland (Ref 4). In the shank-to-shackle method, both Stockless anchors were stabilized and had welded-open flukes because the model tests (Ref 4) showed superior performance with these modifications. A length of chain somewhat in excess of water depth was placed between outboard anchor shank and a padeye welded to the top of the inboard anchor's shank near its shackle connection. It was believed that this aft connection would allow the inboard anchor to function properly. During deployment, the chain would be lightly lashed over the crown of the inboard anchor to prevent fouling.

Figure 29 also shows the second tandem arrangement evaluated (crown-to-shackle technique). It was similar except the joining chain was connected to a padeye attached to the top of the Stockless anchor crown. Again, the flukes were welded open; otherwise they may have closed as soon as any load was applied to the crown by the outboard anchor chain. Figure 30 illustrates the third tandem test arrangement, the ground-ring-to-shackle technique. In this approach the inboard anchor is placed first and then the outboard anchor is lowered and the chain stretched. Welding the flukes open for all three tandem techniques also ensured that both anchors would penetrate immediately, thus insuring a taut mooring.

In addition to evaluating anchor system capacity, installation difficulties were also assessed. The best anchor system could be one that can be installed reliably with PWC assets even though it did not prove to be the highest capacity arrangement. Figure 31 describes the procedure used at Indian Island to install the shank-to-shackle and crown-to-shackle tandem anchor systems. This procedure is similar to that which could be used with fleet moorings, except the mooring would be laid off the bow of a Navy crane barge and chain length between anchors would depend on water depth.

Mooring tests were performed only at San Diego. During these tests, barge displacement, deck load, and line angle were measured. The direction of pull was established to ensure that load was being applied to a single mooring leg. Mooring leg layouts were defined by Reference 5. Load was applied to the test mooring until the rate of barge displacement increased and load dropped off. The test was then abruptly stopped to avoid excessive barge moor displacement and a requirement for leg repositioning.

Two test setups were used (see Figure 32). Pulling one mooring against another was a timesaver because it eliminated the need to install a restraint mooring; however, this could only be done if the mooring leg layouts were suitable. For a dual test setup, the spar marker reference buoy was placed midbarge. By monitoring the direction and displacement rate of the barge relative to the spar, it was possible to determine which of the test moorings yielded.

RESULTS AND DISCUSSION

Anchor Test Results - General

Fifty single and tandem anchor tests and three mooring proof tests were performed at San Diego; twenty-five single and tandem anchor tests were completed at Indian Island. These tests are summarized in Tables 2 through 4. Results of all Navy anchor (Stockless and STATO) tests are described and significant results provided. Each of these anchor tests is further described by a data plot and a data tabulation (see Appendix C). The results of all commercial anchor tests are the subject of a later report.

One data summary is described for guidance. Seven parameters are plotted as functions of true anchor drag distance in Figure 33. In the bottom block, horizontal force at the pulling barge, anchor tension, and chain weight on bottom are plotted versus drag distance. The difference between tension measurements is attributed solely to chain drag both on and in the seafloor. As shown by Figure 33, the contribution of the chain to total mooring load is substantial; this was typical for all the tests. At anchor tension equal to zero, the deck force reflects only chain drag. The 20,000 pounds of chain on bottom caused almost 30,000 pounds of drag resistance in the silt at Indian Island. At 58 feet of drag, roughly 10,000 pounds of chain (about 250 feet) in contact with the seafloor causes about 50,000 pounds of drag resistance. The 3,000pound (nominal) STATO (actual weight 3,500 pounds) provided about 37,000 pounds of resistance at 58 feet of drag. A safe capacity of this anchor in Indian Island silt is 37,000 pounds. With information on the amount of chain in contact with the seafloor, capacities in excess of the basic anchor capacity could be assumed.

In the center block of Figure 33, anchor shank pitch angle and anchor shank roll angle are plotted versus drag distance. A positive pitch angle indicates shank tip down. As shown, the shank assumes a tip up (negative angle) orientation of about 10 degrees as the anchor approaches peak capacity. During drag, the anchor appeared relatively stable, remaining within 6 to 10 degrees of horizontal.

The top block of Figure 33 presents anchor crown and shank tip penetration as functions of drag distance. In the future, only one depth will be plotted for clarity. Penetration leveled out at about 15 feet to the crown, which translates to 19 feet to the tip of the fluke. It appears that the anchor is still penetrating but at a very shallow angle.

Table 5 is an example of the tabulated data for each anchor test. The table lists the data plotted in Figure 33 in addition to various other pieces of data that may be of use in the eventual analysis of these data. Item number 13 is anchor fluke tip depth; it is assumed that the flukes are completely open. For fixed fluke anchors this is valid but for movable fluke anchors the number must be used with care. In sand it is usually obvious when the fluke is open; there is a sudden increase in shank angle associated with a gradual increase in anchor tension. In mud it is not as obvious but is assumed to occur if anchor penetration is initiated and continues.

Tests of the many anchors in various configurations produced results which are grea'ly, but not totally, dependent on the testing media, San Diego fine sand and Indian Island mud (silty clay). Six tests were also run in overconsolidated silt at San Diego. Overall results would have been somewhat different (degree of difference unknown at this time) with different mooring line, type, or size. The differences would most likely occur with anchor and deck tension readings and anchor penetrations. Pitch and roll of the anchor would probably not be as sensitive to changes. In selecting chain size, an attempt was made to size it according to previous performance data or to advertised data. Often, the anchors would hold less than expected, thus chain size could have been less. Since the behavior of anchor and chain were isolated in these tests, it is felt that mooring line effects on anchor behavior will eventually be understood and quantified in a usable prediction scheme. Until then, care should be exercised when extrapolating these data to other sites, anchor sizes, and mooring lines.

Stockless Anchor (Single) .

This anchor was tested in its normal use condition (unstabilized and with movable flukes free to open to 45 to 48 degrees relative to the centerline of the shank) at both San Diego and at Indian Island. These tests were run for confirmation of previous results (Ref 6) and to illustrate problems with using the Stockless anchor in this configuration for fleet moorings; results were similar. Behavior in sand was erratic for the 5K size (efficiencies of 3 to 5) while behavior in mud was consistent but poor. In comparison, the performance of the stabilized Stockless anchor with flukes welded in the open position at 35 degrees for sand and 48 degrees for mud was quite good.

In sand, anchor behavior was consistent with an average anchor efficiency of 5 to 6 for the 9K anchor and 10 for the 5K anchor. Most significantly, these efficiencies were achieved with minimal drag distance which would result in very taut moorings. Tests were not run with a stabilized anchor with 35-degree movable flukes in sand, but previous data (Ref 7) show that the flukes will eventually dig in sands of low to medium density; the improvement due to the reduced fluke angle could be as much as a factor of two. In dense sand and stiff clay seafloors the probability of the Stockless anchor flukes digging in is very low. Welding open the anchor flukes should greatly increase the probability of suitable anchor behavior in these more competent seafloors. Care should be exercised in comparing the mentioned efficiencies with previously reported data because the above values are for the anchor alone. Previous researchers attempted to determine true anchor capacity by separating the chain effect determined through chain pull tests. As can be seen from the results in Appendix A, the chain effect often increases as the anchor is dragged, and the shank forces chain into the seafloor. This effect will be different for different seafloors. The chain effect is real and is part of the total anchor resistance, but, particularly in sand and until it is better understood, the anchor tension alone provides a conservative estimate of expected performance.

In mud at Indian Island, each of the three configurations (i.e., standard, stabilized with movable flukes, and stabilized with fixed flukes) of the 9K Stockless anchor behaved sufficiently different to

clearly show the advantage of fixing the flukes in the open position in mud. Anchor penetrations at comparable drag distances were greater, anchor tensions were greater, and most importantly, mooring tensions were significantly greater. At 41 feet of drag, deck tensions for the above three configurations were 48,000, 50,000, and 67,000 pounds, respectively. Also, the first anchor appeared to have reached peak depth, the second increased slightly to 53,000 before peaking, and, based upon relative shank angles between two and three, option three would probably penetrate further. To put these differences into proper perspective, the effect of the chain laying on (not in) the seafloor is subtracted to show the "true" difference in capacities for Indian Island mud. The values then become 26,000, 30,000, and 50,000 pounds which translate, according to previous methods of figuring anchor efficiency, to 2.5, 2.6, and 4.4, respectively, for the nominal 9K anchor (true weights were used in determining efficiency). A possible reason for these differences is that the anchor flukes stabilized at a partially open position. Previously reported differences (Ref 1) for San Francisco Bay mud show the same relative differences - 2 versus 3.7 to 4. The lower overall values are explained by the reported lower chain drag in San Francisco Bay mud.

Stockless Anchor (Tandem)

In sand, three methods of rigging tandem anchors were tested (see previous section for descriptions). In terms of performance each was satisfactory; there appears to be a slight performance advantage for the shank-to-shackle rigging arrangement. The outboard anchor carried the instrument pack and outboard anchor performance paralleled that of the single anchor. The performance of the inboard anchor is inferred from the difference between deck tension and anchor tension. Based on the differences, the inboard anchor was functioning at least equally to the outboard anchor. Of the three techniques, the shank-to-shackle and crown-to-shackle techniques were equal in terms of installation ease. The ground-ring-to-shackle approach was also effective but somewhat more difficult to install in shallow water at San Diego. In deeper water at Indian Island, installation would have been significantly more difficult, thus it was not tried there. Model tests (Ref 4) in sand of both shank and crown-to-shackle techniques showed superior performance for the shank-to-shackle technique; attachment to the crown caused rotation of the inboard anchor. Prototype tests in sand and mud with the Stockless anchor with welded-open flukes, showed no indication of inboard anchor instability, inferred by overall mooring capacity. Attachment of chain to the crown rather than the shank does simplify installation in deeper water and does not seem to degrade overall performance.

The techniques found suitable for the Stockless anchor in fine sand and soft silty clay will probably be applicable to the vast range of intermediate soil types.

Use of these rigging techniques with higher efficiency anchors has not been proven at prototype size. Higher efficiency anchors need to penetrate deeply in mud and their light weight in relation to their capacity makes them more sensitive to external forces caused by tandem chain attachments. Tandem anchor chain attachment to the inboard anchor

shackle or chain would seem to limit rotational influences on the inboard anchor and, as long as deployment technique is not compromised, may be the safest alternative for higher efficiency anchors at this time.

STATO Anchor

Three sizes of STATO anchor (1K, 3K, and 6K) were tested in sand at San Diego and mud at Indian Island. The 3K STATO was also test-pulled in a dense clayey sand seafloor at San Diego.

Initially, three sizes were to be tested to get some idea of scale effects and to provide a good basis for comparison with other high efficiency anchors. However, initial results in sand were unexpectedly poor, and sufficient scale data were not obtained. Slight modifications to the STATO were required to bring performance back to its expected level. The chronological test sequence which leads to what appears to be necessary changes to expand STATO utility to a broader range of soil types and strengths is described in the following paragraph.

The 1K STATO was first tested in sand and at 5 to 6 feet of drag the anchor rotated out after a peak load of only about 6,000 pounds, far less than expected. This rapid instability would normally indicate that the anchor was improperly stabilized. Stabilizer width agreed with that listed by the drawings (16 inches); however, it did not agree with that projected from a plot of anchor width versus anchor weight for all other STATO anchors. The 1K STATO had not been fabricated previously, thus this problem had gone undetected. "Normal" stabilizer length should have been about 26 inches. While new 1K anchor stabilizers were being fabricated, the 3K STATO with normal stabilizers was tested. It also proved unstable after achieving an anchor load of about 30,000 pounds. The effect of the mooring chain on anchor stability was insignificant because in the two tests performed, the anchor rotated in opposite directions. The 1K STATO with normal 26-inch stabilizers was tested, and it reached about 10,000 pounds before becoming unstable. Its behavior paralleled that of the 3K STATO with its normal stabilizers. Extended stabilizers were fabricated for the 3K STATO with the intent of shortening them sequentially to determine their minimum allowable length. With 18-inch stabilizer extensions (Figure 34) (143-inch total anchor width), the anchor was pulled again. It built up load initially to about 40,000 pounds and then rotated out. Through 140 feet of drag it did not improve and continued to try to embed as evidenced by the fluctuating shank angle. Anchor fluke angle was checked to verify that it was 35 degrees as intended; it was 37 degrees. A 2-degree reduction in fluke angle was not considered adequate to improve performance. Therefore, it was reduced from about 37 to 31-1/2 degrees (by the addition of a 1/2-inch plate between shank and wedge insert, Figure 35), and the anchor was retested. A 30 to 32-degree fluke angle is currently used by the majority of anchor manufacturers for competent seafloors. The anchor built up load gradually until reaching 65,000 pounds. The load appeared to stabilize. On later examination of the data it was noticed that the anchor was beginning to rotate. To determine whether both the fluke angle reduction and stabilizer extensions were necessary, the normal stabilizers were replaced on the anchor and the anchor re-tested. The anchor rotated at about 12 feet of drag. Apparently, both modifications

were necessary. Since it appeared that the 18-inch extension was a good first guess based upon the slight tendency for rotation, smaller extensions were not tried.

The 6K STATO was then tested using its normal stabilizers. Specified fluke angle was 35 degrees yet measured angle was 32 degrees. This tolerance error was fortunately in the right direction for the San Diego sand. Three tests were performed, and the anchor held 105,000 pounds, 72,000 pounds, and about 60,000 pounds. Anchor rotation was again a problem. When fitted with normal stabilizers, all three sizes of STATO anchor behaved in a similar fashion. It appears that the lengths of stabilizers determined as adequate in Port Hueneme beach sand are not adequate for the denser, more uniform, finer grained sand of San Diego Harbor. As of this writing, accurate soil density measurements in San Diego sand were not available; they will be taken shortly. Based on the behavior of all anchors tested and the large chain resistances recorded, it appears that San Diego sand is of high relative density; the need for STATO fluke angle reduction further substantiates this.

Results of tests in mud at Indian Island were in reasonable agreement with previous results reported for San Francisco Bay mud (Ref 3).

Recorded efficiencies, for anchor alone, of the 1K and 3K STATO anchors at 50 feet of drag were 14 and 11, respectively; while total efficiencies, including the effect of buried chain were 20 and 17 respectively.

Anchor tension for the 6K STATO was not recorded, however; total efficiency near 50 feet of drag was 14. The 1K and 3K anchors appeared to be nearing their peak load while the 6K anchor load was still increasing; however, the 6K anchor was steadily rotating. At 41 feet of drag the measured maximum rotation of about 45 degrees was recorded and the test stopped to avoid electrical cable failure. Longer stabilizers would probably have limited rotation. The extended stabilizers on the 3K anchor did not seem to noticeably inhibit anchor penetration or degrade performance; stability was apparently helped.

The three tests of the 3K STATO with extended stabilizers in a dense clayey sand were in a designated anchorage area in San Diego Harbor. These data were probably the most interesting. In each test the anchor dug in and increased to peak load rapidly and then pulled out. When recovered, soil was packed between the shank and flukes which would prevent further embedment.

Based on tests performed to date on the STATO it is possible to make some general recommendations for modifications to expand utility of the STATO to a broader range of soil characteristics. For specific applications, perhaps these changes should be made only if performance is less than expected or if data indicate a very competent seafloor. For general utility, the following changes are recommended prior to further usage.

- 1. For use in sand, measure the fluke angle with the wedge insert in place; if greater than 32 degrees, insert a plate spacer or fabricate a new wedge to achieve the needed fluke angle.
- 2. For sand and mud, extend the stabilizers according to the recommendations of Figure 36. Existing and projected curves of anchor width versus anchor weight are provided. Obviously, extrapolation on the basis of a single data point can be considered highly questionable

but high efficiency anchors are typically scaled as a direct function of anchor weight. Anchor dimensions are normally scaled according to (anchor weight) ; however, as can be seen from Figure 36, STATO scaling differs. A line proportional to wt , straight line on a log-log plot, is drawn through the single data point available (3K STATO with 18-inch stabilizer extensions). The reason for this deviation from normal geometric scaling was structural limitations due to required use of mild steel (Ref 8). Using geometric scaling with the single data point, the 200-pound anchor seems suitably stabilized and the 15,000-pound STATO seems reasonably close. However, until additional data are available, the upper curve which parallels the actual data and amounts to about a 35% increase in anchor width should be used to provide a conservative estimate of required anchor width from which stabilizer length can be determined.

3. Use of mud palm extensions in sand does not seem to degrade performance. Reference 3 supports this contention; therefore, unless the STATO will be used exclusively for competent seafloors, the mud palm extensions should be included as a standard part of the anchor.

Stockless Anchor Moorings

All moorings tested at San Diego were class B riser-type moorings with a design load of 125,000 pounds. The principal soil type at each mooring location was fine sand. Standard, unstabilized, 20,000-pound Stockless anchors with 45- to 48-degree fluke angles were typical of all the tested moorings. Each anchor was jetted in until flukes were fully open in the down position. Based upon the data gathered at San Diego, it was determined that the anchors in their standard condition probably would not have embedded during normal dragging. Each mooring was pulled in only one direction, and care was taken not to displace the mooring; thus, load was increased to the onset of slippage and loading was stopped immediately. Moorings 17, 18, and 51 held 118,000, 115,000, and 99,000 pounds maximum, respectively. At these loads - in fact at far less than these loads - all chain was off the seafloor. These loads reflect true anchor capacity for the above described conditions. Continued dragging of the anchors, as could occur during storm activity, would probably have caused them to come out of the seafloor, with low probability of re-embedment. A fleet mooring anchor should continue to sustain near peak load with drag to minimize catastrophic damage. The reduction in fluke angle to 35 degrees and the addition of stabilizers will produce this type of desired behavior. If anchors are to be jetted into sand or stiff clay seafloors then these modifications should be made. Also, by welding the flukes open, the principal advantage of jetting (achievement of a taut mooring) can be realized without the need for diving support.

SUMMARY AND CONCLUSION

This report provides the results of anchor and mooring tests in fine sand and dense clayey sand at San Diego and in mud at Indian Island. Tests at a third site with a clay seafloor are planned for early 1980.

Anchors typical of fleet moorings, Stockless and STATO, as well as a variety of new high efficiency anchors potentially useful with fleet moorings, were tested under controlled conditions to: (1) provide immediate use data for the Navy and (2) provide the basis for the eventual development of a scheme to predict the behavior of anchors as a function of seafloor engineering properties. A great deal of data was gathered, and the implications of these data are not fully understood at this time. Care should be exercised in using these data to specify the performance of larger sizes of the tested anchors in similar or different soils than those of the test sites. The tests clearly provided surprises in anchor behavior and illustrated the great dependence of anchor behavior on soil characteristics. An effort is underway toward a more complete understanding of the data and toward the development of an anchor behavior predictive scheme. Results will be reported at a later date. In the meantime, some tentative conclusions can be drawn and guidance given concerning the use of the various anchors tested.

- 1. In sand, the stabilized Stockless anchor with welded-open flukes to 35 degrees was often 2 to 4 times more efficient than the standard Stockless anchor. It also held its load more uniformally with drag and developed its peak capacity within a few feet of drag.
- 2. Tandem anchor arrangements using Stockless anchors with welded-open flukes were found that could be reasonably installed with Navy Public Works assets and that appeared to develop individual anchor efficiencies at least equal to those achieved when pulled singly in sand and mud.
- 3. In mud, the efficiency of the stabilized Stockless anchor with welded-open flukes (fully opened) was approximately twice that of the stabilized or unstabilized Stockless anchor with freely moving flukes.
- 4. The standard STATO anchor performed poorly in San Diego sand; however, an increase of about 35% in anchor width (stabilizer extension) and a reduction in fluke angle to about 32 degrees for the 3,000-pound STATO corrected penetration and stability problems and increased anchor efficiency from less than 10 to greater than 20.
- 5. In mud, STATO performance was in relative agreement with previously reported data; however, some rotational instability was noticed, particularly in the 6K STATO, suggesting the need for an increase in stabilizer length.
- 6. Previous STATO tests were concentrated in Port Hueneme sand and San Francisco Bay mud. The STATO was designed on the basis of tests in these seafloors. The recent tests were performed in seafloors which expanded performance data to a more dense sand and to a softer mud; these tests suggest anchor modifications. To expand the utility of the STATO to a broader range of soil conditions, stabilizers should be extended. When used in sand only, the standard fluke angle should be 32 degrees rather than 35 degrees.

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Table 1. Soil Property Data for Vibracore 3 - Indian Island

Original vane shear strength data and density data not presented. Soil gases caused

significant sample disturbance. Shells and shell fragments were found throughout the cores.

Core color was dark olive gray. Soil classification is silty clay. 5 m 4

Increment (in.)	Water Content,	Remolded Vane Shear Strength,	Liquid Limit, %	Plastic Limit,	Plasticity Index	Specific Gravity	Liquidity Index
0-3	148.30	0.241	142.13	04.49	7.77	2.543	1.09
24-27	146.74	0.198					
36-39	150.49	0.313					
48-51	152.67	0.217	124.64	65.45	59.2	2.521	1.47
60-63							
72-75	143.97	0.313	138.64	71.59	67.1	2.511	1.08
84-87	153.16	0.318					
66-96	161.23	9t .0	125.84	70.34	55.5	2.515	1.65
108-111	158.05	0.174					
116-119	155.16	0.184	140.25	70.40	6.69	2.498	1.2
18 ft 28 ft	134.02 110.46		117.00	65.86	51.1		0.88

Table 2. Summary of Test Data for San Diego Harbor Anchor Tests

	Kemarks		Anchor performance was erratic;			Chain connector parted; peak load not recorded.	Anchor performance was very uniform; Load built no ranidly and remained	stable during pull.	Anchor flipped over at about 12 ft of drag at an efficiency of 6.							
	Depth,	,	12	=	12	16	12	15	. 19	12	12	12				
cription	Anchor Specifics	Location 1 - San Diego Harbor - Uniform Fine Sand	Without stabilizers	Without stabilizers	Without stabilizers	With stabilizers	With stabilizers	With stabilizers	With 16 in. stabilizers	With auxiliary flukes	With auxiliary flukes	With auxiliary flukes				
Anchor Description	Fixed/ Movable Fluke	an Diego	. E	£	Ε	بك	μ,	LL,	E	X.	Æ	E				
V	Fluke Angle, deg	1 - S	84	87	84	35	35	35	35	32	32	32				
	Actual Weight, 1b (kg)	Locat	5,350	5,350	5,350	5,950	5,950	5,950	1,070	1,230	1,230	1,230				
i	Nominal Weight, 1b (kg)		5,000	2,000	2,000	2,000	2,000	2,000	1,000	(260)	(260)	(260)				
7.5000	Date (Julian)						3/29/79	3/29/79 (88)	3/29/79 (88)	3/30/79 (89)	3/30/79	4/2/79 (92)	4/2/79 (92)	4/3/79	4/3/79	4/3/79
	Anchor		Stockless	Stockless	Stockless	Stockless	Stockless	Stockless	STATO	Hook	Hook	Hook				
	No. Series		4	4	4	۷	ر. د	5	•	7	۲					
F	No.		-	7	٣		7	ю	_	_	~	3				

Table 2, Continued

	Remarks											continued
3	Depth,	inued)	15-1/2	15-1/2	13	14-1/2	14-1/2	14-1/2	15-1/2	15	15	
scription	Anchor Specifics	Location 1 - San Diego Harbor - Uniform Fine Sand (continued)	-			With I cable depressor	(170 AK) diter 1040 tell	With 2 cable depressors (240 kg) after load cell		1	1	
Anchor Description	Fixed/ Movable Fluke	-go Harbor		íe.	ia,	i.	.	í	£	Σ	æ	
	Fluke Angle, deg	- San Di	,	,	,	,	,	ı	32	32	32	
	Actual Weight, 1b (kg)	ocation 1	1,320	1,320	1,320 (600)	1,320	1,320 (600)	1,320 (600)		2,550	2,550 (1,160)	
	Nominal Weight, 1b (kg)	7	(009)	(009)	(009)	(009)	(009)	(009)	(1,000)	(1,000)	(1,000)	
1			6/1/79	4/3/79	(76) 4/4/19 (96)	61/4/4	(76)	6/4/4	61/4/4	4/4/79	(74) 4/5/79 (95)	
	Anchor		BRUCE	BRUCE	BRUCE	BRUCE	BRUCE	BRUCE	STEVDIG	STEVDIG	STEVDIG	
	Series		92	2	01	=	2	12	15	51	25	
	Š	L	-	7	m —	~	7		_	7	Е.	

Table 2. Continued

	Remarks		2			Anchor flipped over after reaching an		4 Anchor held stablely at an efficiency of about 5.	3		2
3	Depth, ft	inued)	14-1/2	7.	7	14-1/4	14-1/4	14-3/4	15-3/4	13	13-1/2
scription	Anchor Specifics	Location 1 - San Diego Harbor - Uniform Fine Sand (continued)			!	With original stabilizers	With original stabilizers	With stabilizers	With stabilizers		\$ 6 7 6 5 1 1
Anchor Description	Fluke Fixed/ Angle, Movable deg Fluke	ego Harboi	£	æ	£	Σ	£	ía,	Sa.	14.	įs.
	Fluke Angle, deg	- San Di	32	32	32	37	37	35	35	,	,
	Actual Weight, lb (kg)	ocation 1	1,408	1,408	1,408	3,000	3,000	11,370	11,370	2,200	2,200
	Nominal Actual Weight, Weight Ib (kg) Ib (kg	Ļ	(079)	(079)	(079)	3,000	3,000	000,6	000'6	(1,000)	(1,000)
To backer	Carendar Date (Julian)		61/5/79	4/5/79	4/5/79	6/5/79	(56)	4/5/79	4/5/79 (95)	61/9/7	(96) (96)
	Anchor		STEVFIX	STEVFIX	STEVFIX	STATO	STATO	Stockless	Stockless	BRUCE	BRUCE
	No. Series		6	5	6	71	71	13	13	16	91
	No.		-	7	۳		7	-	7	-	7

Table 2. Continued

Test	1												
Series Ancbor Date Nominal Actual Fluke Fixed/ Series (Julian) Weight, Weight, Angle, Fluke Fluke (Julian) Weight, Weight, Hovable Hovable (Julian) Weight, Weight, Hovable Hovable (Solution 1 - San Diego Harbor - Uniform Fine Sand (contin 1) BRUCE (96) (1,000) 2,200 - F (200 kg) after load cell (1,000) 2,200 - F (200 kg) after load cell (1,000) 2,200 - F (200 kg) after load cell (1,000) 2,200 - F (200 kg) after load cell (1,000) 2,200 - F (1,000 kg) after load cell (1,000) 2,200 - F (1,000 kg) after load cell (1,000) 3,000 1,070 35 H (4,11) R in. stabilizers (100) 3,000 3,000 31-1/2 H (4,11) R in. stabilizers (100) 3,000 3,000 31-1/2 H (4,11) R in. stabilizers (100) 4/11/79 6,000 6,000 32 H (0riginal stabilizers (101) (101)			Remarks				Anchor flipped over at an efficiency of about 10; stabilizers are too short.	Anchor performance was erratic; initiated embedment then rotated and came out.	Anchor built up load uniformly, was stable, developed an efficiency of 21.	Anchor flipped at about 10 ft of drag.	Anchor efficiency varied between 9 and 16: anchor unstable and flipped	at above efficiencies; longer stabilizers appear needed.	
Series Anchor Calendar Nominal Series Series Anchor Californ Weight, 15 (46) 15 (46) 15 (46) 16 (46) 17 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 19 (46) 1		1	water Depth, ft	nued)	13-1/2	13-1/2	14-1/2	15	14-1/2	15-1/4	15-1/4	15	14-1/2
Series Anchor Calendar Nominal Series Series Anchor Californ Weight, 15 (46) 15 (46) 15 (46) 16 (46) 17 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 19 (46) 1		scription	Anchor Specifics	r - Uniform Fine Sand (conti	With 1 cable depressor (200 kg) after load cell	With 1 cable depressor at (200 kg) shank	With 26 in. stabilizers	With 18 in. stabilizer extensions	With 18 in. stabilizer extensions	With original stabilizers	Original stabilizers	Original stabilizers	Original stabilizers
Series Anchor Calendar Nominal Series Series Anchor Californ Weight, 15 (46) 15 (46) 15 (46) 16 (46) 17 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 19 (46) 1		Anchor De	Fixed/ Movable Fluke	ego Harbo	í4	ís.	æ	æ	E	£	r	r	¥
Series Anchor Calendar Nominal Series Series Anchor Californ Weight, 15 (46) 15 (46) 15 (46) 16 (46) 17 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 19 (46) 1			Fluke Angle, deg	- San Di	,	,	æ	37	31-1/2	31-1/2	33	32	32
Series Anchor Calendar Nominal Series Series Anchor Californ Weight, 15 (46) 15 (46) 15 (46) 16 (46) 17 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 18 (46) 19 (46) 1			Actual Weight, 1b (kg)	ocation 1	2,200	2,200 (1,000)	1,070	3,000	3,000	3,000	6,000	6,000	6,000
Series Anchor 17 BRUCE 18 STATO 14 STATO 14 STATO 19 STATO 10 STATO 10 STATO 11 STATO 12 STATO 13 STATO 14 STATO 15 STATO 16 STATO 17 STATO 18 STATO 19 STATO 10 STATO 10 STATO 11 STATO 12 STATO 13 STATO 14 STATO 15 STATO 16 STATO 17 STATO 18 STATO 19 STATO 10 STATO 10 STATO 11 STATO 12 STATO 13 STATO 14 STATO 15 STATO 16 STATO 17 STATO 18 STATO 19 STATO 10 STATO 11 STATO 12 STATO 13 STATO 14 STATO 15 STATO 16 STATO 17 STATO 18 STATO 19 STATO 10 STATO 10 STATO 11 STATO 12 STATO 13 STATO 14 STATO 15 STATO 16 STATO 17 STATO 18 STATO 18 STATO 19 STATO 10 STATO 11 STATO 12 STATO 13 STATO 14 STATO 15 STATO 16 STATO 17 STATO 18			Nominal Weight, 1b (kg)	1	(1,000)	(1,000)	1,000	3,000	3,000	3,000	6,000	000'9	6,000
Series A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			Calendar Date (Julian)		61/9/4	(96)	(66) 61/6/7	4/10/79 (100)	4/10/79 (100)	(001)	6/11/79	62/11/7	(101)
			Anchor		BRUCE	BRUCE	STATO	STATO	STATO	STATO	STATO	STATO	STATO
2 × × × × × × × × × × × × × × × × × × ×					13	5	•	2	21	2	2	61	19
	- {	•	No.			~	N	м	4	'n	-	~	8

Table 2. Continued

L'						7	Anchor Description	scription	3	
١	Carine	Anchor	Calendar Date	Nominal Meicht	Actual	Fluke	Fixed/	Anchor Charifine	Water Depth,	Remarks
į			(301100)	1b (kg)	1b (kg)	deg	Fluke			
				7	ocation 1	- San Di	ego Harbo	Location 1 - San Diego Harbor - Uniform Fine Saud (continued)	inued)	
	70	Stockless	6/11/79	5,000	056,2	35	<u> </u>	Tandem - shank to shackle	13	Arrangement easy to install; both
7	20	Stockless	4/11/79	2,000	5,950 (ea)	35	(s.	figging, cotal weight of	13	ducinos apparently tunctioned to peak capacity.
_	21	Stockless	4/12/79	2,000	5,950	35	ie,	Tandem - crown to shackle	16-3/4	Performance somewhat less than
~	21	Stockless	4/12/79	5,000	5,950 (ea)	35	L .,	11,900 lb	16-1/2	somewhat easier to install.
	22	Stockless	4/12/79 (102)	2,000	5,950 (ea)	35	Ĺ	Tandem - ground ring to shackle rigging; total weight is 11,900 lb	13	Performance comparable to crown to shackle technique but installation more difficult.
4	^	Hook	4/12/79	(260)	1,230	32	×	Without auxiliary flukes	12	
8	7	Hook	4/12/79 (102)	(260)	1,230 (560)	32	X:	Without auxiliary flukes	11-1/2	
			Lac	Location 2 -		Harbor	- Anchora	San Diego Harbor - Anchorage Area (1-3 Ft Mud Over Dense Clayey Sand)	nse Claye)	Sand)
	54	STATO	6/16/79	3,000	3,000	31-/12	E	With 18-in. stabilizer	41	Anchor embedded quickly and reliably
2	5,7	STATO	4/16/79	3,000	3,000	31-1/2	æ	With 18-in. stabilizer	17	18, but pulled out with continued
es .	24	STATO	4/16/79 (106)	3,000	3,000	31-1/2	X:	With 18-in. stabilizer extensions	39	sand clogged the flukes and pro- hibited re-embedment.

Table 2. Continued

		\neg	Ţ				1
	Remarks		Sand)				
	Water Depth,	ft	Jense Clayey	38	33	36	_
ption		Anchor Specifics	Location 2 - San Diego Harbor - Anchorage Area (1-3 Ft Mud Over Dense Clayey Sand)		:	1	_
Anchor Description	Fixed/	Movable Fluke	- Anchorage	Σ	Æ	3 :	
	Fluke	Angle, deg	, Harbor	32	32	32	_
	Actual	Weight, 1b (kg)	San Diego	1,408	1,408	(079) (079)	(079)
	Nominal	Weight, 1b (kg)	tion 2 -	(079)	(079)	(079)	
	Calendar	(Julian) Weight, Weight, Angle, Movable 1b (kg) 1b (kg) deg Fluke	Loca	6/16/79	(106)	(106)	(300)
	Anchor			STEVFIX	STEVFIX	STEVFIX	_
	Test	No. Series	1	25			
	ے ہے	Š.	1	Ŀ	- 7		_

Table 3. Summary of Test Data for San Diego Harbor Mooring Tests

Remarks	Anchors jetted-in with flukes down on all San Diego moorings; -SE pull on mooring, max load was 118,000 lb.	-SW pull on mooring; max load 115,000 lb.	-E-W pull on moorings, max load 99,000 lb; buoy 51 displaced at above load.
Water Depth	36	37	28
Mooring Chain Size/Length Buoy to Anchor	20,000 22 ft - 2-3/4 in. riser; 225 ft - 2-1/2 in. leg	20,000 23 ft - 2-3/4 in. riser; 225 ft - 2-1/2 in. leg	20,000 16 ft - 2-3/4 in. riser; 225 ft - 2-1/2 in. leg
Anchor Weight, 1b	20,000	20,000	20,000
Anchor	Stockless without stabilizers	Stockless without stabilizers	Stockless without stabilizers
Mooring Class	æ	æ	æ
Mooring Mooring Number Class	11	18	3/27/79 50 & 51
Date	3/26/79	3/26/79	3/27/79

Table 4. Summary Test Data for Indian Island Anchor Tests

	Remarks	Anchor embedded quickly; began	to fotale at about 30 It drag.				Anchor load cell erratic for test	7; at comparable drag distance (41 ft) fixed-fluke anchor deck tension was 17,000 to higher than movable fluke anchor.	Anchor consistently held 4-5 times its	own weight; also refers to single anchor performance of tests 11 and 12.
	Water Depth (ft)	86	82	78	87	81	79	16	35	92
cription	Anchor Specifics	26 in. long stabilizers	Without auxiliary flukes	Without auxiliary flukes		With 1 cable depressor (200 kg) after load cell	With stabilizers	With stabilizers	With stabilizers	With stabilizers
Anchor Description	Fixed/ Movable Fluke	F	E	£	ís,	is.	(4.	r	ís.	j .
	Fluke Angle (deg)	99	95	95	,	•	87	84	87	87
	Actual Weight 1b (kg)	1,070	1,230	(380) 1,230 (560)	2,200	2,200	11,370	11,370	5,950	5,950
	Nominal Weight Ib (kg)	1,000	(260)	(260)	(1,000)	(1,000)	000'6	000.6	2,000	5,000
	Anchor	STATO	Hook	Hook	BRUCE	BRUCE	Stockless	Stockless	Stockless	Stockless
	Date	61/61/9	6/20/19	6/20/19	6/20/19	6/20/19	6/21/19	6/21/79	6/11/9	6/21/19
	Test No.	_	7	е	4	٠	_	•	•	2

Table 4. Continued

Remarks		Both tandem arrangements were equally efficient: crown-to-shackle approach	slightly easier to install; anchor seems to be initiating rotation near 35 ft of drag (about 15 ft actual anchor drag).	Anchor penetration about one-half that of fixed fluke anchor; 10,000-15,000 lb reduction in dock tenesion from fixed	fluke anchor.					Peak deck tension almost 20,000 1b less than stabilized welded-open fluke version.
3	water Depth (ft)	86	92	89	88	92	78	83	82	89
Anchor Description	Anchor Specifics	Tandem - shank to shackle;	Tandem - crown to shackle; total weight is 11,900 lb	With stabilizers With stabilizers	Twin shank anchor		With flukes fixed open	With fluke extensions and flukes fixed open		Without stabilizers
	Fixed/ Movable Fluke	14	ís,	ΣΣ	ís.	Σ	i a.	(4)	E	E
	Fluke Angle (deg)	84	87	8 8 7	ı	20	20	20	20	20
	Actual Weight 1b (kg)	5,950	5,950 (ea)	5,950	750	1,408	1,408 (640)	2,068 (940)	2,200 (1,000)	10,500
	Nominal Weight 1b (kg)	2,000	2,000	5,000	(340)	(049)	(640)	(0%6)	(1,000)	000'6
Anchor		Stockless	Stockless	Stockless Stockless	BRUCE	STEVFIX	STEVFIX	STEVFIX	STEVMUD	Stockless
Date		6/22/19	6/23/79	6/23/79 6/23/79	6/23/19	6/23/19	6/57/9	6/54/19	6/54/19	6/22/19
Test No.			12	5 4	15	11	18	19	50	21

Table 4. Continued

	Remarks		Extended stabilizers did not appear to degrade performance; anchor penetrated and held well.		Anchor penetrated and held well but rotated; extended stabilizers might improve performance.
	Depth (ft)	83	82	83	88
cription	Anchor Specifics		With 18-in. stabilizer extensions		With original stabilizers
Anchor Description	Fixed/ Movable Fluke	(Au	E	Σ	£
	Fluke Angle (deg)	,	20	95	20
	Actual Weight 1b (kg)	1,320 (600)	3,000	1,100 (500)	009'9
	Nominal Weight 1b (kg)	(009)	3,000	(200)	000,9
	Anchor	BRUCE	STATO	STEVMUD	STATO
	Date	6/52/9	6/25/79	6/22/19	6/25/79
	Test No.	22	23	24	25

Table 5. Typical Data Output for Anchor Test Pull

	STATO	ANCHOR TEST	1837					
TEST DATE	101							
TEST NO. TEST SPRIFS	- 61							
TEST APFA	CAN DIEGO HARROD 1500 FT. SOUTHFAST OF RIINY 49	1500 FT.	SOUTHFAST OF	¥ C	67			
CTABT-FAN TIMES	1101 - 1172							
SEAFL OOR TYPE	FINE SAND BOTTO	M. DEPTH -	1-17 FT. MLLW					i
ANCHOR TYPE	CTATO . AMONI, A. NOPMAI STARTI TYFINS	I.A. NOPMAI	STARTI TZFRS	2	12 NFG. MOV. FLUKES	> 2	Ē	XE.
PETER WEIGHT	. 81 00.0006		-					
FILING BUGIE TYPE.	12.00 DFG A	X 1 J= 1 AUM=U	±61 x					
ALIN. ANCHOO TYPE								
ALIX. ANCHOD WFIGHT	0.00 LR.							
MAIN-AUX ANCHOR SEPAPATION	0.0							
DEPAFSONS - WT. EACH-TOTAL WT.	1 6 6 1 6	0.0 LP.		Š	4	3	Ų	200
MONDENG I INE DESCRIPTION	ANCHOR TO IRRIT VISIN STITUTION OF THE THE TANK OF THE	12 .N12.Y	UNITAR CHAIN	*	-	·	<u>.</u>	1

Anchor depth at end of drag measured — centerline of shank at anchor crown = (-15) inches.	- OCCTITOF CHANK ANGIF INDICATES CHANK TIP RFLOW CROWN																			
Note Anchor depth at end of drag measured – centerline of shank at anchor crown = (-15)	MINTE - DOCTT	ň.	٠ ا ۵	14445.1	1.31661	12H44.0	12564.0	11654.3	11200.1	1076a.B	9.24.01	OBBO. F	4°C 2 40	9404° K	0,000	964G.	4.4.0	972F. 7	10675.7	1 2997.6
Ž		7.	1999	۲.	۲۰,		15.1	r.	15.1	۲۰۰۶	15.3	۲°۶۱	٠.		۲,	٠. م	15.	15.1	٦.	15.3
	TIO NFOTH VFTCHT	=	7 7 7 4	υ σ	A. A.	۸.	C & Z	٥.	18.0	18.0		10.0	- 6-	· •	C*0~	14,7	18.¢			
FROFFOTH	ANCHOD FILIKE WATEO DEDTH TOTAL BOTTOM	12	FEFT	۲۰۰۱	15.2	15.1	15.4	15.4	15.4	4.5	16.1	14.1	٠.٠	16.3	۲۰۶۱	76.2	9			
IPFO WATE	14. WATE	-	1444	14.2	14.4	14.5	13.2	13.4	14.4	14.4	14.5	14.4	14.3	7.5	14.2	13.A	13.5			
- INITIAL CHANK DEDTH ZEDAFD TO BEFLECT MFAGIDFO WATFORFOTH	ON BOTTOM ON BOTTOM OFPTH TIP OFPTH	5.	, AS	8465.1	7.5155	C \$707	454P.0	5654.3	5208.1	4748.R	4236.9	ABO.A	4852.4	3404F	9407.9	1465.5	7147.4	1726.3	4475.3	7097 . A
) TO 0E!		o	CEFT	172.8	145.9	136.9	130.6	112.7	103.9	A5.1	A. 7.	71.4	76.A	49.7	71.0	73.1	62.B	74.3	93.7	159.5
+ ZFBNFF	CHAIN LENGTH CHAIN WEIGHT ANCHOR CROWN	α	r foc	4.0°	۴. ۵۲	F. 44	۲.67	K4.A	79.A	8.10	A. 7.	a . o . i	A.F.C.	4.60	131.A	130.A	139.A	4 . F F !	115.8	45.9
K DEPT	10. 11.	^	ner									3.5	3.4	3.4	E 6	_	_			4
I Al CHAN	ANGE ANGE	ď	PFG	ı,	۲.	3.2	10.4	c a	7.,	7.7	2.5	c a	0	10.0	٠,٥		12.5		17.8	11.0
	POTATION ANGLE SHANK ANGLE WIPE POPE ANGLE DECK HORITS, FOOCE	U	ن ايد د	6.4-	-4.3	-4.3	-2.5	7.5	6.0		7,2	2.5	2.5	5	9	4	-10.8	18.5	77.5	-50.0
AT CA	, , , , , , , , , , , , , , , , , , ,	4	FFET	14.0	14.0	0.4	4.6	15.0			ر د		5.5	2	4	7	7.5	2	. v	15.
	NGAG NISTANCE NFCK TENSION ANCHOP TENSION DACKAGE NEPTH	٣	KIPA	c • c	7.5	11.3	15.0	75.0	37.5		67.5	, C	95.0	6	α	40	0.50	000		20.4
	1. 0985 2. 05CK 3. 8MCHG	٨	K TOS	20.0	2.0	4	604	6.0			9	200	1 24 0	200		-				44.0
	-0 - 3	-	-			0.4	4	0			9 6 7		17.5			4 60			4 00	31.4

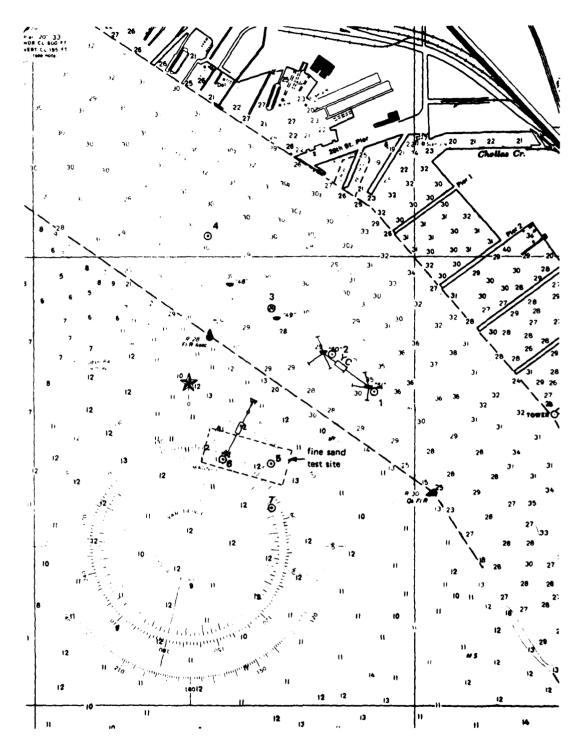


Figure 1. Test and core locations at San Diego Harbor - location 1.

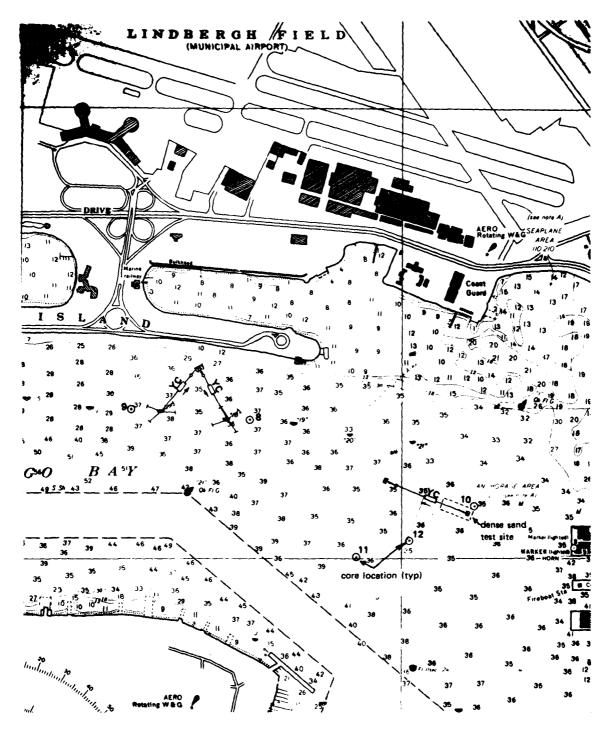


Figure 2. Test and core locations at San Diego Harbor - location 2.

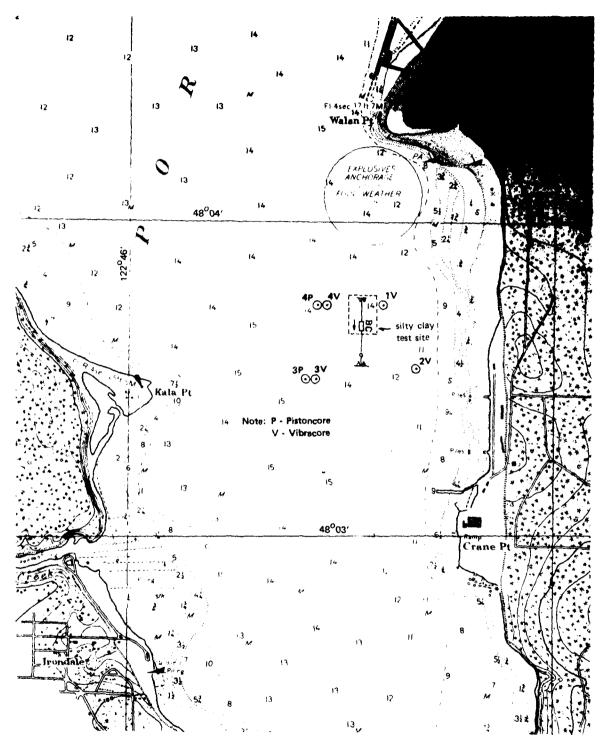


Figure 3. Test and core locations - Indian Island.

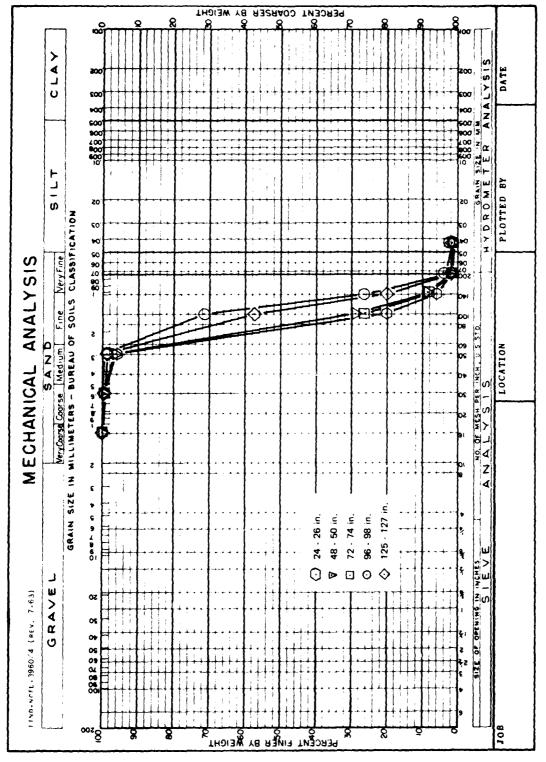


Figure 4. Grain size distribution curves for Vibracore 5 - San Diego Harbor.

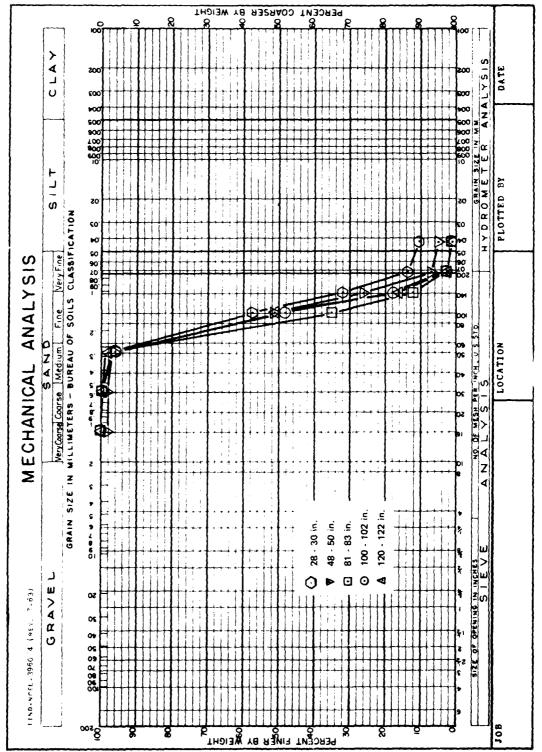


Figure 5. Grain size distribution curves for Vibracore 6 - San Diego Harbor.

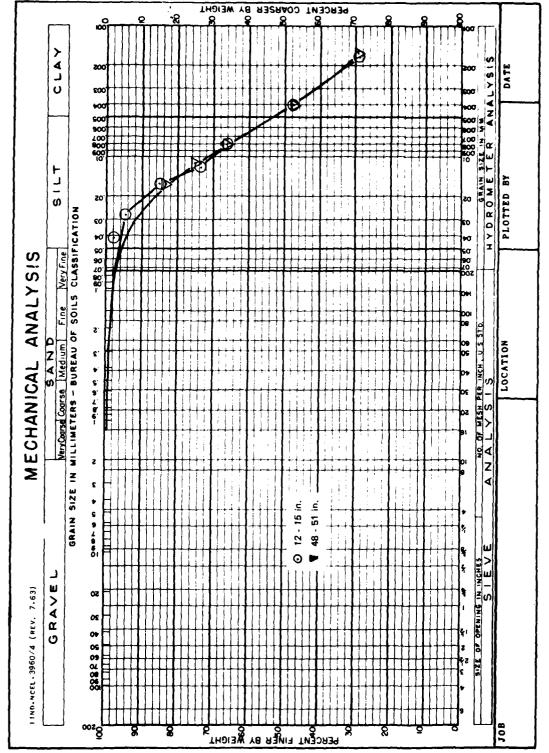


Figure 6. Grain size distribution curves for Vibracore 3 (12 to 51-inch penetration) - Indian Island.

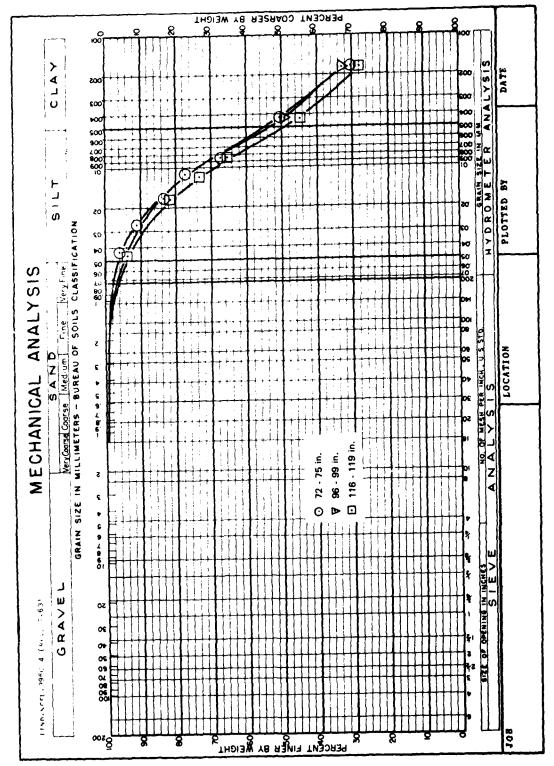
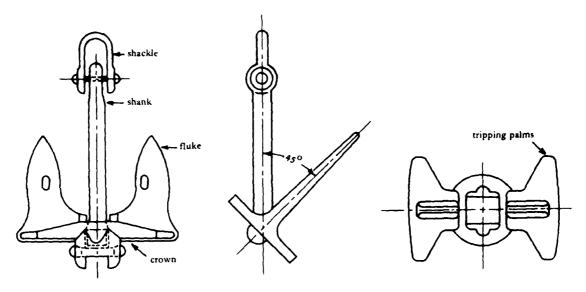


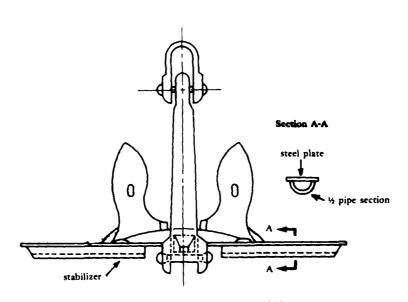
Figure 7. Grain size distribution curves for Vibracore 3(72 to 119-inch penetration) - Indian Island.



Figure 8. Barge crane with all test anchors.



a. Navy Standard Stockless Anchor



b. Navy Stockless Anchor with Stabilizers

Figure 9. Navy Stockless anchor.

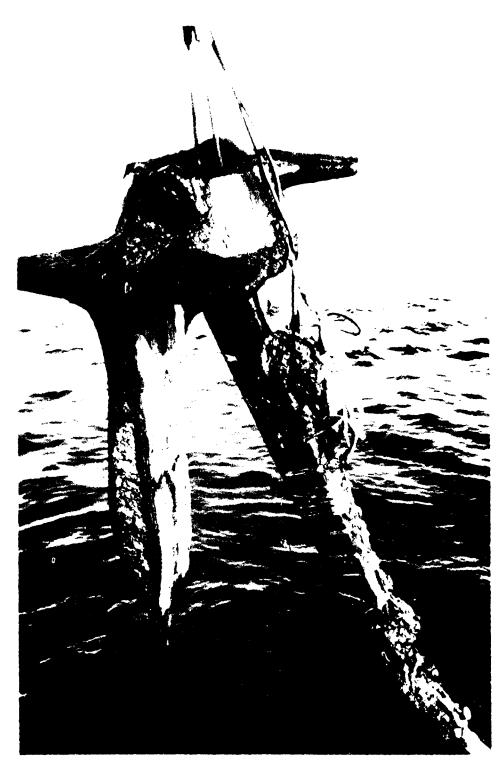
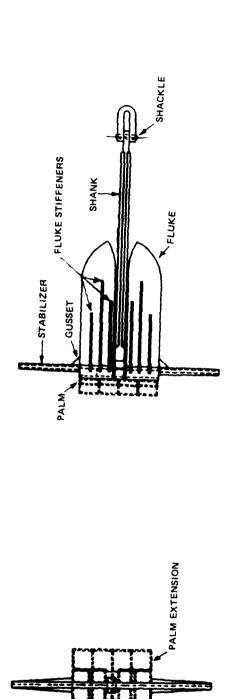


Figure 10. Navy standard Stockless anchor.



Figure 11. Navy Stockless anchor with stabilizers and welded-open flukes.



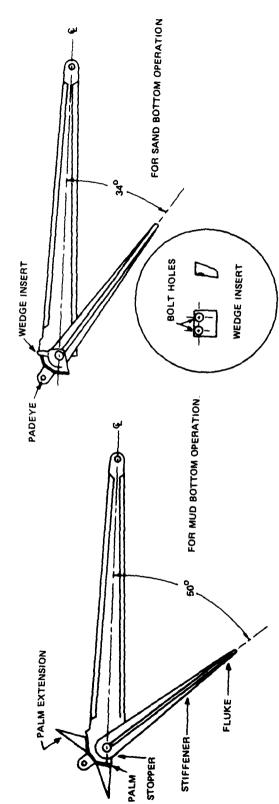


Figure 12. Navy STATO anchor.



Figure 13. Navy 6,000-pound STATO anchor.

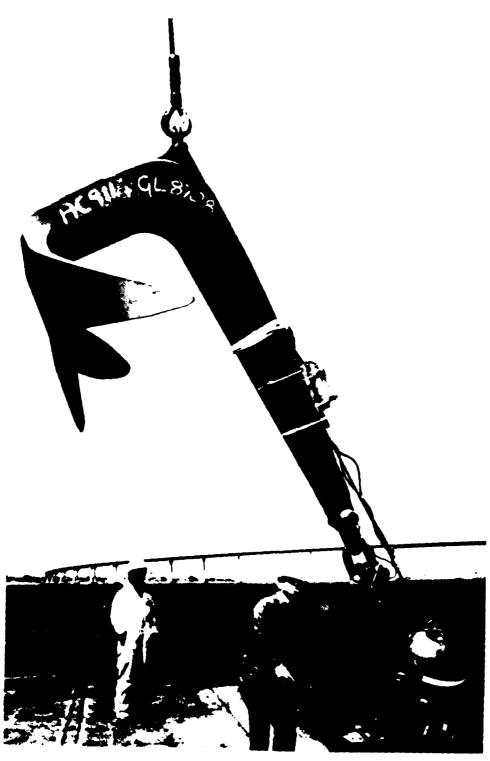


Figure 14. Cast BRUCE anchor.

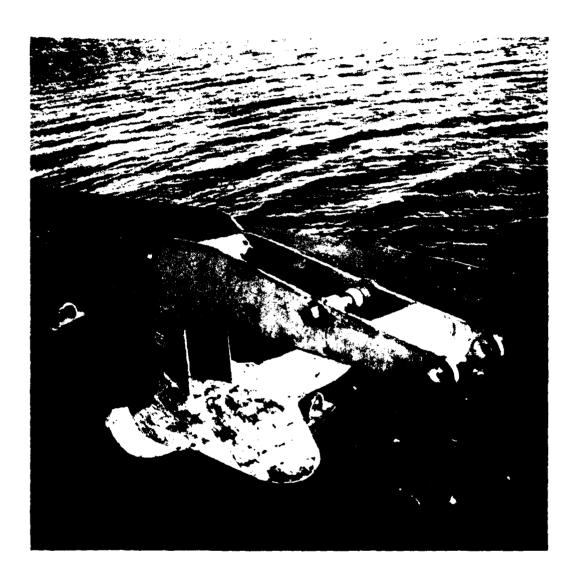


Figure 15. Welded BRUCE anchor.



Figure 16. Cast BRUCE anchor with single cable depressor.

Figure 17. STEVDIG anchor.



Figure 18. STEVMUD anchor.



Figure 19. STEVFIX anchor without mud extensions.



Figure 20. Hook anchor.

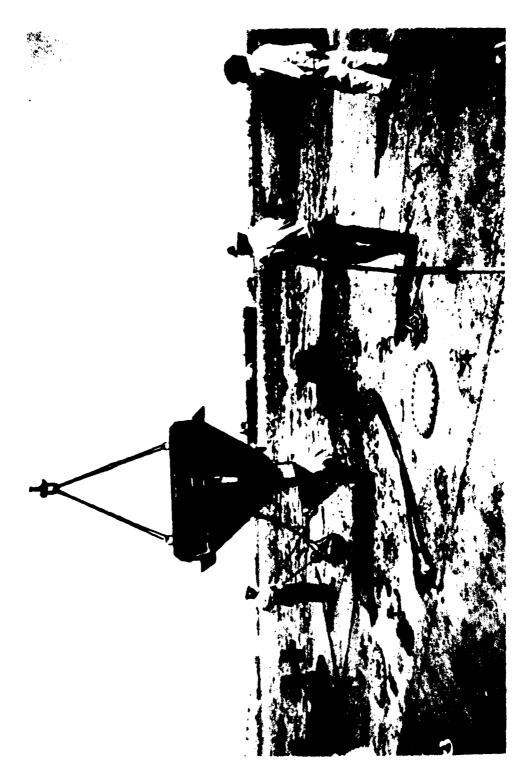


Figure 21. Hook anchor with auxiliary flukes.

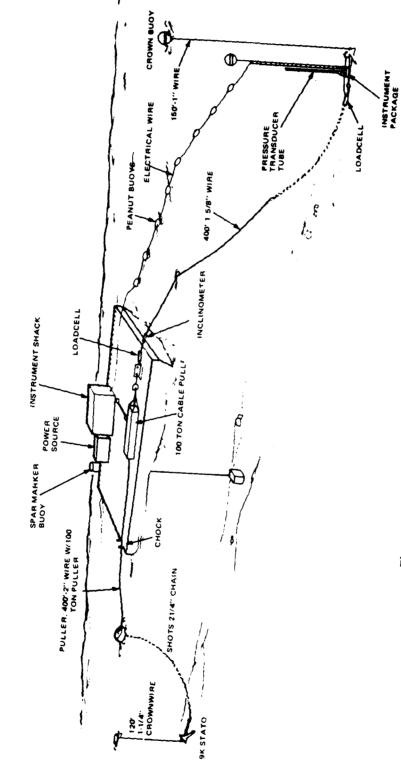


Figure 22. Anchor test setup showing major components.



Figure 23. Spar marker reference buoy.



a. San Diego System



b. Indian Island System

Figure 24. Underwater portion of test measurement system.

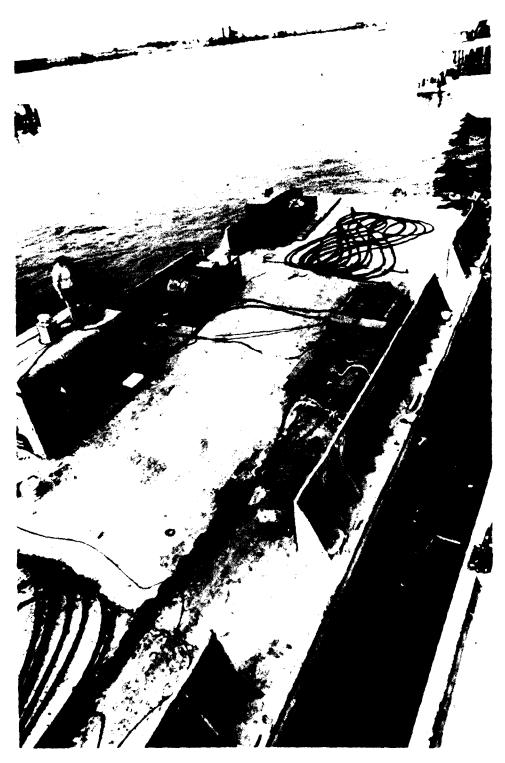


Figure 25. Test deck layout showing cable pulling system and prerigged test wire.



Figure 26. Test deck layout showing deck load cell, cable puller and faked electrical test wire.

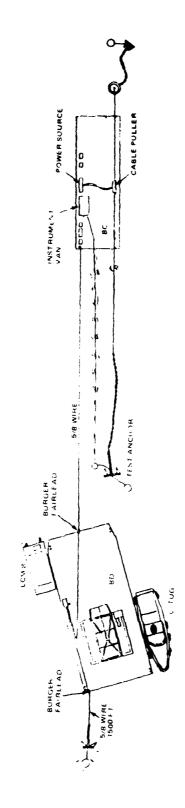


Figure 27. Overall test layout - single and tandem anchor tests

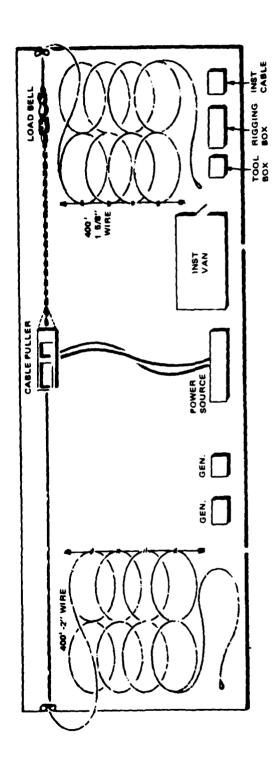


Figure 28. Barge layout for anchor test.

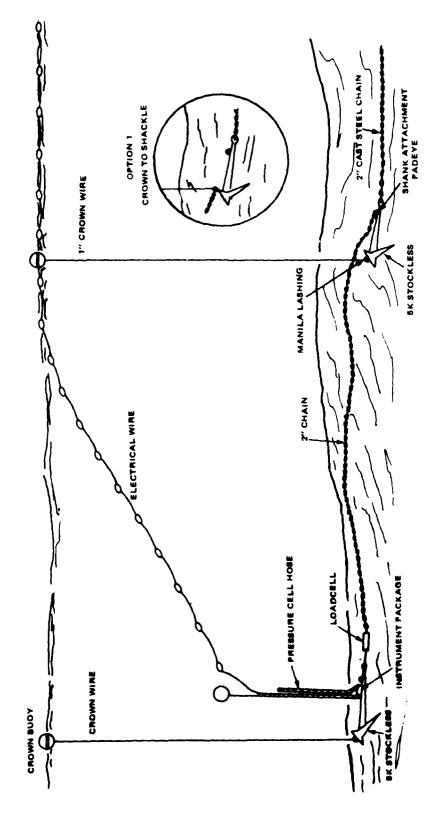


Figure 29. Tandem anchor test setup for shank-to-shackle and crown-to-shackle techniques.

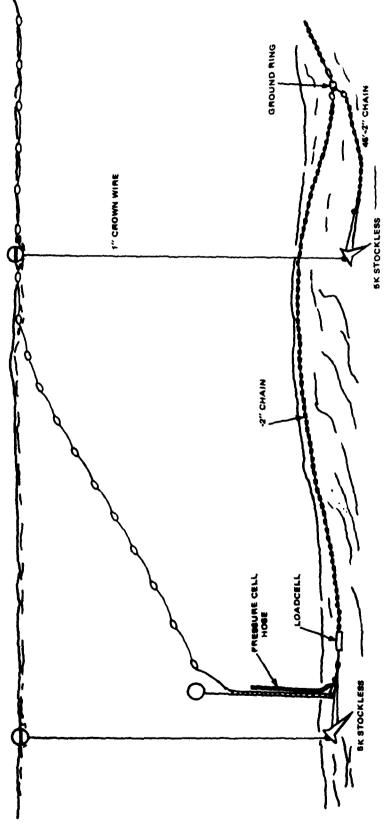
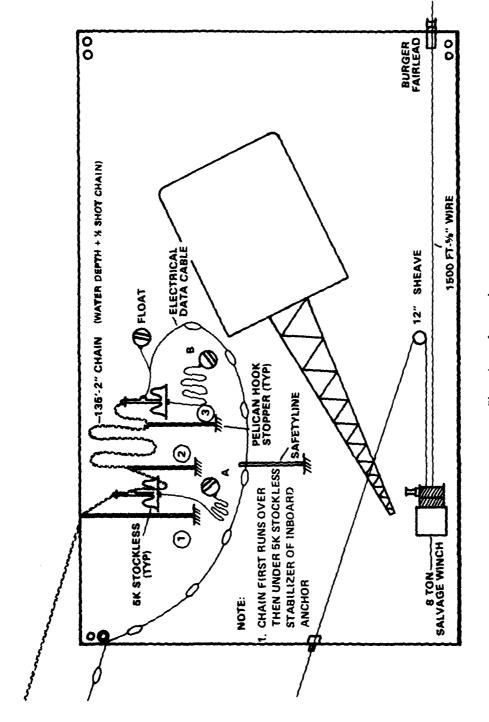


Figure 30. Tandem anchor test setup "ground ring to shackle" technique.

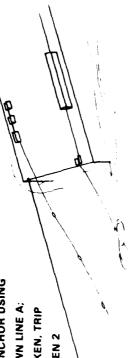


a. Plan view of crane barge.

Figure 31. Tandem anchor deployment method used at Indian Island at 90-foot water depth.



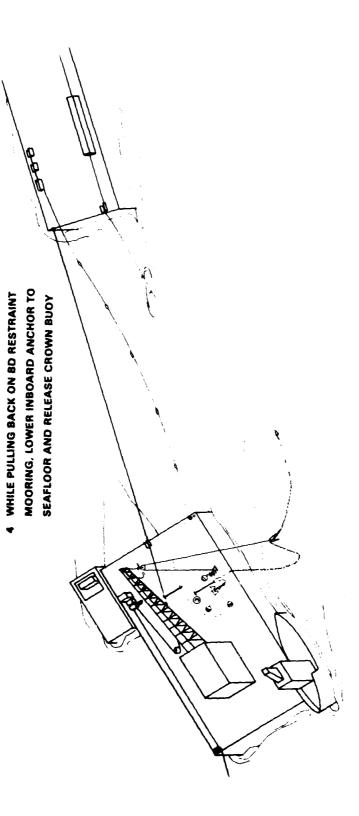
3 PICK UP INBOARD ANCHOR USING SHEAVE OVER CROWN LINE A; ONCE STRAIN IS TAKEN, TRIP PELICAN HOOK 1 THEN 2



b. Beginning anchor deployment.

Figure 31. Continued.

. 3 \ E.



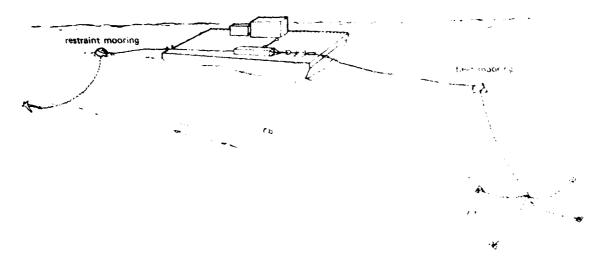
c. Lowering inboard anchor to seafloor and releasing crown buoy.

Figure 31. Continued.

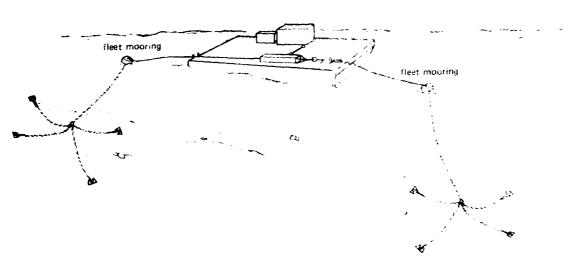
- 6 PICK UP ON OTHER ANCHOR UBING SHEAVE OVER CROWN WIRE THEN RELEASE PELICAN HOOK 3
- 4 BC PULL IN ON DATA CABLE THEN BD RELEASE DATA CABLE FROM CORNER RESTRAINT
- 2 LOWER ANCHOR TO SEABED WHILE PULLING
 BACK ON BD RESTRAINT MOORING: THEN
 RELEASE CROWN BUOY

d. Completing anchor deployment.

Figure 31. Continued.



a. Single mooring test police



b. Dual mooring test pull.

Figure 32. Mooring test arrangements.

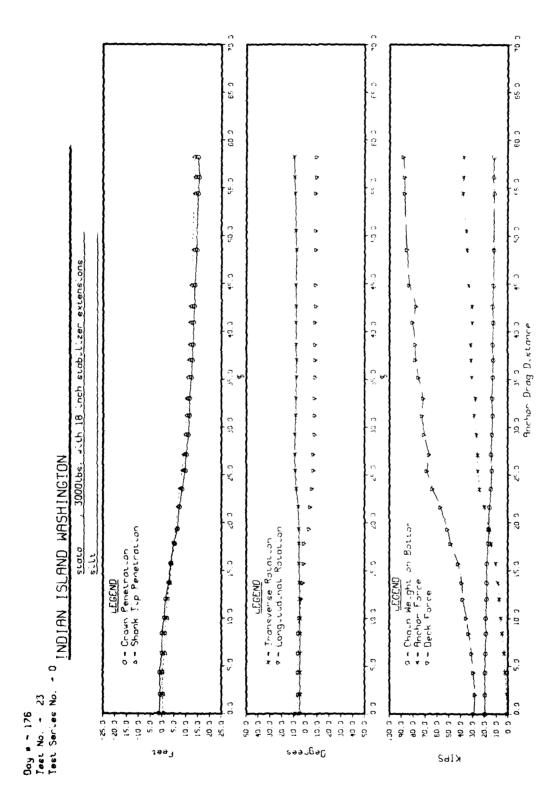


Figure 33. Typical data plot for anchor test pull.



Figure 34. STATO anchor with extended stabilizers attached (standard stabilizer on deck).



Figure 35. STATO anchor with plate addition between shank and wedge insert to reduce fluke angle to about 32 degrees.

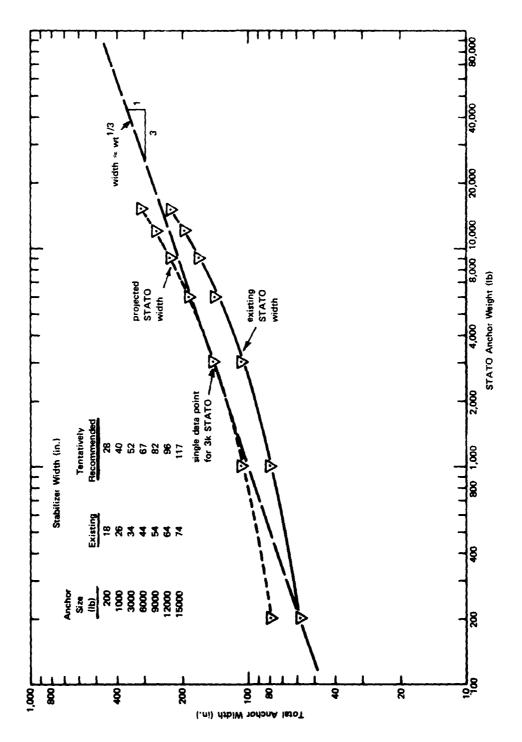


Figure 36. Recommendations for STATO anchor stabilizer lengths.

Appendix A

ADDITIONAL SAN DIEGO HARBOR SEAFLOOR PROPERTIES

Twelve vibracores were taken at San Diego. Of these, only eight cores were analyzed. Principally, San Diego Harbor consists of medium to fine sand with up to 2 to 3 feet of overlying mud in the dredged areas near the moorings (refer to Figures 1 and 2). The shallow area located primarily south of the dredge channel shown in Figure 2 is a uniform fine sand with no detectable surface mud layer. Grain size curves for cores SDV5 and SDV6 (Figures 6 and 7 in the main text) show the extremely uniform nature of the area.

Grain size curves for the remaining six cores are presented as Figures A-1 through A-6. Cores 1, 2, 3, 8, and 9 were taken near prospective moorings and typically show medium to fine sand at expected anchor fluke embedment depths. Cores 10, 11, and 12 were taken to locate an expected soft mud site; however, one was not located. Core 12 was a very uniform, fine-grained sand to 20 feet; it was not analyzed in detail. Cores 10 and 11 showed a very competent strata at 3 to 4 feet below the mud surface. This layer is practically impenetrable to standard ship anchors, yet it is classified as the anchorage area for commercial vessels. The 45- to 47-inch increment of core 10 (Figure A-6) represents the dense clayey sand.

Also provided in this section are plots of accumulative time versus vibracorer penetration depth for several apparently distinct areas (Figures A-7 through A-10). These curves are probably meaningless much below 5 to 7 feet, but they do offer insight into the variability, relative stiffnesses, and sensitivities of certain areas. In particular, Figure A-8 should be noted for cores 5, 6, and 7 at the fine sand test site. The curves are practically superimposed, lending further credence to the uniformity of the fine sand test site.

Figure A-11 provides recent vane shear data for Indian Island mud gathered with a bottom-sitting platform. Shear strength increases almost linearly from zero at the surface to 1-1/2 psi at 21 feet. Remolded shear strength readings were taken at only two depths. These data show a relatively insensitive soil where the ratio of undisturbed to disturbed strength was 1.6 at 7 feet and 2.1 at 10 feet.

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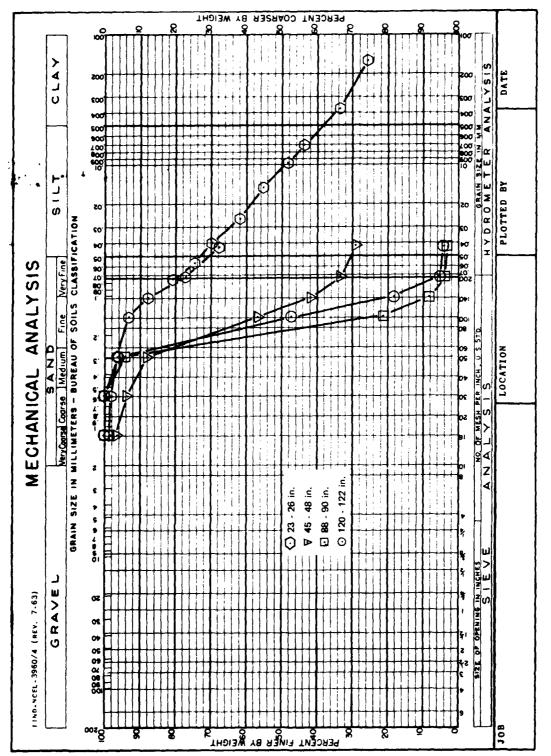


Figure A-1. Grain size distribution curves for Vibracore 1 - San Diego Harbor.

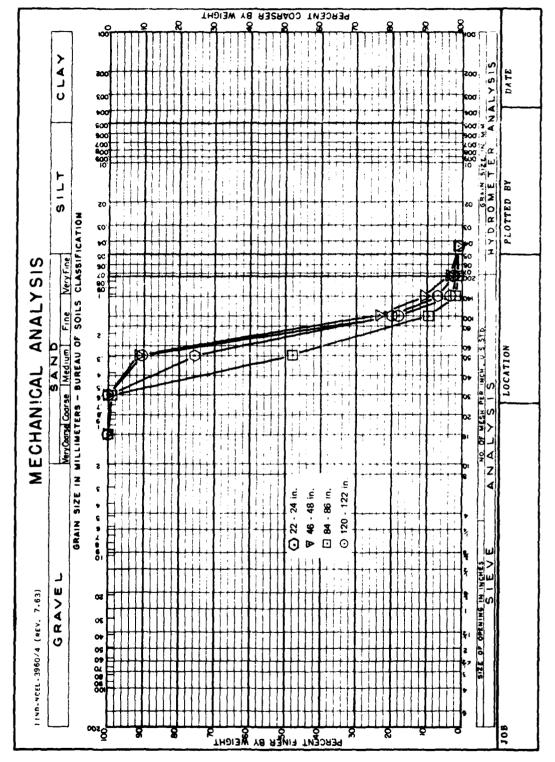


Figure A-2. Grain size distribution curves for Vibracore 2 · San Diego Harbor.

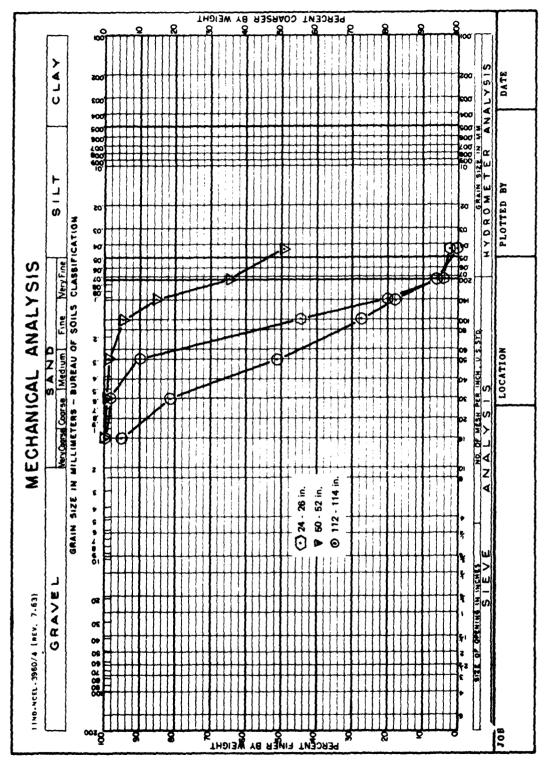


Figure A-3. Grain size distribution curves for Vibracore 3 - San Diego Harbor.

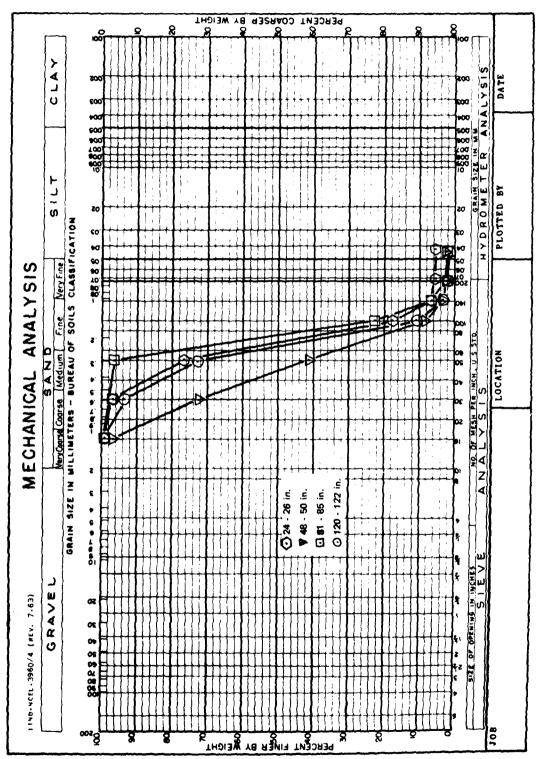


Figure A-4. Grain size distribution curves for Vibracore 8 - San Diego Harbor.

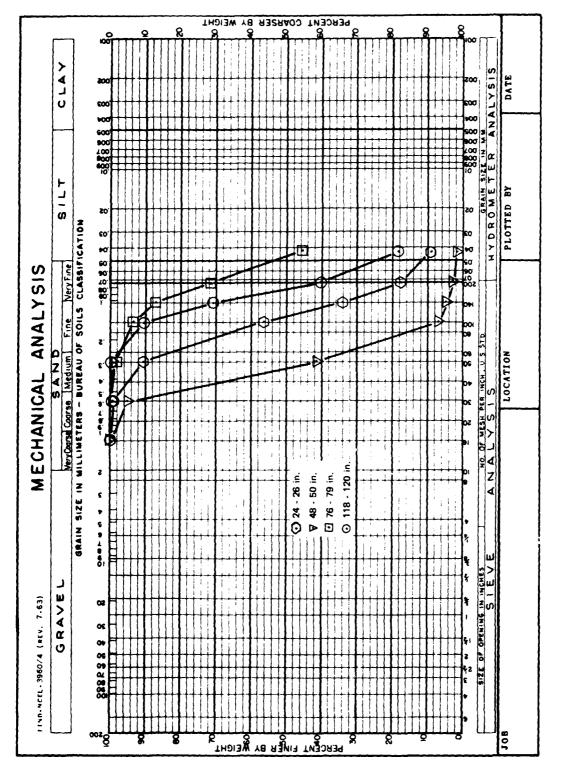


Figure A-5. Grain size distribution curves for Vibracore 9 - San Diego Harbor.

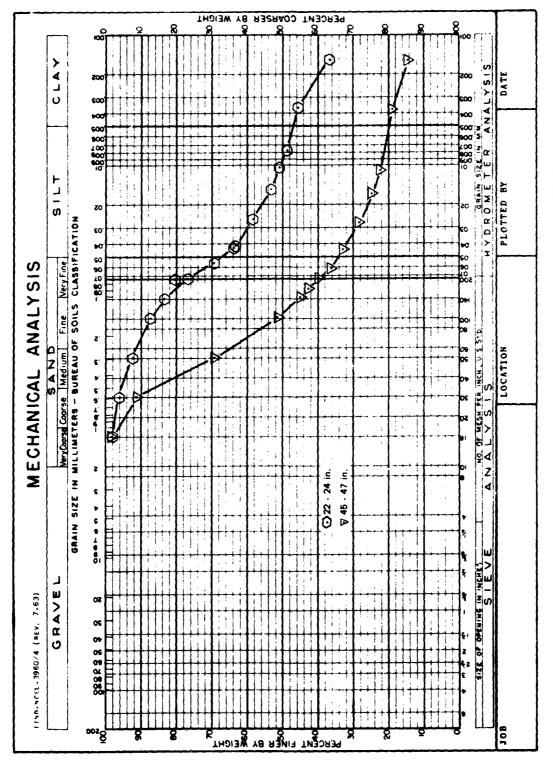


Figure A-6. Grain size distribution curves for Vibracore 10 - San Diego Harbor.

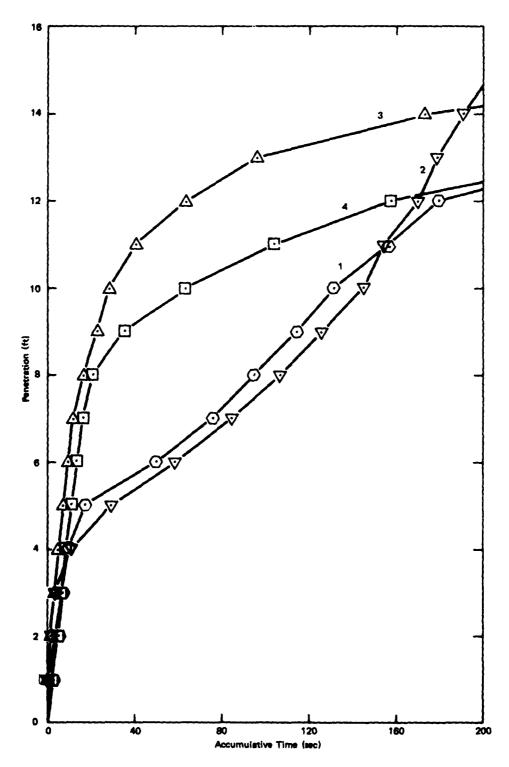


Figure A-7. Vibracorer penetration depth versus time for cores 1-4 - San Diego Harbor.

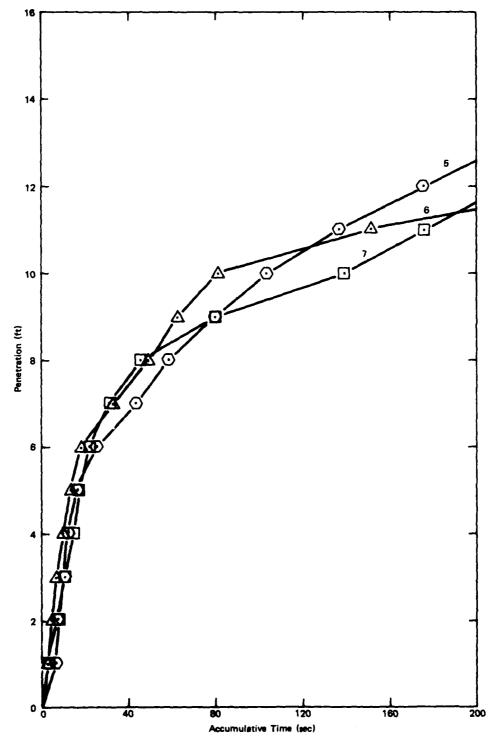


Figure A-8. Vibracorer penetration depth versus time for cores 5-7 - San Diego Harbor.

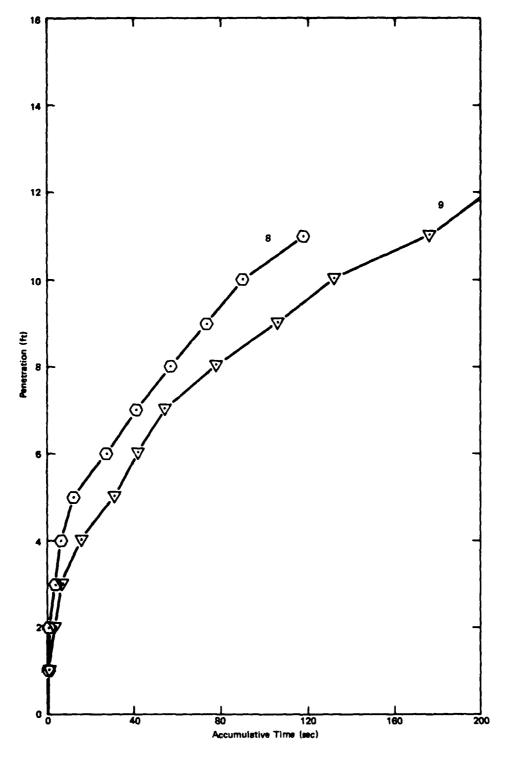


Figure A-9. Vibracorer penetration depth versus time for cores 8-9 - San Diego Harbor.

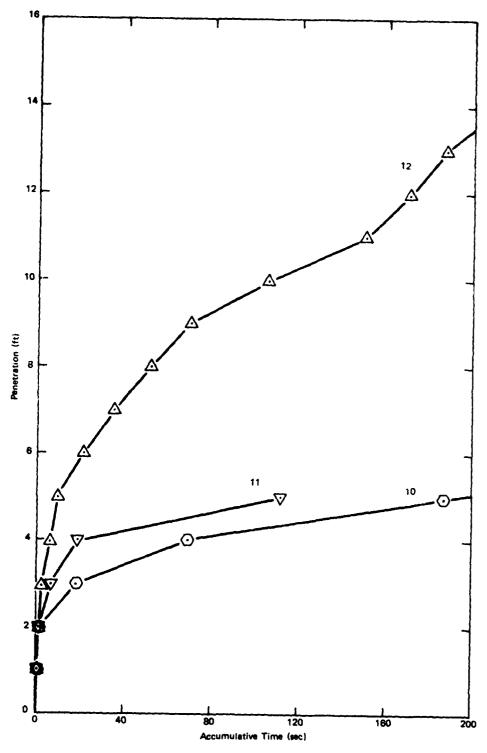


Figure A-10. Vibracorer penetration depth versus time for cores 10-12 - San Diego Harbor.

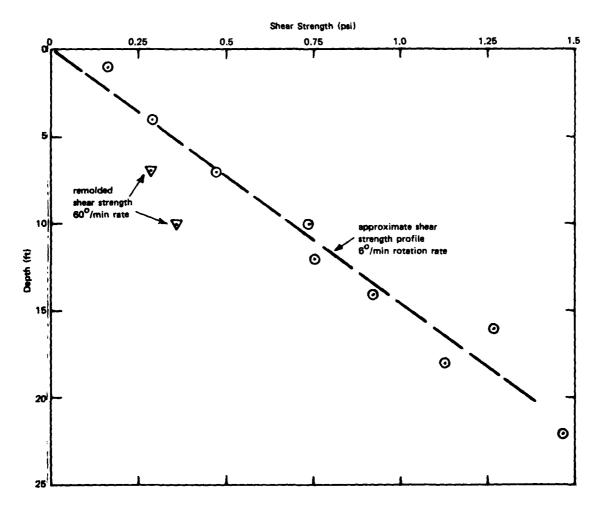


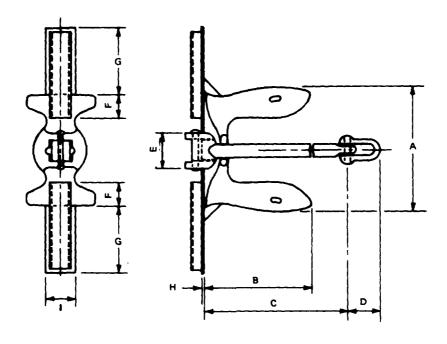
Figure A-11. Vane shear strength profile for Indian Island mud.

Appendix B DIMENSIONS OF ALL TESTED ANCHORS

General dimensions of all the anchors tested are provided. Also included is a tabularized listing of the location of the instrument package on the shank relative to the shackle end of the shank.

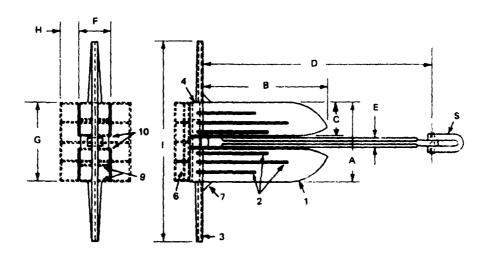
Table B-1. Location of Instrument Package on Anchor Shank

Anch	or	Centerline of Package to Shank Tip, in.		
Name	Nominal Size	San Diego	Indian Island	
STATO	1,000 lb	18	19-1/4	
	3,000 lb 6,000 lb	44 50	34 34	
Stockless	5,000 lb 9,000 lb	45 29	42-1/2 32	
STEVFIX	640 kg 940 kg	16	58 58	
STEVMUD	500 kg 1,000 kg	-	- -	
STEVDIG	1,000 kg	21	-	
BRUCE	340 kg 600 kg 1,000 kg	38 30	38 33 18	
Hook	560 kg	29	43	



Nominal	Anchor Dimensions (in.)								
Weight (lb)	Α	8	С	D	E	F	G	н	-
500	29-3/4	26-7/8	37-1/4	7-5/8	8-1/2		_		_
1,500	43	38-3/4	53-5/8	11	12-1/8	-	} —	l	-
3,000	54-1/8	48-3/4	67-1/2	13-7/8	15-3/8	11	30	1/2	13
5,000	64-1/8	57-3/4	80-1/8	16-1/2	18-1/4	13	36	1/2	16
6,000	67-7/8	62-9/16	85-1/16	17-3/8	19-1/8	14	36	1/2	16
7,000	71-7/16	65-7/8	89-9/16	18-5/16	20-1/8	15	36	1/2	16
9,000	78-1/16	70-3/8	97-1/2	20	22-1/8	16	36	3/4	16
10,000	80-1/2	74-3/16	100-7/8	20-5/8	22-11/16	17	36	3/4	19
13,000	87-7/8	79-1/8	109-3/4	22-1/2	24-7/8	18	40	3/4	19
14,500	90-7/8	83-3/4	114	23-1/4	25-5/8	19	40	3/4	21
18,000	98-3/8	90-3/8	122-3/4	25-1/4	27-3/4	20	45	1	21
20,000	101-7/8	91-3/4	127-1/4	26-1/8	28-7/8	21	45	1	21
25,000	109-3/4	96-7/8	137-1/18	28-1/8	31-1/8	22	48	1	22
30,000	116-5/8	107-1/4	145-5/8	29-13/16	33-3/16	24	50	1	23
40,000	127-3/4	117-13/16	160-1/16	32-11/16	36	27	36	1-1/4	26

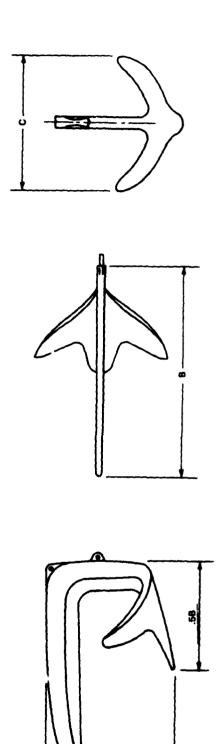
Figure B-1. Dimensions of standard Stockless anchor.



Nominal Weight	Dimensions of Anchors (in.)								
(IP)	Α	В	С	D	ε	F	G	Н	ı
200	23	25	10	42	2	9-1/2	23	6	59
1,000	28	43	75	80			28	- 1	80
3,000	41-1/2	69	18	129	4	19	41-1/2	13	109-1/2
6,000	55	82	24	144	5	21	55	15	143
9,000	62	96	27	160	6	27	62	16	170
12,000	69	108	30	186	7	30	69	18	197
15,000	76	121	33	205	8	32-3/8	76	20	224

Nominal	Thickness of Plates (in.)									
Weight (Ib)	1	2	3	4	5	6	7	8	9	10
200	1/4	1/2	1/4	1/4	1/4	1/4	1/4	1/4 x 4	1/4	1/2
3,000	1-1/4	1	1/2	5/8	5/8	5/8	5/8	1/2 × 6	5/8	5/8
6,000	1-1/2	1	1/2	3/4	3/4	3/4	3/4	5/8 × 7	3/4	3/4
9,000	1-3/4	1-1/8	6/8	7/8	7/8	7/8	7/8	3/4 × 7	7/8	7/8
12,000	2	1-1/4	5/8	1	,	1	1	3/4 × 7	1	1
15,000	2-1/4	1-1/2	5/8	1-1/8	1-1/8	1-1/8	1-1/8	3/4 x 7-1/2	1-1/8	1-1/8

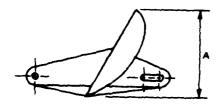
Figure B-2. Dimensions of Navy STATO anchor.

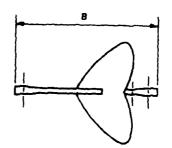


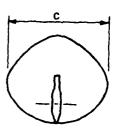
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Dimensions (mm)	B. 1930 2060 2430
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Weight	리 7 48 1320 2200
Nominal	21 5 00 00 21 00 00

•Note: 340 kg Bruce is welded, not cast, and has a twin plate shank separated by specers (see Figure 15.)

Figure B-3. Dimensions of BRUCE anchor.







Nominal Weight						
kg	•	<u>Ib</u>				
600		1320				
1000		2200				
3000		6600				
6500	1	14300				
9000		19800				

Nomina	al Weight			
		A	B	C
kg	<u>Ib</u>	mm	mm	mm
120	264	521	1061	696
200	440	720	1200	830
605	1331	1040	1735	1195
1350	2970	1365	2255	1555
1810	3982	1500	2500	1725

Figure B-4. Dimensions of BRUCE cable depressors.

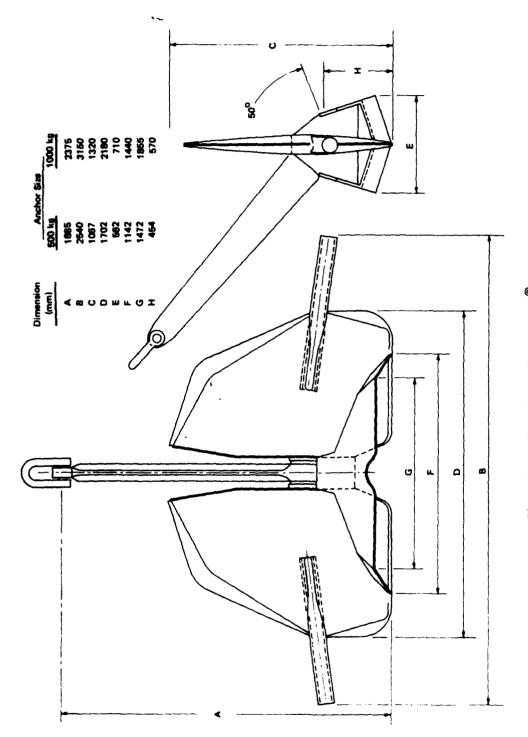


Figure B-5. Dimensions of STEVMUD® anchor.

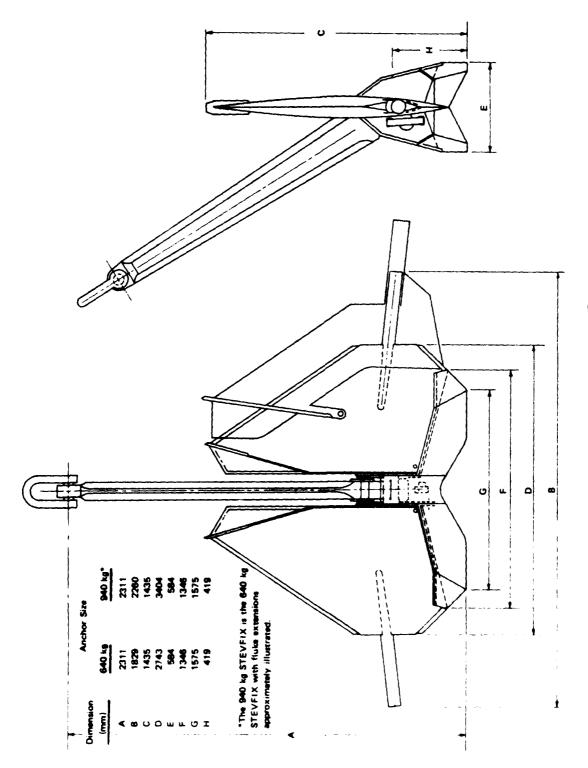


Figure B-6. Dimensions of STEVFIX® anchor.

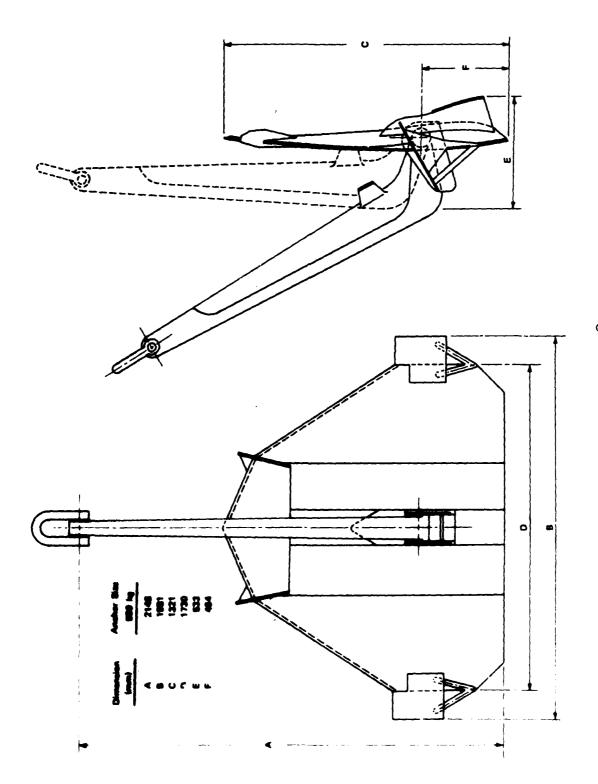


Figure B-7. Dimensions of Hook® anchor.

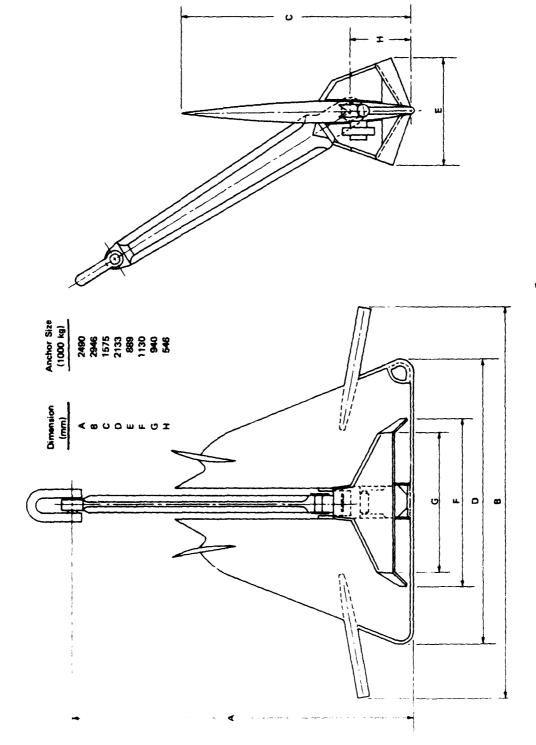


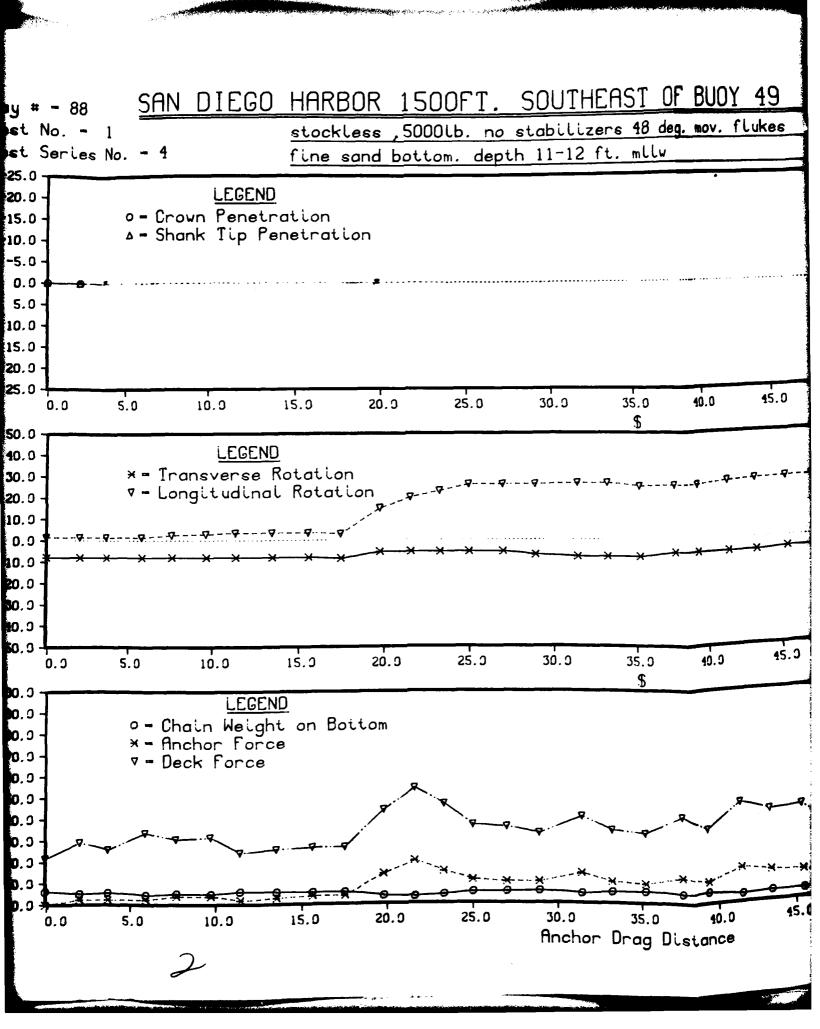
Figure B-8. Dimensions of STEVDIG® anchor.

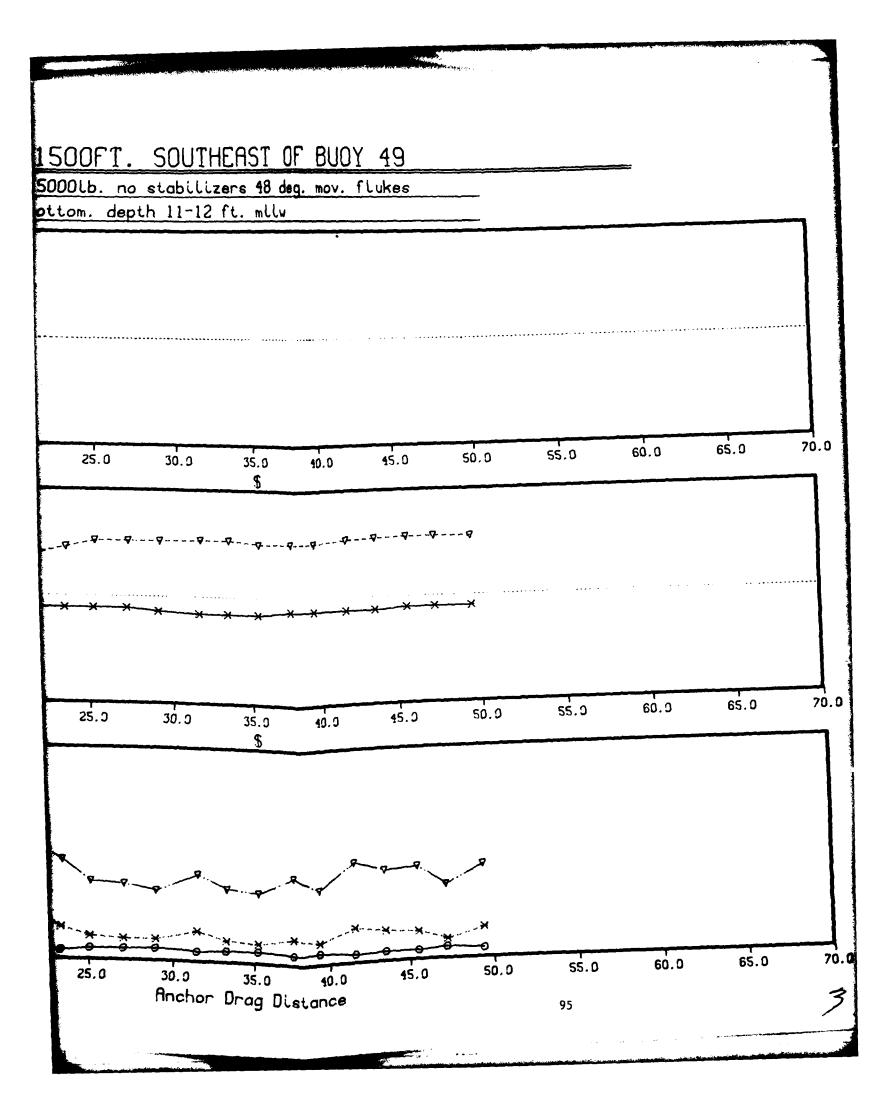
Appendix C

STOCKLESS AND STATO ANCHOR TEST DATA

All test results for the Stockless and STATO anchors are included in this section. Anchor and deck tension, chain weight on bottom, anchor shank tip and crown penetrations, anchor shank longitudinal rotation (pitch), and anchor transverse rotation (roll) are plotted as functions of true anchor drag distance. Presented opposite each data plot is a digital listing of all plotted data plus additional descriptive data that may be useful during the eventual analysis of the data. When data were unavailable either through instrumentation difficulties or because the instrument pack was not used due to time constraints (this occurred at Indian Island), straight lines with a zero ordinate were plotted. There were several instances at San Diego where partial shorts at the load cell electrical connector occurred during testing. The anchor load cell was particularly sensitive to these shorts since its output, exclusively, was amplified at the anchor and transmitted to the vessel. When this occurred, all data but anchor load cell were recorded. At the fine sand site in San Diego Harbor, problems often occurred with the pressure transducer; these did not occur at the deeper dense clayey sand site at San Diego and at Indian Island. Apparently, partial kinking of the pressure transducer hose was sufficient to restrict water flow into the hose. For those tests where depth readings were obviously in error, columns 4, 11, 12, and 13 on the data summaries are absent. Also, anchor shank penetrations are not listed or plotted for the Stockless anchor even when package depth (column 4) is listed. An error was detected in the specification of package location on the shank. The correct location is listed in Table B-1. Shank penetrations can be calculated directly using the correct location in conjunction with anchor dimensions listed in Appendix B and anchor shank angles listed in Appendix C. Listed on most Appendix C tables is an embedment depth of the centerline of the anchor shank at the crown end of the anchor. This depth was recorded by crown wire measurement at the end of the test. This value reflects only the condition of the anchor at the end of drag and not necessarily peak anchor embedment.

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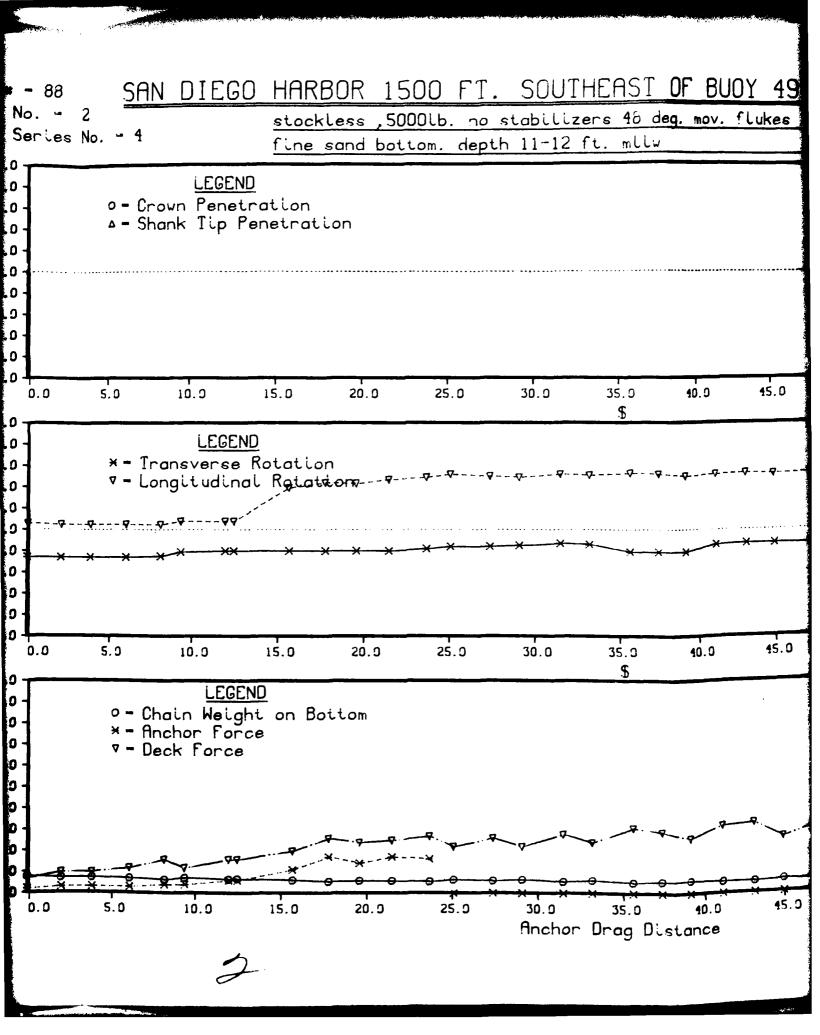
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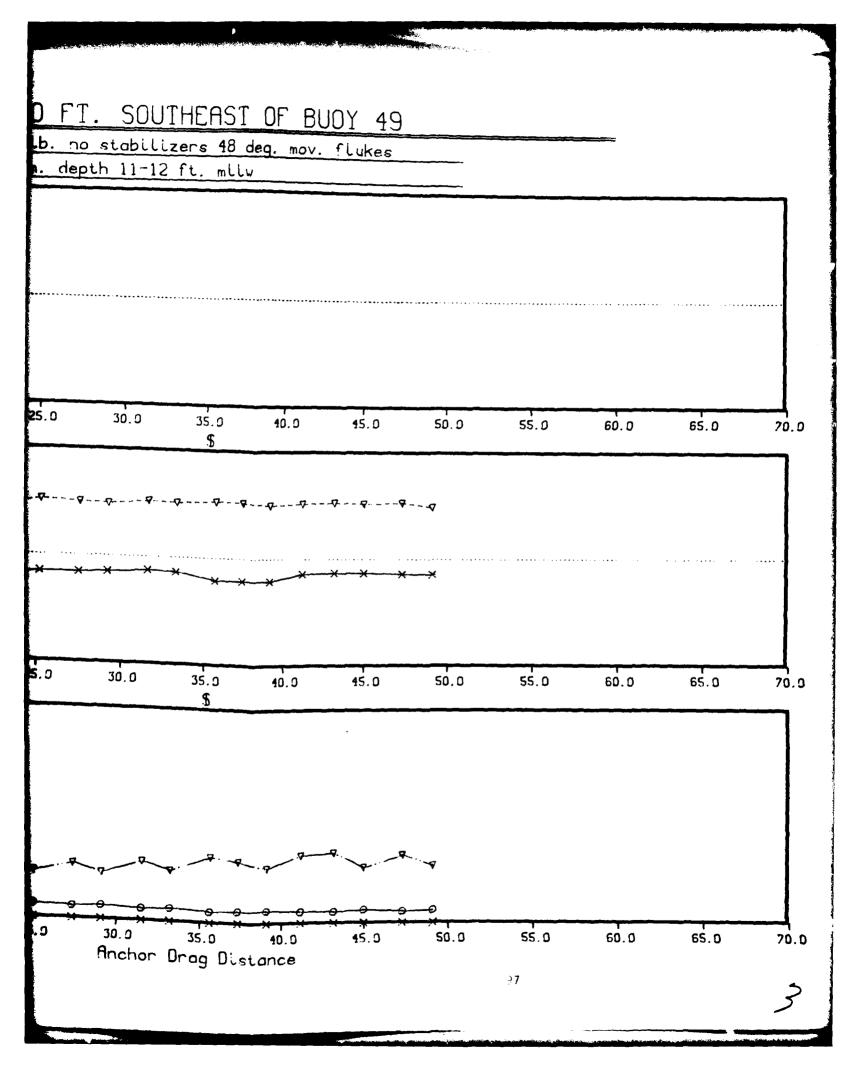
TEST DATF
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STABT-FND TIMES
STABT-FND TYPE
ANCHOR TYPE
MIT. ANCHOR WFIGHT
MAIN-AUS ANCHOR SEPARATION
DEPRESCOSS-NO.-WT.FACH-TOTAL WT.
MODRING LINE DESCRIPTION 4 CAN DIFGO MADROD ISON FT. SOUTHFAST OF BUDY 49 1526 - 1636 FTM SAND BOTTOM. DEPTH 11-12 FT. MILW STOCKLESS -SOON, B. NO STABILIZERS 48 DEG. MOV. FLUKFS 5350.00 IR. 44.00 DEG. - 0 0=MOV 1=FIX A.OO IR.

O.O FFET
O.O FFET
O.O AGET 1.1251N. DIFLOCK CHAIN TO 180FT 2.01N STHOINK CHAIN TO 600FT 21N. WIDE BODE 1. NOAG DISTANCE 5. ROTATION ANGEE 4. CHAIN LENGTH ON ROTTON 13. ANCHOR FLUKE TIP DEPTH 2. RECK TENSION 7. WIDE RODE ANGLE 11. ANCHOR PORTON PORTON 14. WATER DEPTH 4. PACKAGE OFFITH 4. DECK HORIZ, EDGE 11. ANCHOR PORTON DEPTH 15. TOTAL ROTTON WEIGHT 15. ANCHOR SHAWK TIP DEPTH 0FG -13.0 -13.0 -13.0 -13.0 -10.5 -10.5 -10.0 -10.0 -10.0 -2.0 -2.0 -7.5 -7.0 -10.5 -7.0 -7.0 9 FFF T 444.9 359.0 106.4 259.3 269.3 252.3 252.3 241.7 13 10 195 7898.3 7270.9 7270.9 74 16 (196 13/74),1 12610,0 12610,0 12620,0 12630,0 11711,4 12630,0 11401,0 11 FFFT 17 FFFT ***** **** **** **** **** 10-0 10-0 10-0 10-0 11-0 10-0 11-0 10-0 1 0EG 111-5 111-7 110-0 10-0 9-0 8-3 8-0 7-7 7-7 7-7 7-1 7-1

DISTANCE BARGE TRAVELLED DISTANCE ANCHOR TRAVELLED

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Day # - 88
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1730 - 1741
FIME SAMN ROTTOM. DEPTM |1-12 FT. MLLW
STOCKLESS "SHOOLR" NO STARILITEDS AR DEG. MOV. FLIWFS
5350.00 LR.
44.00 DEG. - 0 0=MOV 1=FIX
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                            9. CHAIN LENGTH ON MOTTOM
10. CHAIN WEIGHT ON MOTTOM
11. ANCHOR CROWN DEPTH
12. ANCHOR CHANK TIP DEPTH
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POSTTIVE SHANK ANGLE INDICATES SHANK TIP BELOW CROWN

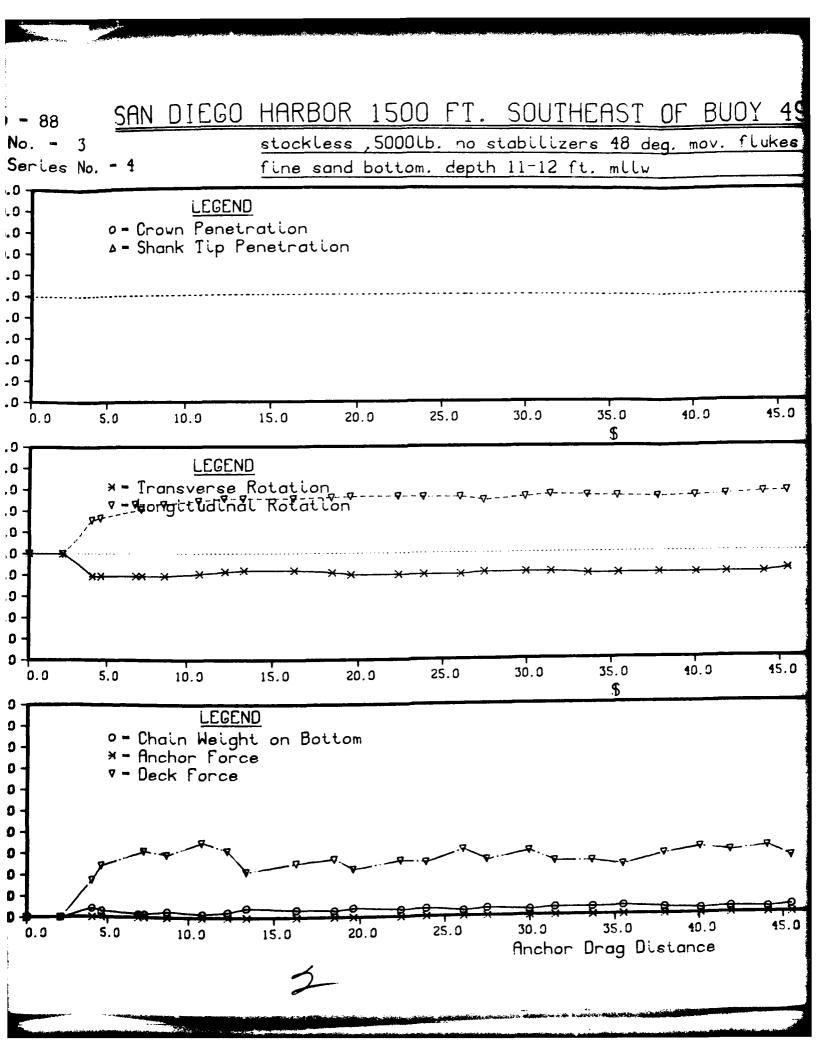
TEST DATE

TEST OATE
TEST MINTEST TEST SENTEST SENSTART-END TIMES
SEAFLOR TYPE
ANCHOR TYPE
ANCHOR WEIGHT
FLIKE ANGE-TYPE.
AUX. ANCHOR TYPE
AUX. ANCHOR SEDARATION
DEPRESSOS-NO.-UT.FACM-TOTAL UT.
MODRING LINE DESCRIPTION

1. DPAG DISTANCE 2. DECK TENSION 3. ANCHOR TENSION 4. PACKAGE DEPTH

K JBS

S. ROTATION ANGLE
A. SMANK ANGLE
7. WIRE ROPE ANGLE
8. DECK MORIT, FORCE



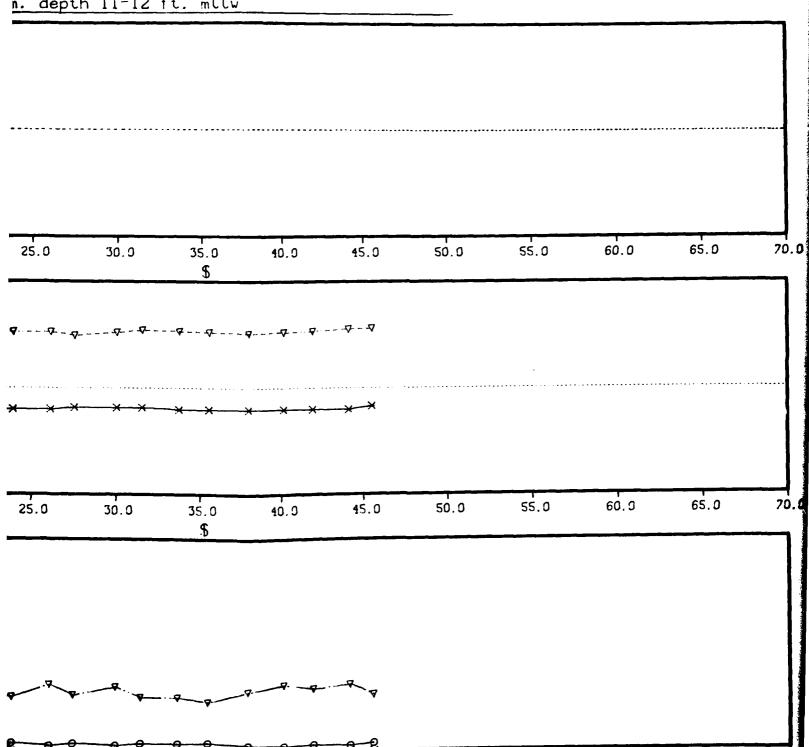
FT. SOUTHEAST OF BUDY 49

Lb. no stabilizers 48 deg. mov. flukes

35.0 Anchor Drag Distance

n. depth 11-12 ft. mllw

25.0



55.0

99

50.0

45.0

60.0

65.0

Day # - 89 Test No. -STOCKLESS ANCHOR TEST T S CAN DIFFO MADROD ISON FT. SOUTHFAST OF RUNY 49 1103 - 1109 FINE SAND ROTTON, DEPTH 11-12 FT. MILW STOCKLESS SOUNDER, STABILITESS-ADDIA, 700, 35 DEG. FT. FLUKE 5950,00 IA. 35.00 DEG. - 1 0=MOV 1=F11 O.O IA. O.O FFFT O.O FFFT O.O FFFT O.O CA. O.O CA. ALCHOD TO GOET 1.125IN. DIFLOCK CHAIN TO LAPET 2.019 STHOITHK CHAIN TO GOOFT NOTE - INITIAL CHANK REDTH ZERGED TO DEFLECT MEASURED WATERDEPTH 14 FFFT 16.0 16.0 16.0 16.0 16.0 0.0 2045.9

A Q FET 12.1 200.2 15.0 175.1 21.9 175.3 21.9 175.3 21.9 175.5 21.9 175.1 21.9 175.1 21.9 175.1 21.9 175.7 2.0 175.7

TEST DATE
TEST NO.
TEST SEPICA

4. PALREUT DEPTH N. DECK MORIT., 190CF 12

FFFT KIPS KIPS FFET OF DEF DEG

0.0 13.0 3.0 14.1 1.5 -3.0 21.6

2.0 18.0 4.0 16.4 0.0 3.0 20.4

4.0 25.0 14.0 16.4 0.0 3.0 20.4

6.0 74.0 22.0 17.0 5 10.0 16.2

MOTE- ALI PULL LIME AND CHAIN IS OFF ROTTOM AT 12.0

MOTE- ALL PULL LIME AND CHAIN IS OFF ROTTOM AT 12.0 54.0 28.0 17.5 5 9.0 11.0

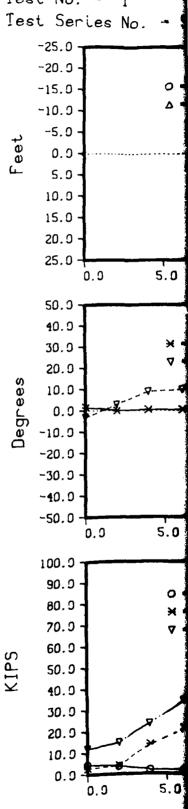
MOTE- ALL PULL LIME AND CHAIN IS OFF ROTTOM AT 12.0 56.0 35.0 17.2 15 9.4 12.5

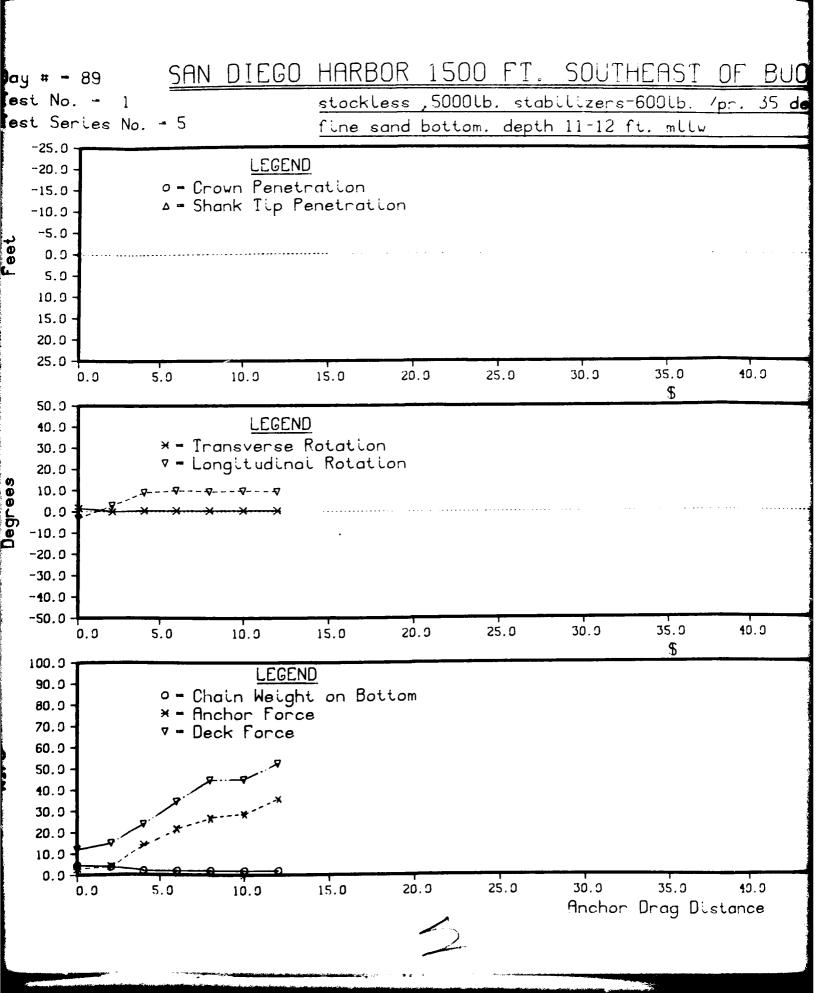
MOTE- ALL PULL LIME AND CHAIN IS OFF ROTTOM AT 12.0 56.0 35.0 17.2 5 9.4 12.5

DISTANCE MARGE TRAVELLED 17.0 DISTANCE ANCHOR TRAVELLED -4.2

MOTE - DOSTITIVE SHANK ANGE INDICATES SHANN TIP RELOW FROMN

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SOUTHEAST OF BUOY 49 stabilizens-600lb. /pr. 35 deg. fx. fluke depth 11-12 ft. mllw **2**5.0 30.0 35.0 40.0 50.0 55.0 45.0 60.0 65.0 70.0 \$ 30.0 50.0 25.0 35.0 45.0 55.0 65.0 40.0 60.0 70.0 \$ **2**5.0 30.0 55.0 65.0 45.0 50.0 60.0 70.0 35.0 40.0 Anchor Drag Distance

101

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Day # - 89
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 TEST DATE

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TEST APE

START-FNO TIMES

SEAFLOND TYPE

ANCHOR TYPE

ANCHOR TYPE

ALIE ANCHOR SEPARATION

OFDEDESCOS, NO. - MILE ACHITOTAL WI.

MONDING LINF DESCRIPTION
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CAN DIFFOR HAPPOD ISON FT, SOUTHFAST OF SUMY 49

1468 - ISON
FINE SAND ROTTON, OFFTH 11-12 FT, MILW
STOCKLESS "SOMOLA" START 17FPS-MODIA, 7PP, NS DEG. FT, FLUKE
SSOO,ON IR.
15.00 OFFG. - 1 = nemov 1self
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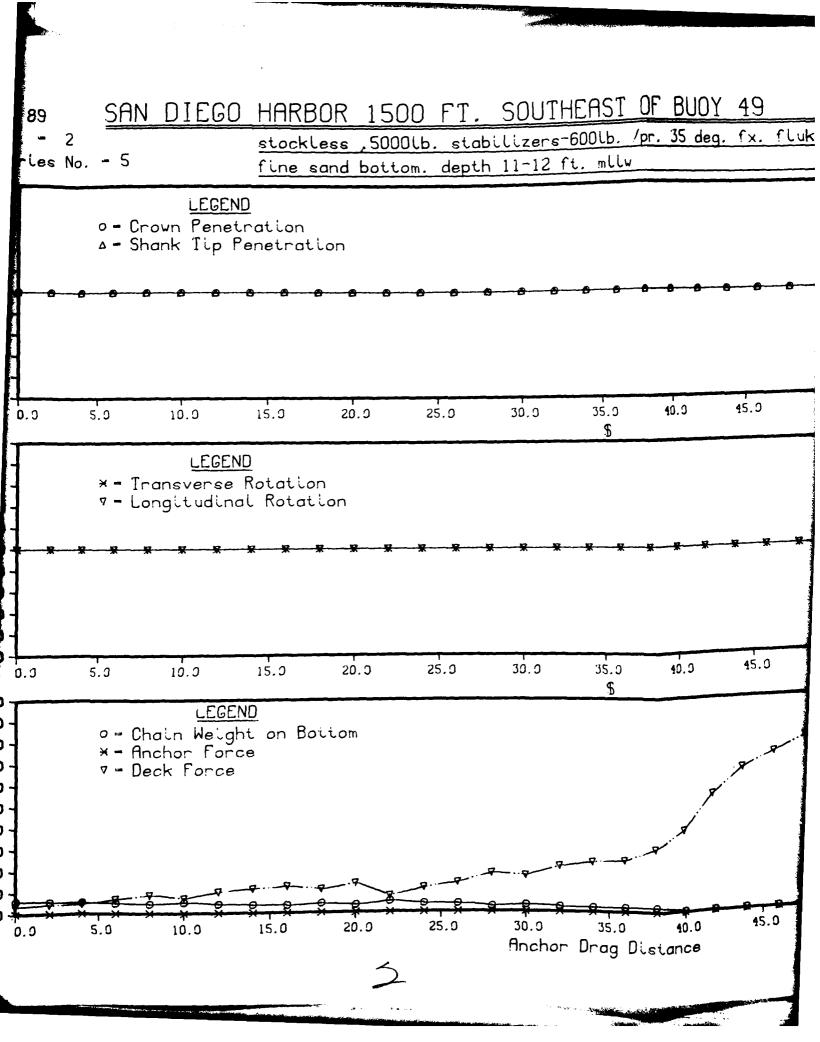
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    DISTANCE MARGE TRAVELLED DISTANCE ANCHOR TRAVELLED
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          100.0
       - OTE - DOCTITIVE CHAIN
AND E THOSENTE
CHANN TID RELOY
COOK!
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500 FT. SOUTHEAST OF BUOY 49 00lb. stabilizers-600lb./pr. 35 deg. fx. fluke tom. depth 11-12 ft. mllw 25.0 30.0 35.0 45.0 40.0 50.0 55.0 60.0 65.0 7Ò.0 25.0 30.0 35.0 45.0 55.0 40.0 50.0 60.0 65.0 70.0 25.0 30.0 50.0 60.0 70.0 45.0 55.0 65.0 35.0 40.0 Anchor Drag Distance 103

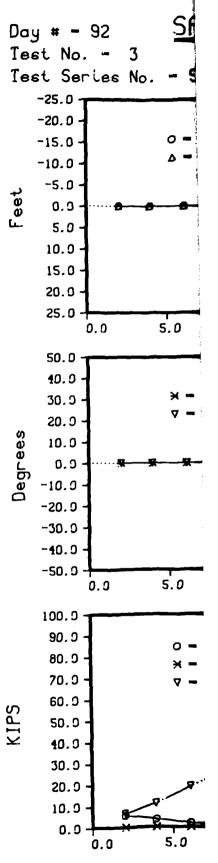
NOTE - INITIAL CHANK OFFTH TERRED TO DEFLECT MEAGINED MATERIEFTH

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1. NOAK DISTANCE S. BOTATION ANCHE 9. PHAN LENGTH ON BOTTOM 1. ANCHOR FLUKE TID DEPTH 2. ANCHOR TENCION 7. WISE DOBS ANCHE 11. ANCHOR CODWN DEPTH 15. TOTAL ROTTOM WEIGHT ON WHITTOM 14. WEETS OFFIT PARTY A. PARTY ANCHOR TENCION 7. WISE DOBS ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM WEIGHT 1. ANCHOR CHAMM TID DEPTH 15. TOTAL ROTTOM TID D
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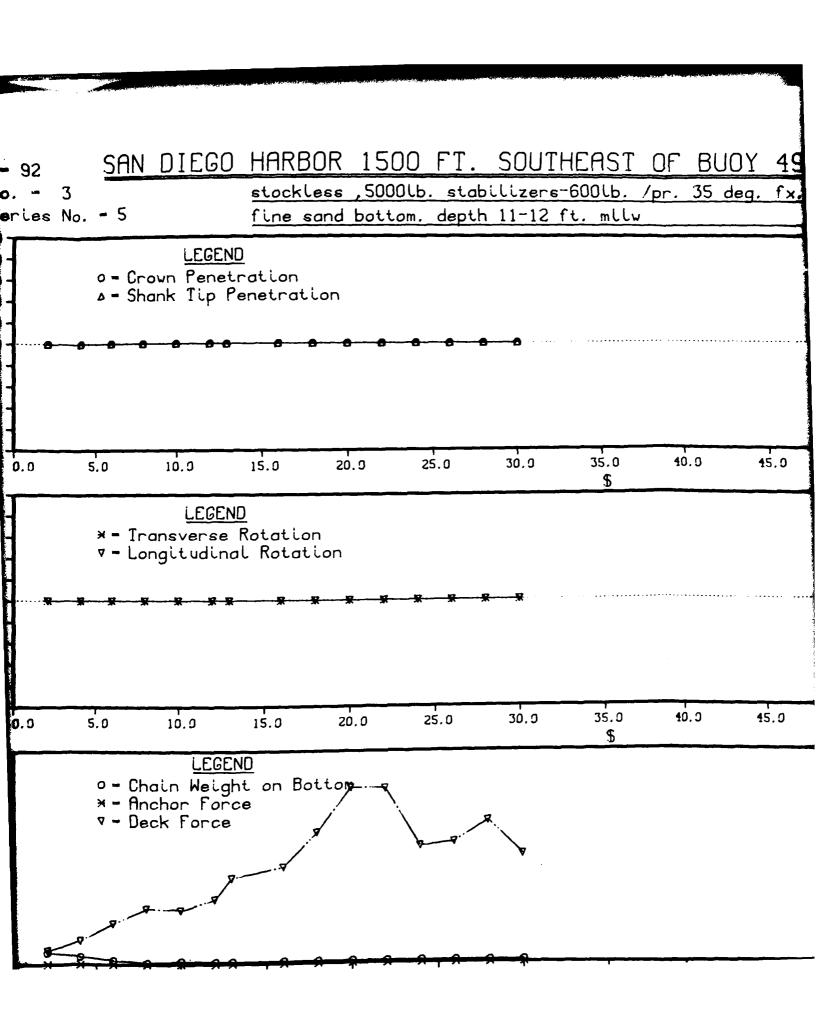
DISTANCE MARGE TRAVELLED 29.0 DISTANCE ANCHOW TRAVELLED 10.4

Note Anchor depth at end of drag measured — centerline of shank at anchor crown = 34 inches.

NOTE - DOSTTIVE SHANK ANGLE INDICATES SHANK TID RELOW CODYN

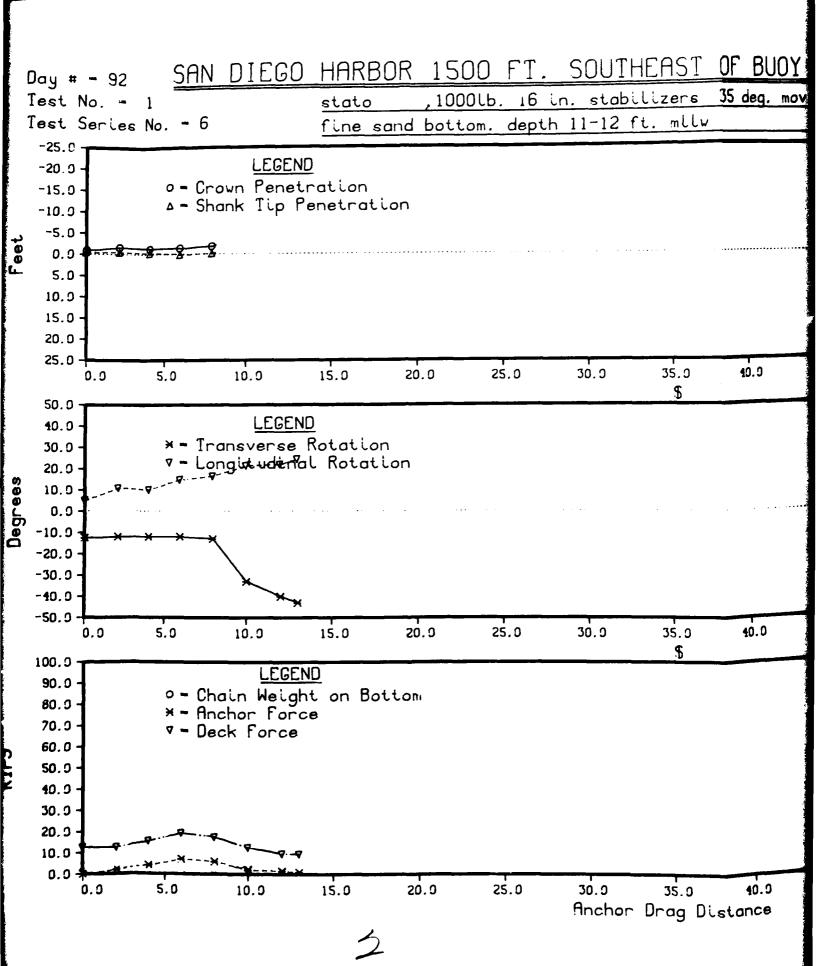


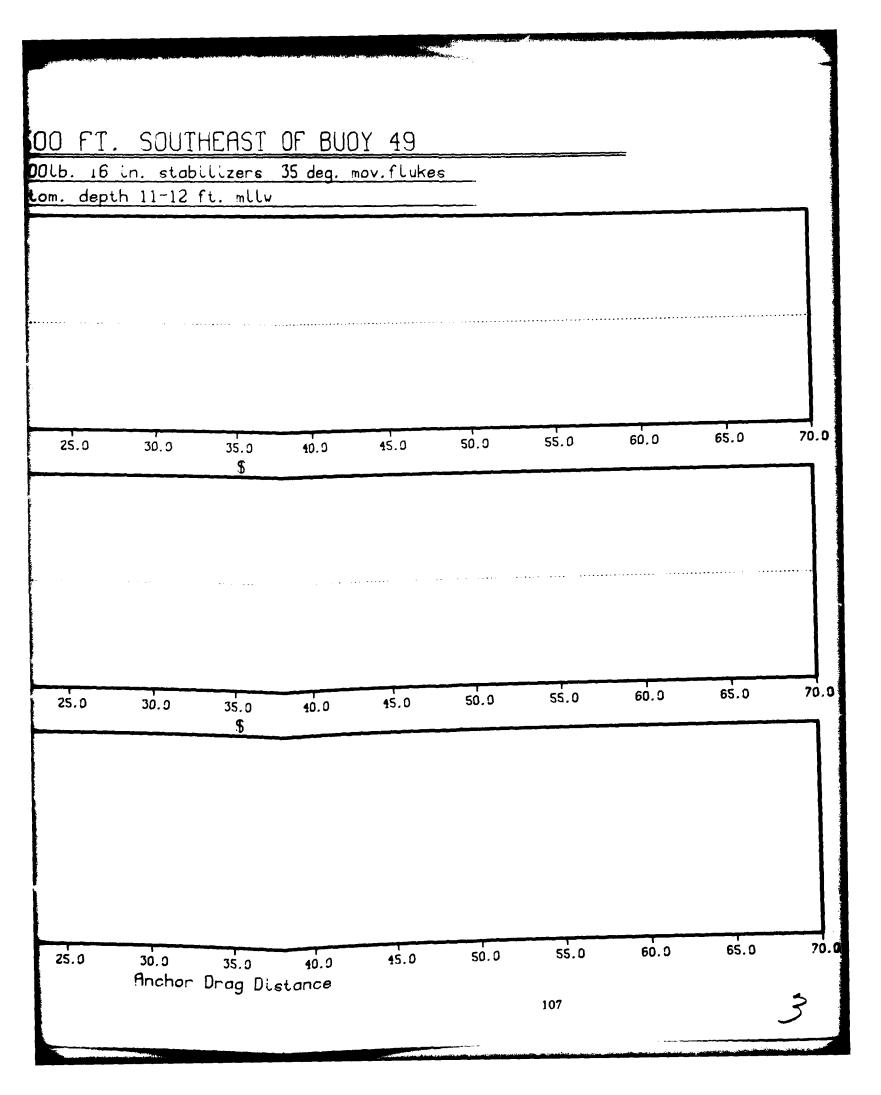
The state of the s



FT. SOUTHEAST OF BUOY 49 stabilizers-600lb. /pr. 35 deg. fx. fluke depth 11-12 ft. mllw 35.0 40.0 45.0 30.0 **2**5.0 50.0 55.0 60.0 65.0 70.0 \$ **2**5.0 35.0 40.0 45.0 50.0 55.0 30.0 60.0 65.0 70.0 **25**.0 45.0 50.0 55.0 60.0 65.0 30.0 35.0 40.0 70.0 Anchor Drag Distance 105

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Day # - 92
                                                                                                                                                                                                                                       Test No. -
                                                                                                                                                                                                                                       Test Series No.
                                                                                                                                                                                                                                             -25.0
TEST DATE
TEST MO-
TEST SEGIES
THES
STAPLONG TYPE
ANCHOP TYPE
AUX. ANCHOP MIGHT
MAIN-AUX ANCHOP SEPARATION
DEMPRESSION.-WILEACH-TOTAL WT.
MODRING LIME DESCRIPTION
                                                                                                                                                                                                                                             -20.0
                                                                         1 6 CAN DIEGO MARROD 1500 FT. SOUTHFAST OF RHOY 49 1056 - 1244 FIME SANN BOTTOM. DEPTH 11-12 FT. MLLW CTATO - 1000(R. 16 IN. STARILIZERS 35 DEG. MOV.FIJMES 1070.00 LR. 35.00 DEG. - 0 0=MOV 1=FIT
                                                                                                                                                                                                                                                                                               0 -
                                                                                                                                                                                                                                             -15.0
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O- O-O EFFT
O- O-O ER-
NNCHOR TO JARET 21N. WIRF ROPF
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                                         NOTE - INITIAL CHANK DEPTH ZEROFO TO REFLECT MEASURED WATERDEPTH
                                                                                                                                                                                                                                                10.9
                                                                                                                                                                                                                                                15.0
                                          S. POTATION ANGLE
6. SHAMK ANGLE
10. CHAIN WEIGHT ON ROTTOM
7. WISE POSE ANGLE
11. ANCHOP CROWN DEPTH
8. DECK HOPIZ, FROCE 12. ANCHOP SHAWK TIP DEPTH
                                                                                                                                                                                                                                                20.0
                                               0FG
-12.5
-17.6
-17.0
-12.0
-13.0
-40.0
-43.0
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FEET
118.5
111.0
77.3
45.2
77.3
124.8
153.4
141.3
                        3
KIPS
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2.0
4.0
7.0
6.0
2.0
1.5
                                                              6
DEG
5.0
10.0
14.0
16.5
21.5
27.0
24.6
                                                                                       # IPS
17.6
12.5
15.4
19.3
17.5
12.6
9.7
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                                     FEET
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15.8
16.1
15.8
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15.4
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DISTANCE NARGE TRAVELLED
DISTANCE ANCHOR TRAVELLED
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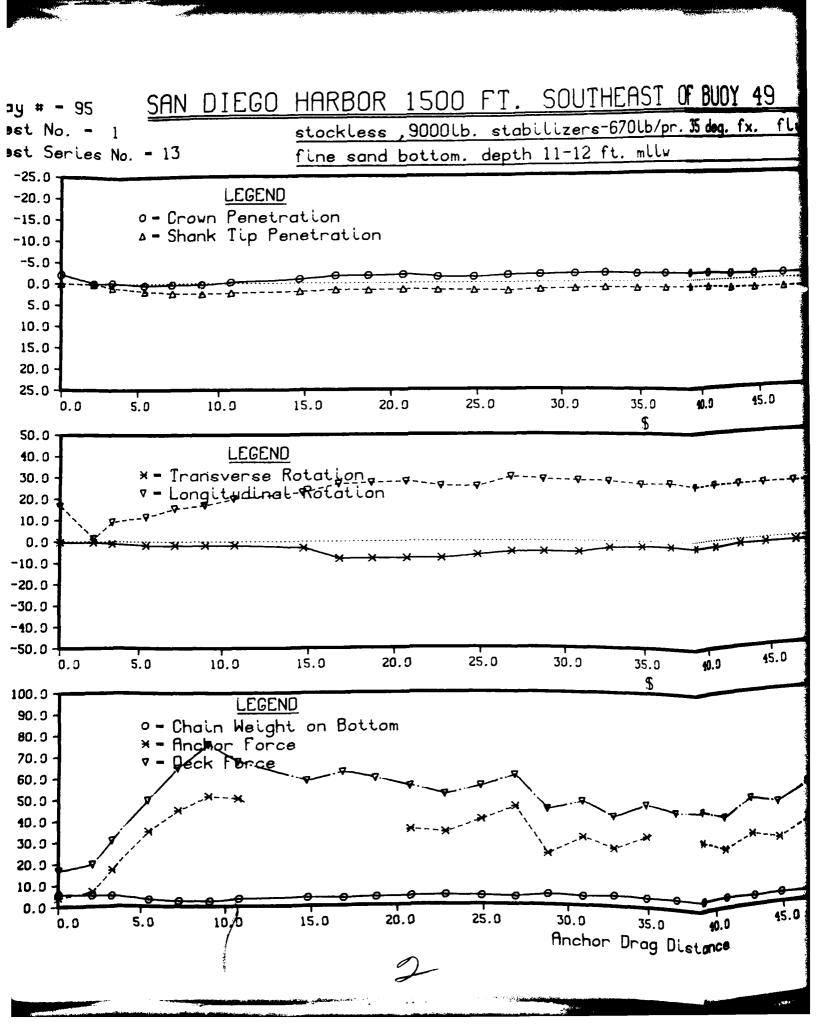


SAN Day # - 95 Test No. -Test Series No. 13 -25.0 STOCKLESS ANCHOR TEST TEST DAIF TEST WM. TEST SERIES TEST ABEA STADT-FNO TIMES SEAFLONG TYPE ANCHOD TYPE ANCHOD TYPE ANCHOD FIGHT FLIME ANGLE-TYPE, ANTA ANCHOD WFIGHT MAIN.AIX ANCHOD WFIGHT MONDING LINE DESCRIPTION -20.0 Cri -15.0 13 CAN DIEGO MARROR 1500 FT. SOUTHFAST OF RIMY 49 1514 - 1832 FINE SAND BOTTOW, DEPTH 11-12 FT. MILW STOCKLESS "GOOD B. STARI 17EPS-670[8/PR. 15 DEG. FT. FLIWES 11370.00 [8. 35.00 DEG. - 1 0=MOV 1=FIX Sh -10.0 -5.0 eet 0.00 IR. 0.0 FFFT 0.0 0.0 PPFT 0. 0.0 - 0.0 LB. NCHOR TO LARFT PIN. STUDLINK CHAIN TO GROFT PIN. WIDE DOPF 5.0 NOTE - INITIAL CHANK DEDTH PEODED TO DEFLECT MEASURED WATEODEDTH 10.9 15.0 1. MORG DIS:. 2. DECK TENTS 3. RECHOR TENTSON 4. PROKROE DEPTH S. ROTATION ANGLE A. SMANK ANGLE 7. WIPE POPE ANGLE 9. DECK HOPIZ, FOO GF 9. CHAÎN YEINGTH ON POITON 13. ANCHOD FILME TIP OFFITH 10. CHAÎN YEIGHT ON ROTTON 14. MATED OFFITH 15. TOTAL BOTTOM WEIGHT FORCE 12. ANCHOD CHÂNK TIP OFFITH 20.0 5 C . 3 - 11.8 C . 11 10 5472.2 5715.4 5765.2 3754.6 2441.0 7466.4 3777.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 4097.7 25.0 15 10c 17nn2,2 167nc,4 16401,2 16601,2 1301,6 1501x,6 15467,7 1504,1 15167,7 1504,1 15167, 0.0 5.0 50.0 40.0 35.5 34.0 40.0 46.0 24.0 32.0 27.0 33.0 30.0 20.0 Degrees 10.0 31.5 7.0 23.0 30.0 36.0 37.0 33.6 0.0 -10.0 -20.0 DISTANCE MARGE TRAVELLED BISTANCE ANCHOR TRAVELLED -30.0 -40.0 HATE - DASTITUE SHAW ANGLE THATCATES SHAWE TID RELAW CROWN -50.0 5.0 0.0 100.0 90.0 80.0 70.9 60.0 50.0 40.0 30.9 20.0 10.0

0.0

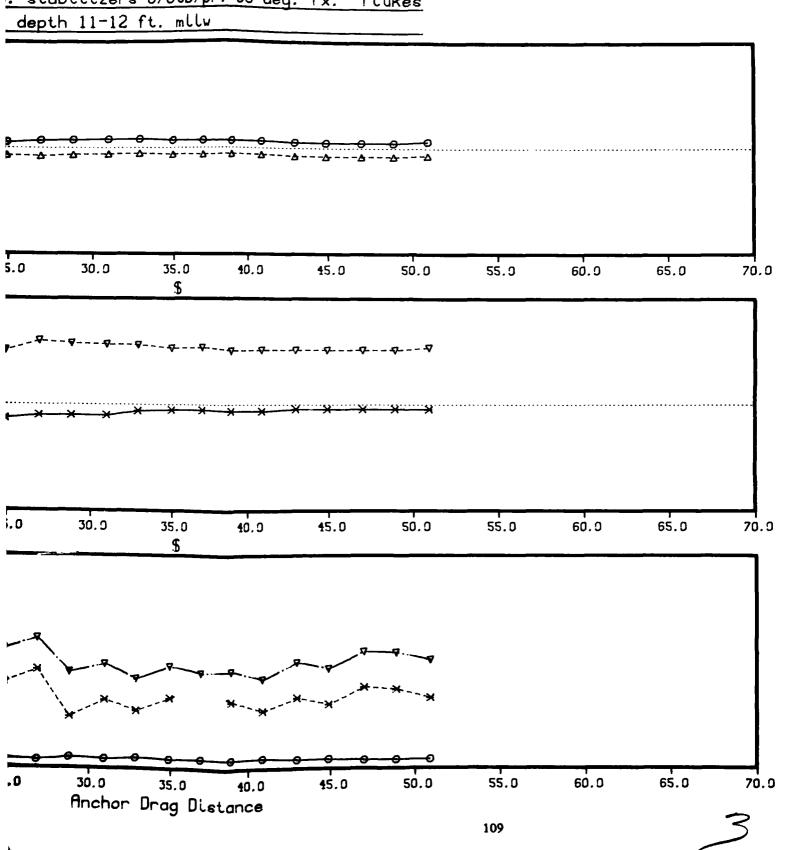
0.0

5.0



FT. SOUTHEAST OF BUOY 49

. stabilizers-670lb/pr. 35 deg. fx. flukes depth 11-12 ft. mllw



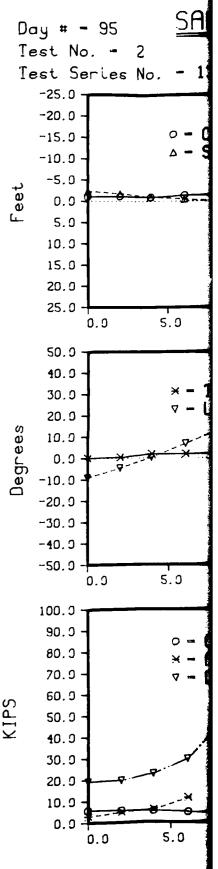
STOCKLESS ANCHOR TEST

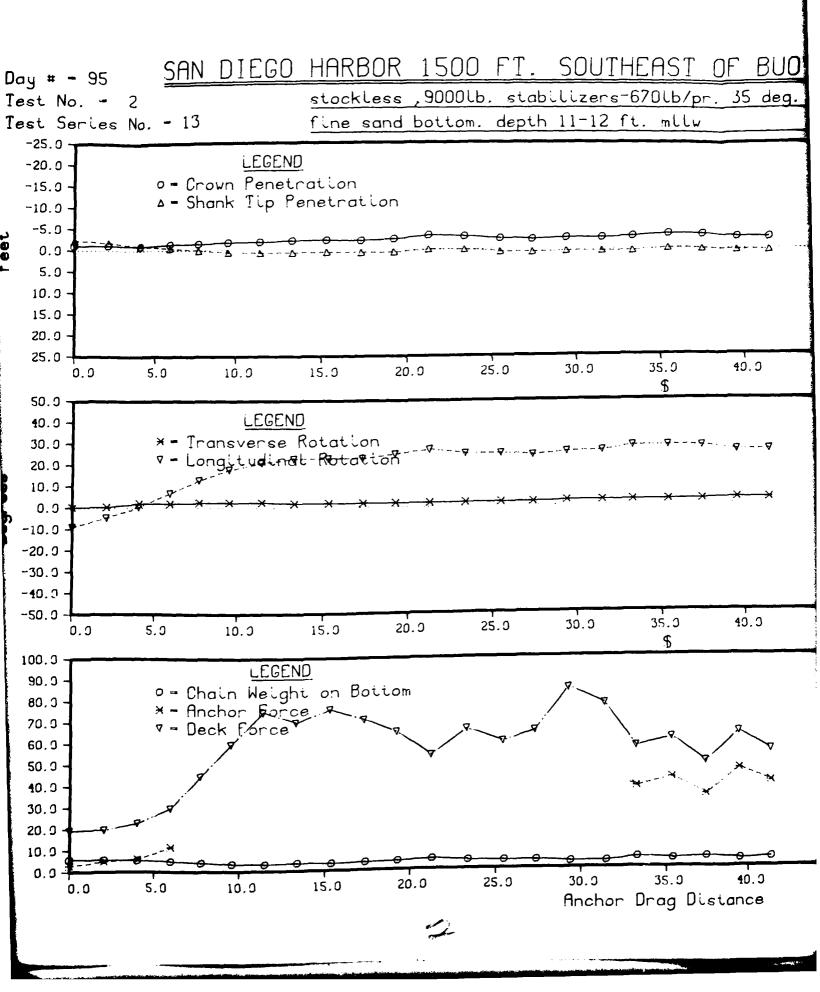
NOTE - INITIAL CHANK DEPTH PEDDED TO DEFLECT MEASURED METERDEPTH

	1. 3040	TISTANO	F 5.	ROTATIO	ON ANCIE	٠ ٩,	CHAIN	(EWILLIN	Un EULLUM		-OU FILLE	110	P 1	
	2. OFCE			CHANK .	ANG F	10.	CHATN	wF I GHT	ON BOTTOM	14. #47	FO DFDTH			
	7. 6-CH			WIPF P	DOF ANG		ANCHOR	COOPN	REPTH	IS. TOT	AL BOTTOM	WEIGHT		
	4. 04CH			DECK H		DOCE 12.	ANCHO	CHANK	TIP OFFTH					
	4. Date	406 1166		171 (14 71	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,									
,	,	,	4	•	Α.	7	R	9	10	11	12	13	14	15
FFFT	¥105	K 105	FFET	Df G	DFG	OFG	-105	FFFT	1 25	FFFT	FFFT	FFFT	FFFT	160
0.1		3.0	11.0	. 6	-9.2	7.3	19.3	193.5	5017.0	14.6	13.5	16.0	15.4	17147.4
		5.0	14.1		-4.5	7.3	19.8	183.5	5750.1	14.5	13.9	17.0	35.8	17120.7
2.0			14.4	2.0		7.0	22.A	172.5	SAAR.A	14.7	14.9	17.4	15.0	14868.4
4.0		6.0		5.0	7.0	6.4	29. B	155.5	4047.5	14.3	15.2	17.7	15.8	16717.5
6.0		11.5	15.0		13.0	5.2	44.9	132.4	4213.1	14.3	15.9	19.7	15.0	15507.1
7.A			15.5	2.5			59.A	112.6	7584.1	14.0	16.2	18.0	15.0	14954.1
٩.٨			15.7	2.5	18.0	4.5	74.8	100.3	1190.5	13.0	16.4	10.0	15.0	14560.5
11.5			16.8	7.5	21.1	3.9			1774.3		16.4	7.9	15.	15144.7
13.4	70.0		15.7	2.0	23.4	3.7	49.9	118.6		13.6		17.7	15.9	14757.1
15.4	74.0		15.4	2.n	23.0	3.7	75.A	106.4	3347.1	13.5	16.3			15207.5
17.4	71.0		15.7	2.0	23.0	3.5	70.9	120.5	7873.5	13.6	16.4	17.R	15.9	
19.1			15.5	2.0	25.0	3.6	£4.0	132.3	4210-2	13.2	16.2	17.5	15.9	15580.2
21.3			14.9	2.0	27.0	3.6	53.9	154.0	4900.9	12.3	15.4	16.7	15.4	14270.9
27.4			15.4	2.0	25.1	3.7	45.9	126.7	4077.5	12.7	15.4	17.0	15.4	15402.5
25.5			15.5	2.0	25.0	4.2	59.A	122.5	3897.3	13.2	16.7	17.5	15.4	15747.7
27.4			15.4	2.0	24.0	3.9	64.B	121.6	2870.A	13.4	16.3	17.7	15.4	15740.6
			15.4	7.5	25.5	3.6	84.A	92.A	2954.4	13.0	16.7	17.4	₹5. Q	14774.4
29.4			15.4	2.5	25.0	3.8	77.3	99.7	7155.4	13.0	16.2	17.4	15.9	14525.4
31.5		30.0	15.3	2.5	24.4	3.5	56.9	151.2	4411.4	12.7	16.1	17.2	15.4	14181.8
33.3		34.0			28.0	4.0	40.9	126.9	4036.5	12.1	15.5	16.6	15.0	15404.5
35.4		42.0	14.7	2.5			49.4	152.1	4838.7	12.3	15.6	16.7	15.A	16208.7
37.4		34.0	14.4	2.5	27.5	4.0			3751.5		16.0	17.2	15.4	15121.5
39.5		46.0	15.2	3.0	25.5	4 - 1	43.3	117.9		12.A			15.4	15729.2
41.4	55.0	40.0	15.7	٥.٠	25,4	4.1	54.9	137.0	4359.2	12.9	16.1	17.1	1-7-	14,540

DISTANCE MARGE TRAVELLED 42.0 DISTANCE ANCHOR TRAVELLED 41.4

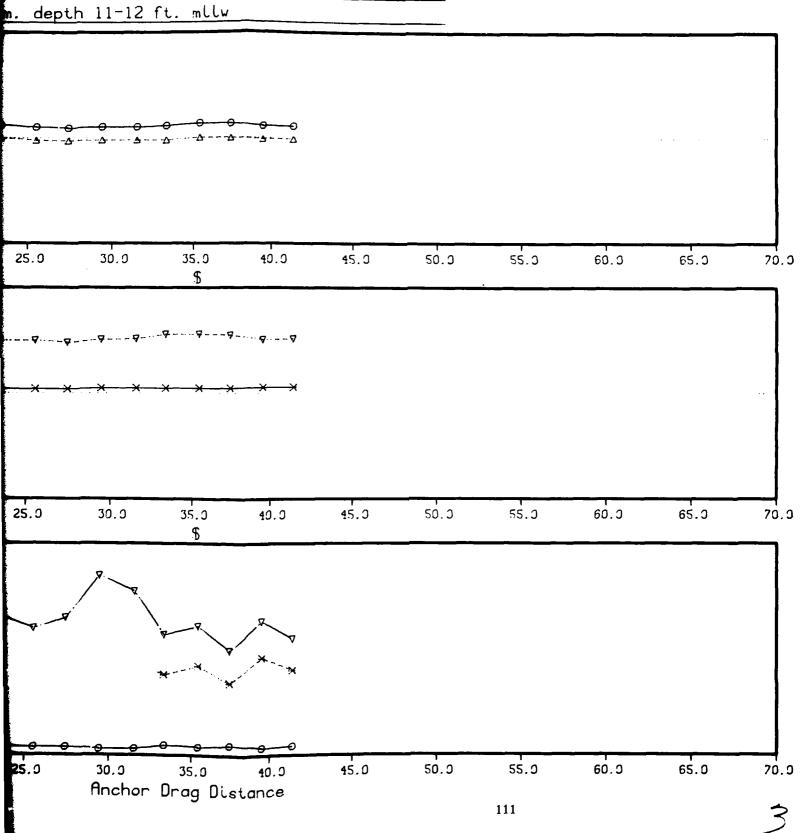
NOTE - DOCTTIVE CHANK ANGLE THOTCATEC CHANK TID RELOW COMM





D FT. SOUTHEAST OF BUOY 49

lb. stabilizers-670lb/pr. 35 deg. fx. flukes



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Day # - 95
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                Test No. - 1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                Test Series No.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            14
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              -25.0
                                                                                                                                                                                                                                                                 ANCHOR TEST
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              ~20.0
 Crd
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              ~15.0
                                                                                                                                                                                       14
CAN DIEGO HARROR 1500 FT. SOUTHFAST OF RIDY 49
1337 - 1350
FINE SAND BOTTON. DEPTH ||-|2 FT. MILW
CTATO 1300018+ 37 DFG. MOV. FLUKES
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 Shd
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              ~10.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      -5.0
                                                                                                                                                                                       O.OO IR.

O.O FFFT
O.O - O.O LR.
ANCHOR TO LARGE ZIN. STUDLINK CHAIN TO 400FT ZIN. WIRF ROPF
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            0.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            5.0
                                                                                                        NOTE - INITIAL SHANK DEPTH ZEPOED TO PEFLECT MEASURED WATERDEPTH
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      10.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      15.0
                      1. DRAG DISTANCE
2. DECK TENSION
3. ANCHOR TENSION
4. PACKAGE DEPTH
                                                                                                    5. ROTATION ANGLE 9. CHAIN LENGTH ON ROTTOM
6. SMANK ANGLE 10. CHAIN WEIGHT ON ROTTOM
7. WIDE ROPE ANGLE 11. ANCHOR CHANK TIP DEPTH
8. DECK HORIZ. FORCE 12. ANCHOR CHANK TIP DEPTH
                                                                                                                                                                                                                                                                                                                               13. ANCHOR FLUKE TIP OFFIH
14. WATER DERTH
15. TOTAL BOTTOM WEIGHT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      20.0
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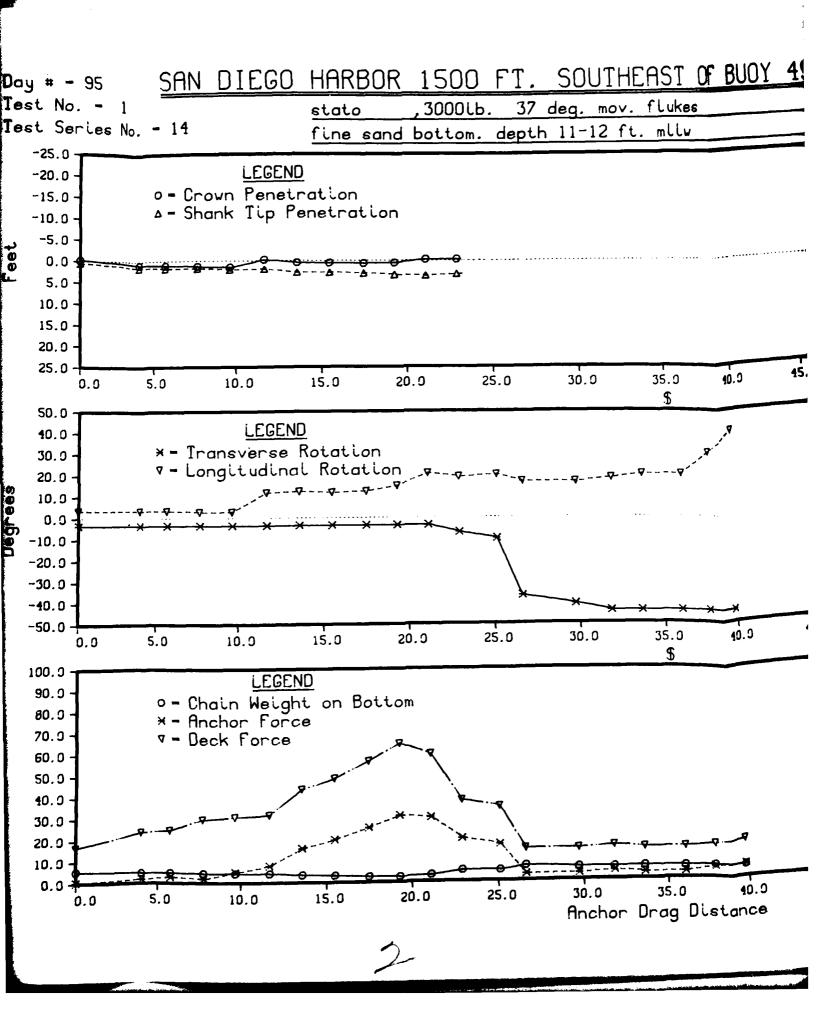
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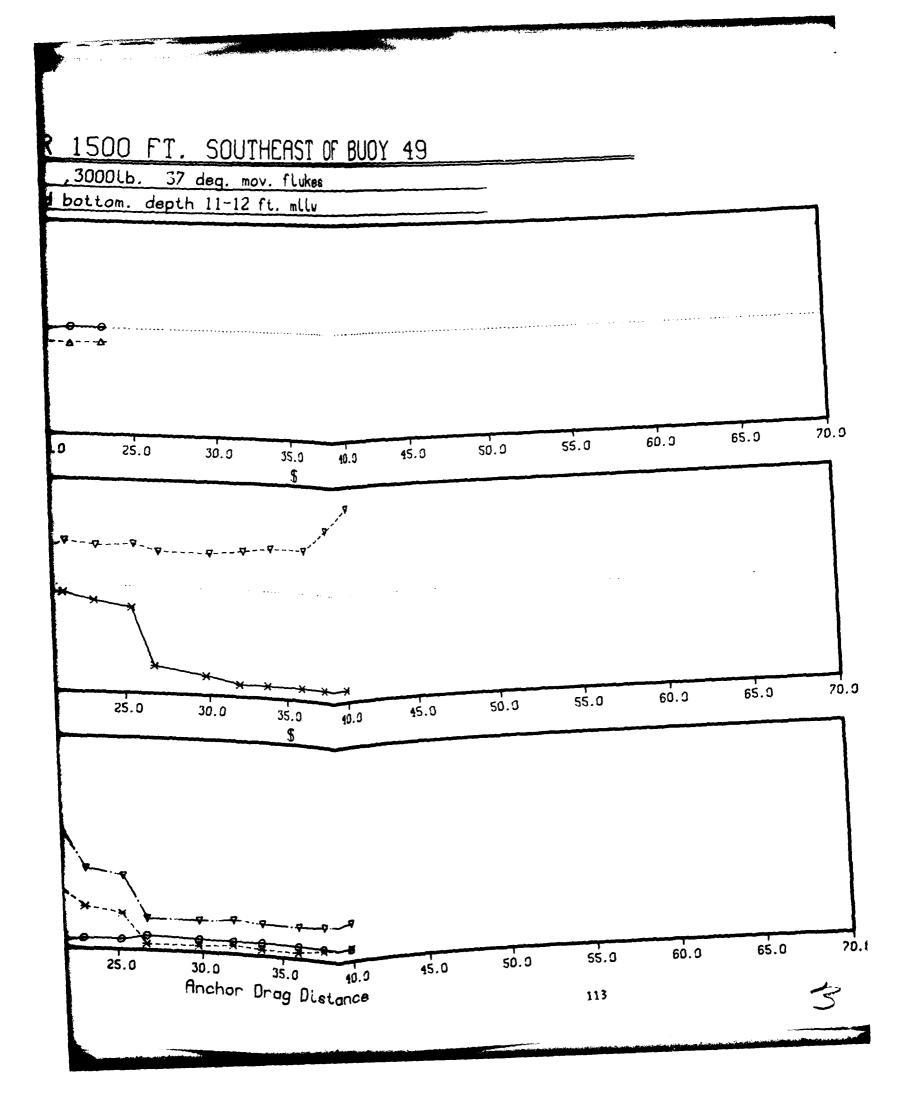
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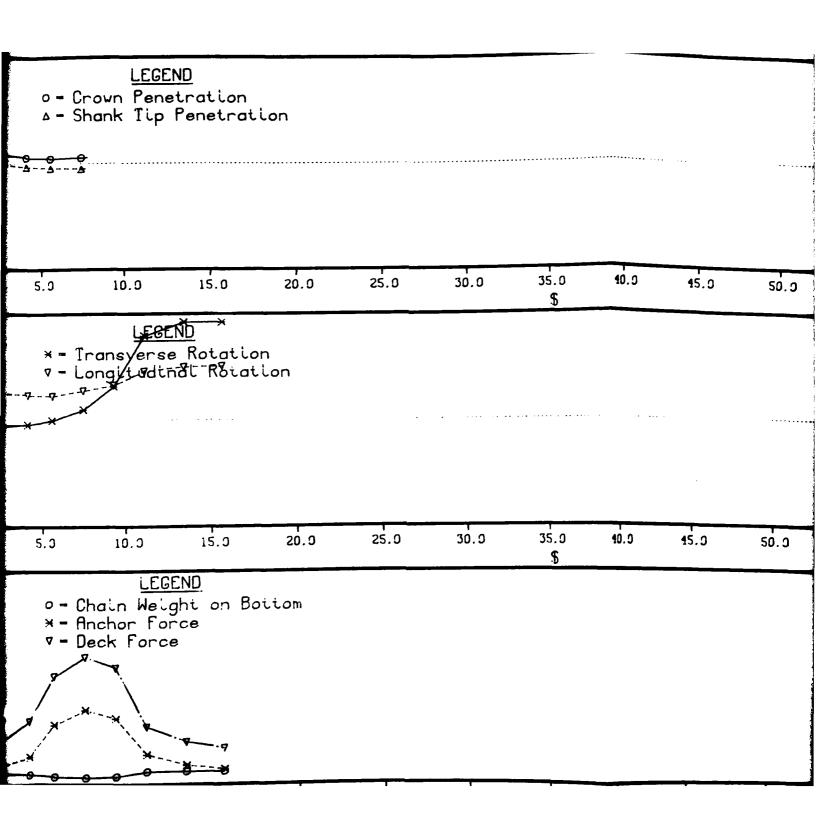
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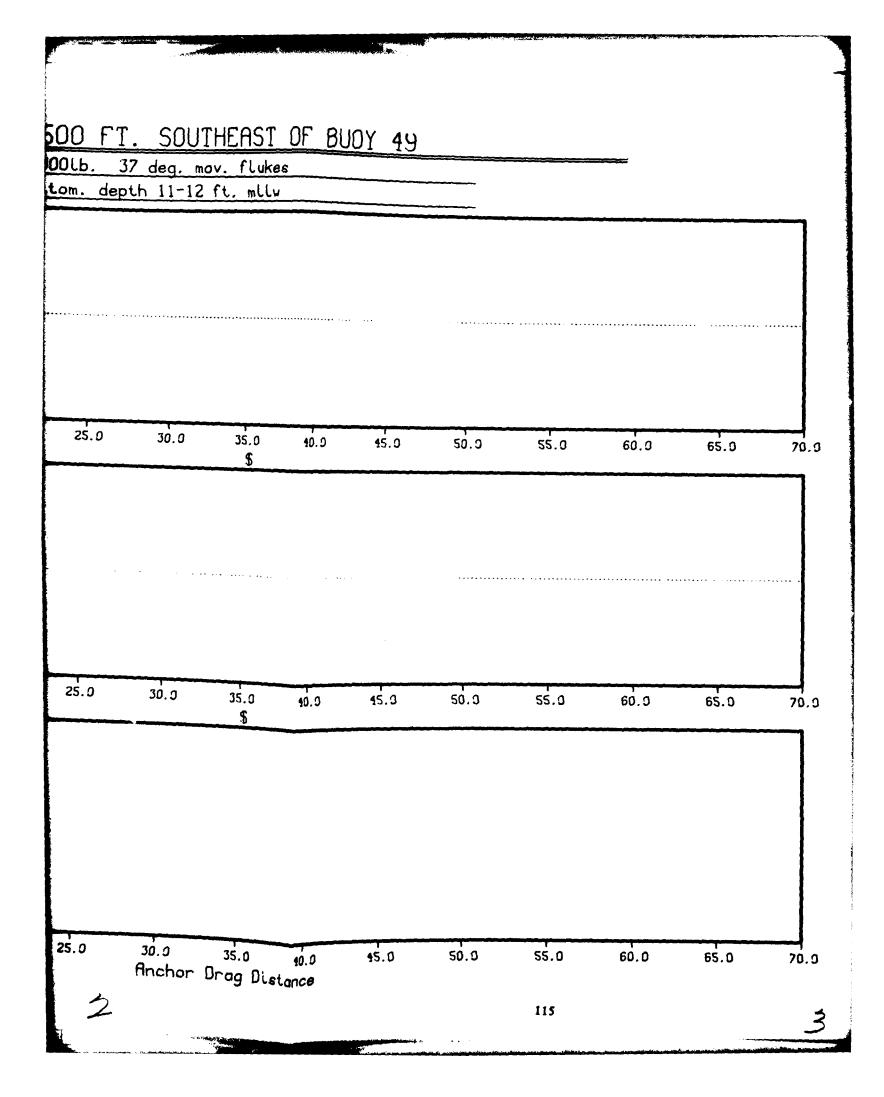




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Day # - 99
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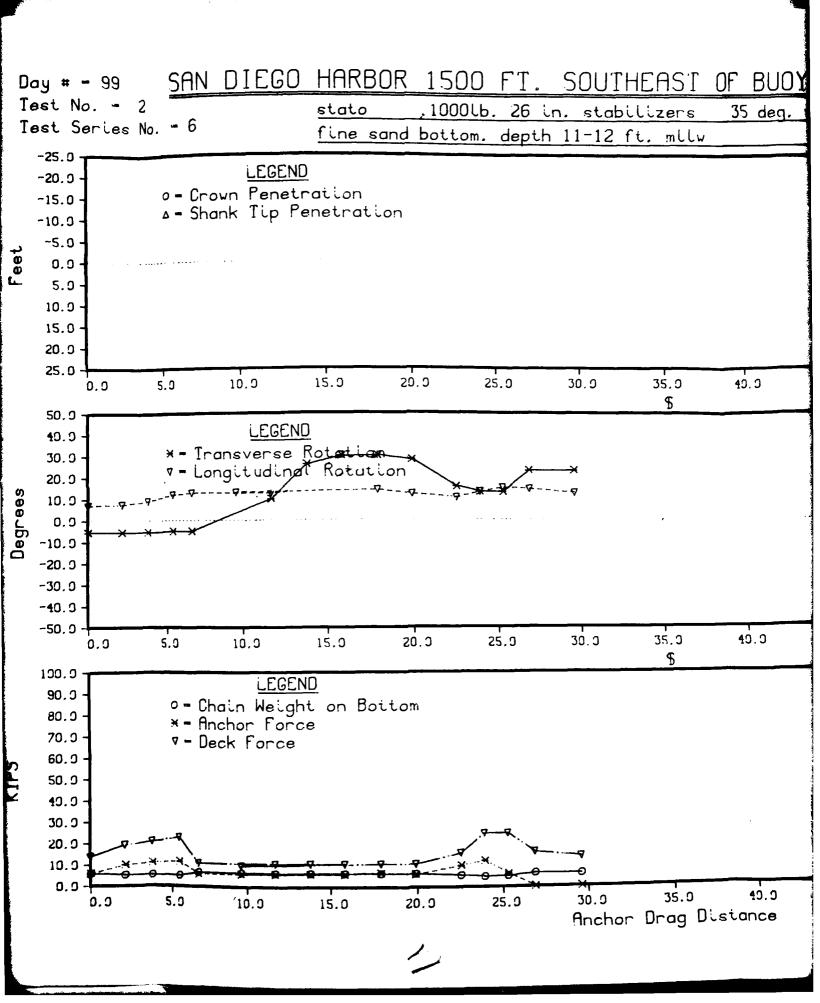
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7. WIPE DOPE ANGLE
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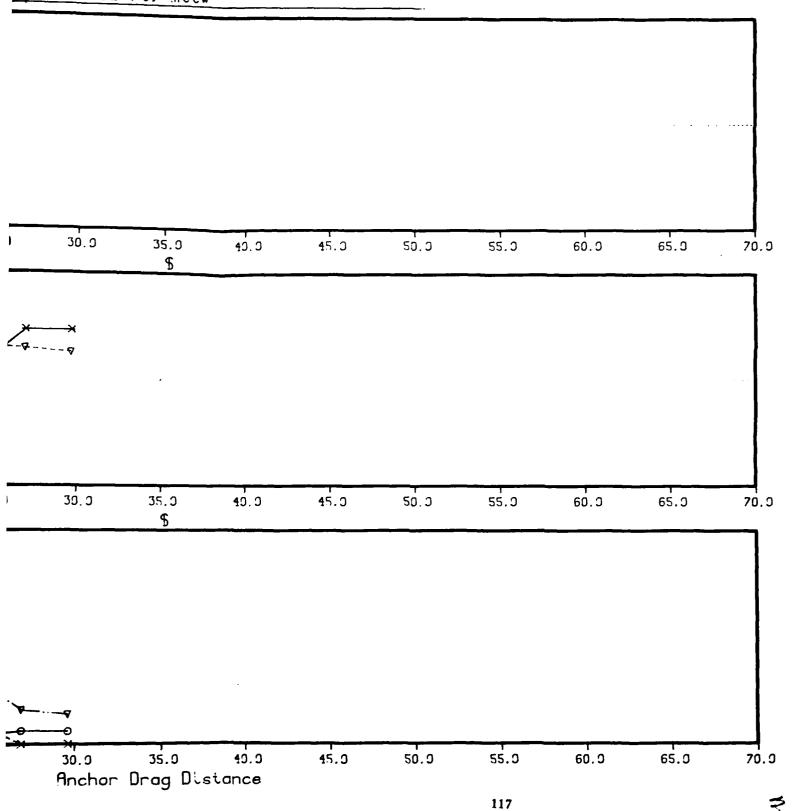
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T. SOUTHEAST OF BUOY 49

26 in. stabilizers 35 deg. mov. flukes lepth 11-12 ft. mllw



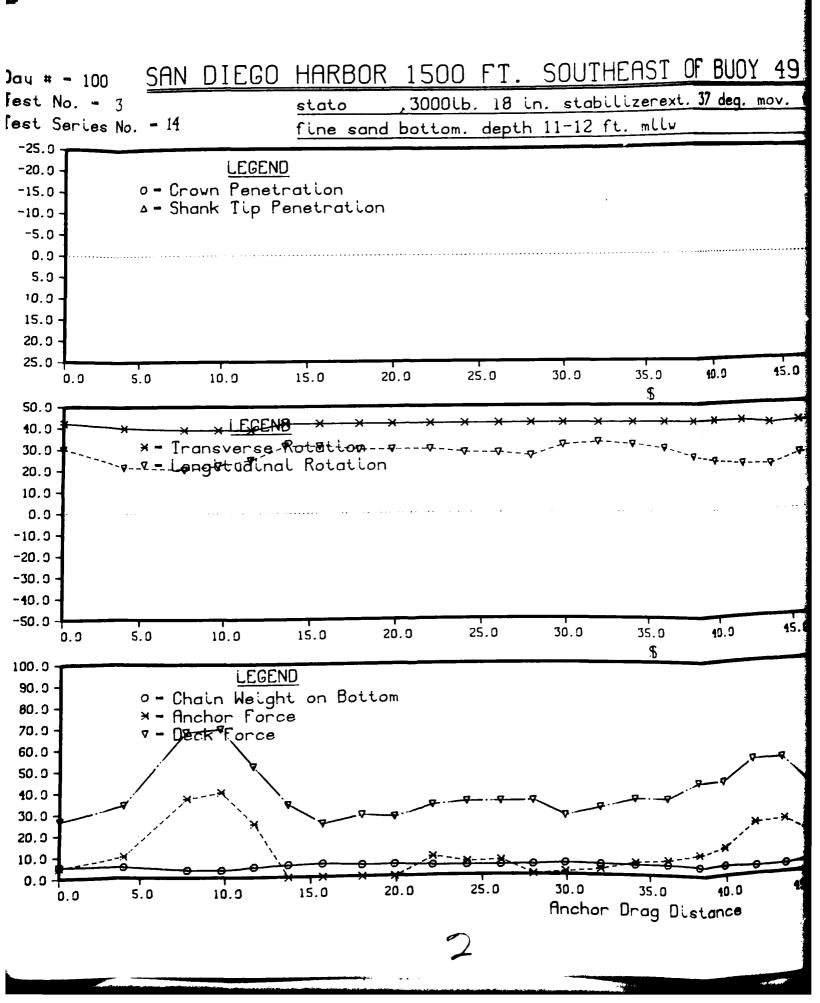
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Day # - 100
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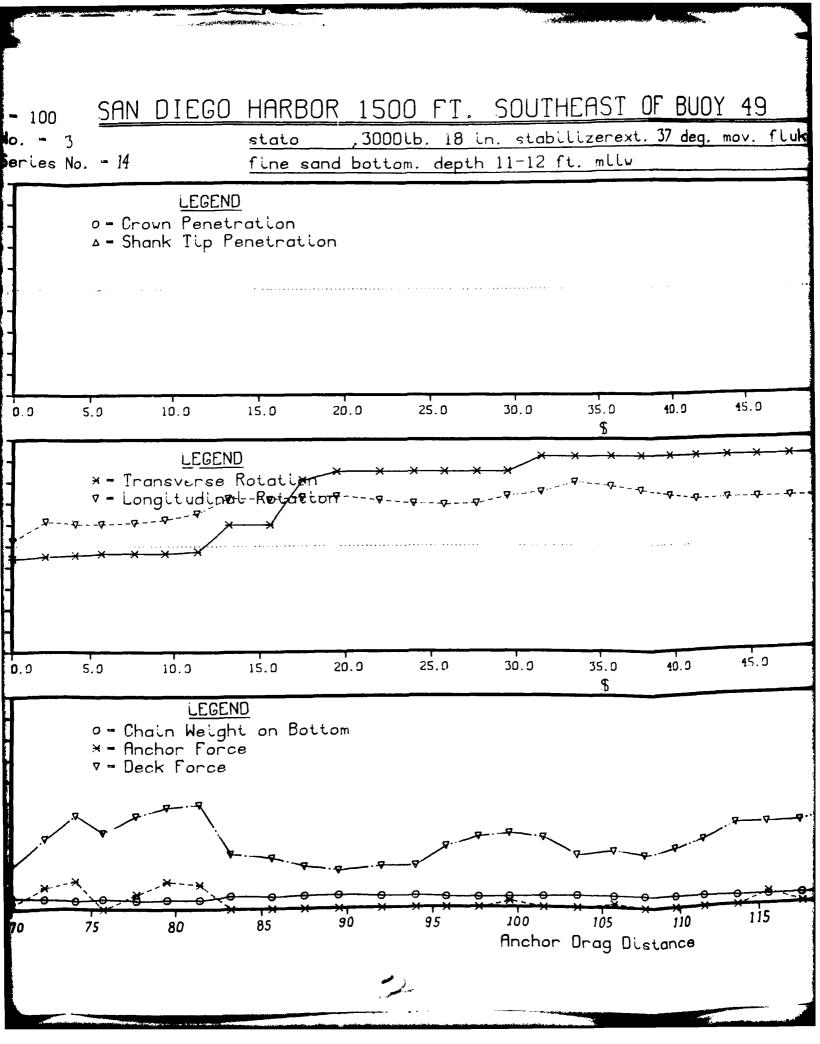
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OO FI. SOUTHEAST OF BUOY 49 10lb. 18 in. stabilizerext. 37 deg. mov. flukes om. depth 11-12 ft. mllv 25.0 30.0 55.0 35.0 60.0 65.0 50.0 70.9 40.0 45.0 \$ 25.0 30.0 35.0 60.0 65.0 55.0 70.0 45.0 50.0 40.0 5.0 60.0 30.0 65.0 70.9 50.0 55.0 35.0 40.0 45.0 Anchor Drag Distance 119



500 FT. SOUTHEAST OF BUOY 49 000lb. 18 in. stabilizerext. 37 deg. mov. flukes Ltom. depth 11-12 ft. mllv 25.0 30.0 35.0 60.0 65.0 45.0 50.0 55.0 70.0 40.0 25.0 30.0 35.0 45.0 50.0 55.0 60.0 65.0 70.0 49.0 130 95 135 100 Anchor Drag Distance 121

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TEST SERIFS

1504 - 1870

SEAFLORD TYPE

ANCHOR TYPE

ANCHOR WIGHT

FLINKF ANGLE-TYPE.

AUTHOR TYPE

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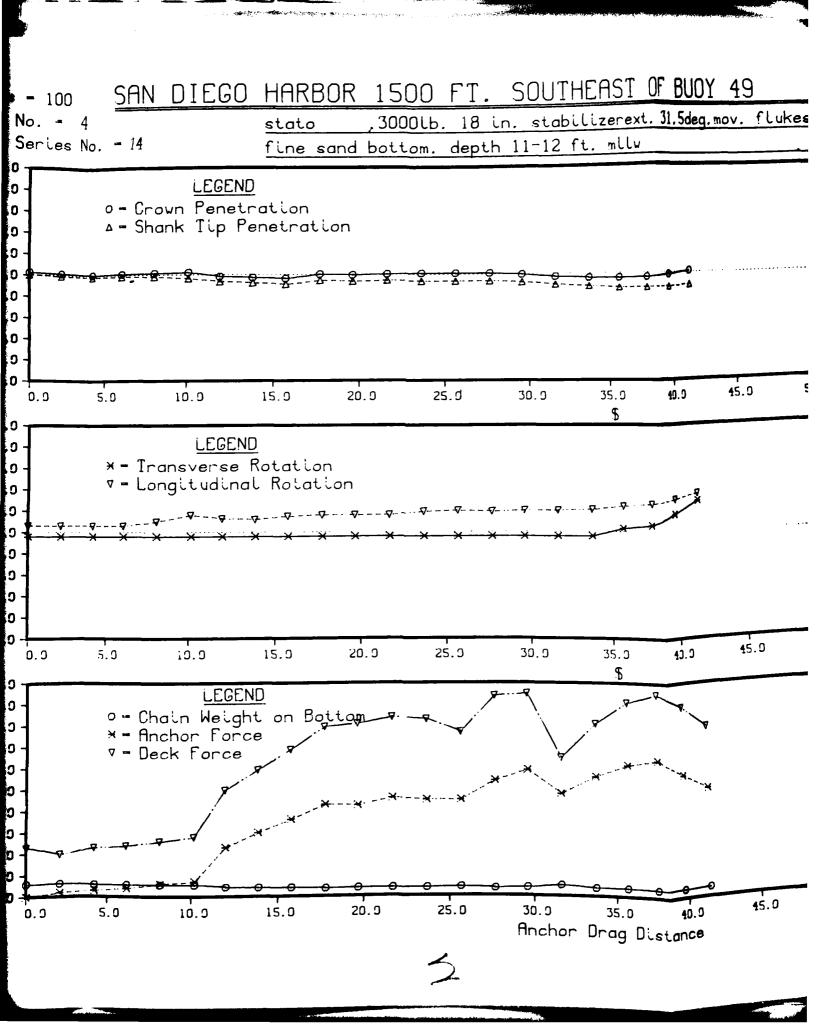
NOTE - INITIAL CHANK DEPTH PERGED TO REFLECT WEASHRED WATERDEPTH

	1. DOAG DISTANCE 4.			. ROTATION ANGLE 9.			CHAIN	LFNGTH	AN BOTTOM 13	13. AND	13. ANCHOR FLUKF		TIO NEPTH		
	P. DECK			CHANK	ANG F	10.	CHAIN	WFIGHT	ON HOTTOM	14. #41	FR DFDTH				
	3. ANCH		ION 7.		POPE ANG			CRUMN		15. TO	AL BOTTOM	HFIGHT	ī		
	4. PACK		TH 4.	DECK	10R[7. F	noce 12.	#MCHU6	CHANK	TIP NEPTH						
1	,	3	4	5	6	7	A	9	10	11	12	13	14	15	
FEFT	FIPS	< [₽5	FFFT	DFG	n# r-	DEG	# IPS	FFFT	į AS	FEFT	FEFT	FFFT	FFFT	í ec	
0.0	23.0	0.0	14.1	-2.0	7.0	5.9	>2.9	211.5	5927.4	13.9	14.5	17.3	14.5	#G27.4	
2.0	20.0	2.0	14.5	-2.0	3.0	6.0	19.9	>53.9	4201.0	14.2	14.8	17.6	14.5	9201.0	
4.7	23.0	3.0	14.4	-2.0	3.1	4.2	22.9	192.5	5407.6	14.4	15.0	17.4	14.5	REAT.A	
6.2	24.0	4.0	14.7	-2.0	3.0	4.2	23.9	179.1	5699.6	14.3	14.9	17.7	14.5	8699.K	
9.2	26.0	6.0	14.7	-2.0	5.0	6.0	25.9	175.2	5573.9	14.1	15.0	17.4	14,5	4571.Q	
10.2	24.n	7.0	14.0	-2.0	A.n	4.9	27.9	170.1	5413.4	13.9	15.4	17.7	14.5	8417.4	
12.0	50.0	23.0	15.7	-2.0	6.7	4.4	49.9	140.0	4455.4	14.9	16.1	18.5	14.5	7455.4	
13.9	59.5	30.0	14.0	-2.0	6.0	3.9	59.4	133.4	4744.7	15.2	16.4	14.9	14.5	7744.7	
15.9	69.0	36.0	16.7	-2.0	7.4	3.5	48.9	128.2	4079.7	15.4	16.8	19.1	14.5	7079.3	
17.8	79.5	47.0	15.4	-2.0	8.1	3.3	79.4	116.8	1715.1	14.4	15.9	18.2	14.5	4715.3	
19.7	A1.0	47.5	15.4	-2.0	A. ^	3.1	20.9	122.9	7911.2	14.6	16.1	18.4	14.5	4911.7	
21.7	84.0	46.0	15.4	-2.0	A.^	3.0	#3,9	122.4		14.4	15.9	18.2	14.5	4,005,4	
27.7	93.0	45.0	15.5	-2.0	9.5	3.0	97.9	174.1	3947.7	14.7	16.1	18.7	14.5	4947.7	
25.7	77.0	45.0	15.5	-2.0	10.0	3 4 0	76.9	133.9		14.7	16.1	16.2	14.5	7261.7	
27.7	94.0	54.0	15.5	-2.0	9,5	2.9	93,9	111.1	3575.9	14.3	16.1	18.2	14.5	4535.9	
29.6	95.0	59.0	15.9	-2.0	10.0	2.6	94.9	125.1	3982.1	14.6	16.4	18.5	14.5	6907.1	
31.6	65.0	48.0	16.4	-7.0	10.0	7.8	44.9	160.R	5116.4	15.2	17.0	19.1	14.5	#116.4	
13.7	91.0	54.0	16.4	-7.0	10,5	3.1	A0.9	122.9		15.5	17.5	19.5	14.5	4911.7	
35.7	91.0	61.5	17.1	1.5	12.0	2.8	90.9	120.9		15.6	17.9	19.7	14.5	6844.7	
37.7	95.1	64.0	17.1	3.0	13.0	2.8	94,9	114.7		15.5	17.9	19.4	14.5	6650.0	
19.7	89.0	57.0	17.0	0.9	15.0	2.8	AA.9	123.9	3944.0	15.0	17.A	19.3	14.5	6944.0	

DISTANCE SARGE TRAVELLED 47.0 DISTANCE ANCHOR TRAVELLED 41.6

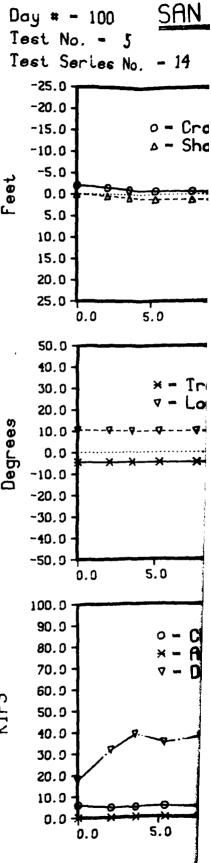
Note Anchor depth at end of drag measured -- centerline of shank at anchor crown # 18 inches.

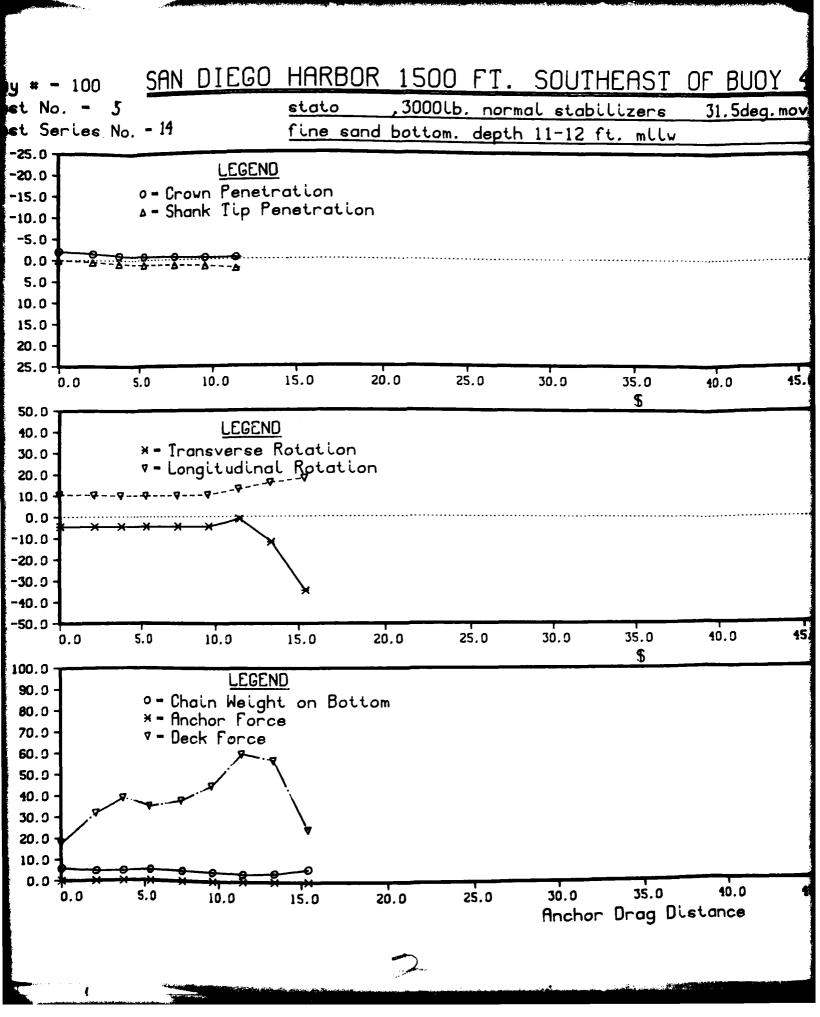
HOTE - DOSTTIVE CHANK ANGLE INDICATES CMANK TID RELOW CROWN



1500 FT. SOUTHEAST OF BUOY 49 3000lb. 18 in. stabilizerext. 31.5deg.mov. flukes bottom. depth 11-12 ft. mllv 2 - 2 - 2 - 2 - 2 - 2 - 2 70.0 65.0 60.0 55.0 50.0 45.0 25.0 30.0 35.0 40.0 \$ 70.0 65.0 60.0 55.0 50.0 25.0 45.0 30.0 35.0 43.3 70.0 65.0 60.0 55.0 50.0 25.0 45.0 35.0 Anchor Drag Distance 123

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                                                                                                                                                                                NOTE - INITIAL CHANK DEPTH ZEROFD TO REFLECT MEASURED WATERDEPTH
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                                                                                                                                                                                    S. ROTATION ANGLE 9. CHAIN LENGTH ON ROTTOM AS SHARK ANGLE 10. CHAIN WELGHT ON ROTTOM TO WIRE ROBE ANGLE 11. ANCHOR CROWN DEPTH 8. DECK HORIZ. FORCE 12. ANCHOR SHANK TIP DEPTH
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14. WATER DEPTH
15. TOTAL BOTTOM WEIGHT
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           0,0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             150.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             135.9
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             120.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             105.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        90.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        75.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        60.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         45.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         30.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         15.0
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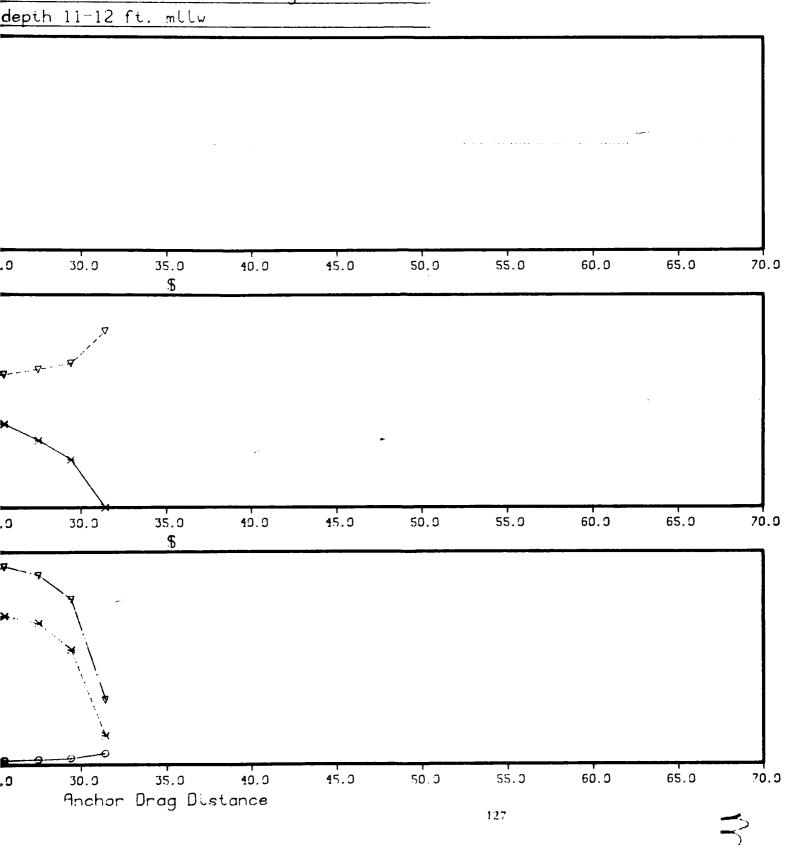
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0.0

SAN DIEGO HARBOR 1500 FT. SOUTHEAST OF BUOY 49 ,6000lb. normal stabilizers 32 deg. mov. flukes stato fine sand bottom. depth 11-12 ft. mllw **D.** - 19 LEGEND o - Crown Penetration 45.0 50.0 10.0 15.0 20.0 25.0 30.0 35.0 40.0 5.0 \$ LEGEND * - Transverse Rotation ▼ = Longitudinal Rotation 40.0 45.0 50.0 5.0 35.0 19.9 15.0 20.0 25.0 30.0 LEGEND 0 - Chain Weight on Bottom * - Anchor Force V = Deck Force 45.0 50.0 40.0 **5**.0 25.0 30.0 35.0 10.0 20,0 15.0 Anchor Drag Distance

FT. SOUTHEAST OF BUOY 49

normal stabilizers 32 deg. mov. flukes



```
Day # = 101
                                                                                                                                                                                                                                                                                                        Test No. - 2
                                                                                                                                                                                                                                                                                                        Test Series No.
                                                                                                                                            ANCHOP TEST
                                                                                                                                                                                                                                                                                                               -25.0
TEST DATE
TEST MO.
TEST SERIFS
TEST AREA
START-END TIMES
SEAFLOOR TYPE
AMCHOR TYPE
AMCHOR BYOF
AUT. AMCHOR TYPE
AUT. AMCHOR BYEGHT
MAIN. AUCHOR WEIGHT
MAIN.AUX ANCHOR WEIGHT
MAIN.AUX ANCHOR STPADATION
DEBRESCRIC.MO.-WT.FACH-TOTAL WT.
MODRING LINE DESCRIPTION
                                                                                                   101
                                                                                                                                                                                                                                                                                                              ~20.0
                                                                                                   C 19
CAN DIFON HARROD 1500 FT, SOUTHFAST OF LIST 1154
FINE SANN BOTTON. DEPTH 11-12 FT, MILW
STATO ... ADDOIGH. NORMAL STABILIZERS
COOR OF UR.
                                                                                                                                                                                                                                                                                                              -15.0
                                                                                                                                                                                                                                                                                                              -10.0
                                                                                                   4000.00 LB.
12.00 DEG. - 0
                                                                                                                                                                                                                                                                                                                  -5.0
                                                                                                    0.0 FFFT
n- n.n - 0.0 LA.
ANCHOP TO IRRET 2.5IN. STUDLINK CHAIN TO 340FT 2IN WIRE POPE
                                                                                                                                                                                                                                                                                                                     0.0
                                                                                                                                                                                                                                                                                                                     5.0
                                                     . NOTE - INITIAL CHANK DEPTH PERDED TO REFLECT MEASURED MATERDEPTH
                                                                                                                                                                                                                                                                                                                  10.0
                                                                                                            9. CHAIN LENGTH ON ROTTOM
10. CHAIN WEIGHT ON ROTTOM
11. ANCHOR CROWN DEPTH
12. ANCHOR CHANK TIP DEPTH
            1. DEAG DISTANCE
2. DECK TENSION
3. ANCHOR TENSION
4. PACKAGE DEPTH
                                                                                                                                                                                                                                                                                                                  15.0
                                                                                                                                                                                                                                                                                                                  20.0
                                                                                                                                      9
FEET
140.9
146.6
148.9
119.5
108.1
90.9
93.4
152.5
140.9
130.0
134.3
137.4
140.8
                                                                                                                                                        10
LRS
715].9
7468.6
5923.5
5420.6
498].7
4582.7
7768.7
7768.7
7768.7
7768.7
7768.7
7768.7
                                                                                                                                                                                  11
FEFT
14-0
14-1
13-6
12-8
13-3
13-4
13-4
13-6
11-5
11-2
11-4
10-9
11-1
              # [PS 29.5] 39.5 39.6 65.0 79.0 65.0 103.0 110.0 60.0 59.5 64.0 57.0 55.0 51.0 60.0 45.0
                                                                OFG
0.0
0.0
0.0
0.0
1.0
2.5
3.0
3.0
3.0
3.0
3.0
1.0
3.0
                                                                                                     DEG
5.6
5.5
4.6
4.2
3.4
3.4
3.7
4.5
4.5
4.7
                                                                                                                                                                                                                                                                                                                  25.0
                                  * IPS
                                .6
12.5
10.6
33.8
45.0
50.6
72.5
33.8
31.3
35.0
28.8
25.0
23.8
18.8
                                                                                                                                                                                                                                                                                                                 50.0
                                                                                                                                                                                                                                                                                                                  49.0
                                                                                                                                                                                                                                                                                                                  30.0
                                                                                                                                                                                                                                                                                                                 20.3
                                                                                                                                                                                                                                                                                             Degrees
                                                                                                                                                                                                                                                                                                                 10.0
DISTANCE MARGE TRAVELLED DISTANCE ANCHOR TRAVELLED
                                                                                                                                                                                                                                                                                                                     0.0
 Note Anchor depth at end of drag measured — centerline of shank at anchor crown =(-24) inches.
                                                                                                                                                                                                                                                                                                              -10.0
                                                                                                                                                                                                                                                                                                              -20.0
 NOTE - POSITIVE SHANK
ANGLE INDICATES
SHANK TIP BELOW
CROWN
                                                                                                                                                                                                                                                                                                             -30.0
                                                                                                                                                                                                                                                                                                             -40.0
                                                                                                                                                                                                                                                                                                             -50.0
                                                                                                                                                                                                                                                                                                             100.0
                                                                                                                                                                                                                                                                                                                 90.0
                                                                                                                                                                                                                                                                                                                 80.0
                                                                                                                                                                                                                                                                                                                 20.0
                                                                                                                                                                                                                                                                                                                 60.0
                                                                                                                                                                                                                                                                                                                 50.0
                                                                                                                                                                                                                                                                                                                 40.0
                                                                                                                                                                                                                                                                                                                 30.0
```

5.0

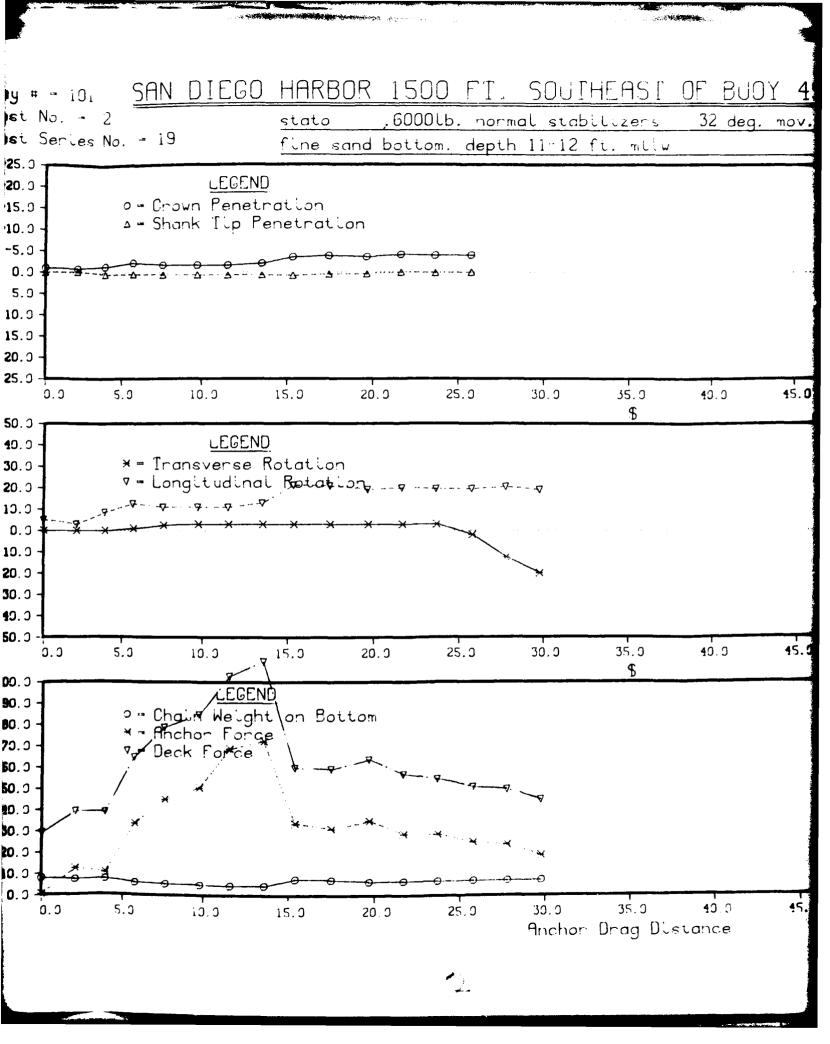
5.3

5.0

0.0

0.0

20.0 10.0 0.0



FI. SOUTHEAST OF BUOY 49 normal stabilizers 32 deg. mov. flukes depth 11-12 fr. mi.w **5**.0 55.0 60.0 65.0 70.0 50.0 40.0 30.0 35.0 · **4**5.0 \$ **5.**0 60.0 65.0 70.0 55.0 50.0 35.0 30.0 40.0 45.0 \$ 60.0 65.0 70.0 55.0 50.0 45.0 40.0 30.0 35.0 Anchor Drag Distance . 9

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Day # - 101
                                                                                                                                                                                                                                                                                           Test No. -
                                                                                                                                                                                                                                                                                          Test Series No.
                                                                                                                                                                                                                                                                                                  -25.0
                                                                                                              STATO
TEST DATE
TEST MO.
TEST SEPIES
TEST AREA
START-END TIMES
SEAFLOOR TYPE
ANCHOR TYPE
ANCHOR TYPE
AUT. ANCHORD TYPE
AUT. ANCHORD TYPE
AUT. ANCHORD TYPE
AUT. ANCHOR SEIGHT
MAIN-MAIR ANCHOR SEPARATION
DEPRESSORS.NO.-WILEACH-TOTAL WI.
MOORING LINE DESCRIPTION
                                                                                                                                                                                                                                                                                                  -20. O
                                                                                                   101
                                                                                                 3
19
2AN DIEGO HARROO 1500 FT. SOUTHFAST OF RUOY 49
1210 - 1220
FINE SANN BOTTON. DEPTH 11-12-FT. MLLW
2TATO ... 600018. NOPMAL STARILIZEPS 32 OF6
6000.00 LR.
12.00 DEG. - 0 0:MOV 1:FF!
                                                                                                                                                                                                                                                                                                  -15.0
                                                                                                                                                                                                                                                                                                  -10.0
                                                                                                                                                                                                    32 NEG. MOV. FLIMES
                                                                                                                                                                                                                                                                                                      -5.0
                                                                                                   0.00 IR.
0.0 FFFT
0- 0.0 - 0.0 LR.
ANCHOR TO TARFT 2-5IN. STUDLINK CHAIN TO 340FT 2IN WIRF PORF
                                                                                                                                                                                                                                                                                    eet
                                                                                                                                                                                                                                                                                                         0.0
                                                                                                                                                                                                                                                                                                         5.0
                                                        NOTE - INITIAL CHANK DEPTH ZERGED TO REFLECT MEASURED WATERDEPTH
                                                                                                                                                                                                                                                                                                      10.0
                                                        5. ROTATION ANGLE
6. SHANK ANGLE
7. WIPE POPE ANGLE
A. DECK HORIZ, FOR
                                                                                                           9. CHAIN LENGTH ON ROTTOM
10. CHAIN WEIGHT ON ROTTOM
11. ANCHOR CROWN DEPTH
12. ANCHOR SHANK TIP DEPTH
            1. DRAG DISTANCE
2. DECK TENSION
3. ANCHOR TENSION
4. PACKAGE DEPTH
                                                                                                                                                                                                                                                                                                      15.0
                                                                                                                                                                                                                                                                                                      20.0
                                 3
KIPS
0.0
5.0
12.5
13.1
22.5
32.5
55.0
                                                                                                                 9
FEET
142.0
160.2
141.9
145.3
127.9
124.2
98.3
A5.7
126.1
146.8
137.9
159.3
154.6
                                                                                                                                                       10
185
7120.3
8034.3
7218.6
7284.4
6412.8
6226.2
4927.3
4297.3
6322.5
7362.5
6916.0
7754.0
                                                                  5
0FG
-5.5
-5.5
-2.0
-2.0
0.0
8.5
11.0
30.0
40.0
                                                                                                                                                                                                                                                           15
Lec
13120.3
14034.3
13218.6
13286.4
12412.8
12226.2
10227.3
10290.4
12322.5
13362.5
12916.6
13989.0
13754.0
                                                                                                                                                                                                                                          25.0
FEET 0.0
2.0
4.1
6.1
8.2
9.9
11.8
13.6
13.6
17.7
19.8
21.8
23.8
                                                  FEET
14-1
14-0
13-6
13-5
14-0
14-2
14-1
13-8
13-6
13-7
13-7
                                                                                  0FG

4.c

17.c

17.c

17.c

16.n

21.c

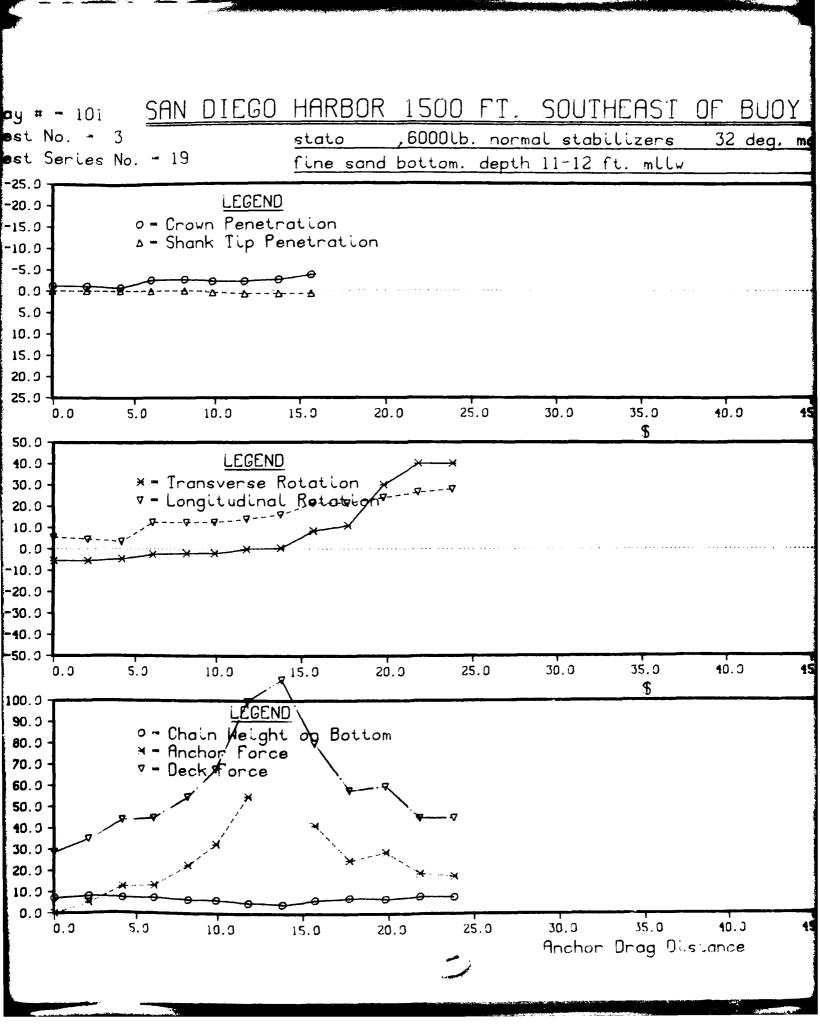
21.c

24.n
                                                                                                                                                                                                                                                                                                                           0.0
                                                                                                                                                                                                                                                                                                                                                                   5.0
                                                                                                                                                                                                                                                                                                       50.0
                                 41.3
25.0
28.8
18.8
17.5
                                                                                                                                                                                                                                                                                                       40.0
                                                                                                                                                                                                                                                                                                       30.0
                                                                                                                                                                                                                                                                                                       20.0
DESTANCE BARGE TRAVELLED DESTANCE ANCHOP TRAVELLED
                                                                                                                                                                                                                                                                                                      10.0
  Note: Anchor depth at end 
of drag measured — 
centerline of shank at 
anchor crown = (-6) inches
                                                                                                                                                                                                                                                                                                  -10.9
                                                                                                                                                                                                                                                                                                   -20.0
                                                                                                                                                                                                                                                                                                  -30.0
                                                                                                                                                                                                                                                                                                  -40.0
                                                                                                                                                                                                                                                                                                  -50.0
                                                                                                                                                                                                                                                                                                                           0.0
                                                                                                                                                                                                                                                                                                                                                                  5.0
                                                                                                                                                                                                                                                                                                  100.0
                                                                                                                                                                                                                                                                                                      90.0
                                                                                                                                                                                                                                                                                                      80.0
                                                                                                                                                                                                                                                                                                      70.0
                                                                                                                                                                                                                                                                                                      60.0
                                                                                                                                                                                                                                                                              KIPS
                                                                                                                                                                                                                                                                                                       50.0
                                                                                                                                                                                                                                                                                                       40.0
                                                                                                                                                                                                                                                                                                       30.0
                                                                                                                                                                                                                                                                                                       20.0
                                                                                                                                                                                                                                                                                                       10.0
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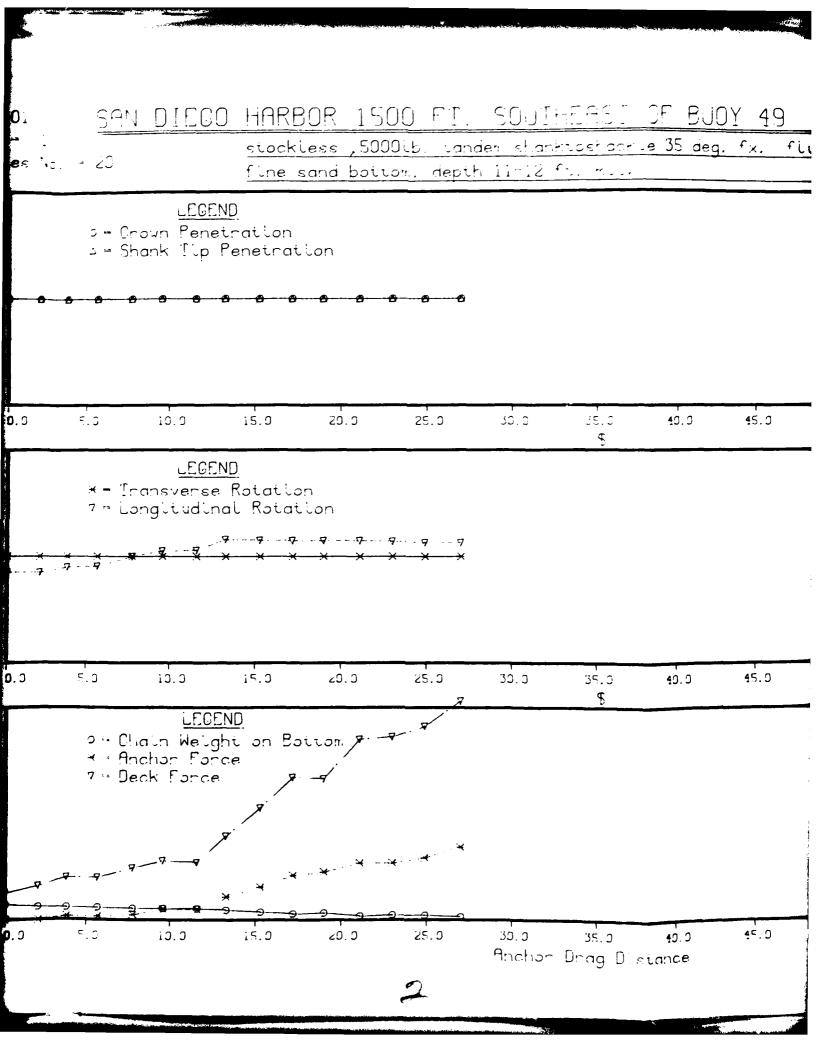
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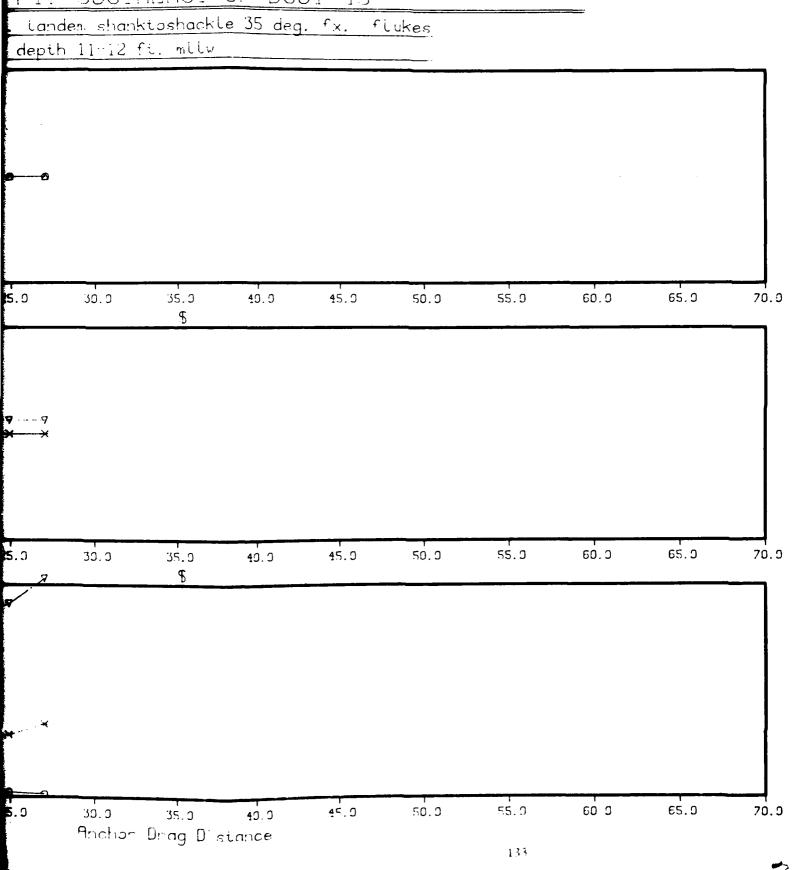


FT. SOUTHEAST OF BUOY 49 normal stabilizers 32 deg. mov. flukes depth 11-12 ft. mllw 35.0 30.0 40.0 45.0 50.0 55.0 60.0 65.0 70.0 \$ 5.0 30.0 35.0 45.0 40.3 50.0 60.0 55.0 65.0 70.0 \$ 30.0 45 0 50.0 35.0 55.0 60.0 65.0 40.J Anchor Drag Distance 131

	•						STOCKLES	s ANCI	HOP TEST						
	DATE .					101									
TEST DATE TEST NO.						1									
						20									
TEST SEATES TEST AREA						CAN DIFFO MARROS 1500 FT. SOUTHEAST OF RUNY 49									
START-END TIMES						1400 - 1421									
SEAFI DOR TYPE						FINE SAND ROTTOW. DEPTH 11-12 FT. MILW									
ANCHOR TYPE						STOCKLESS . SOOOL B. TANDEM SHANKTOSMACKLE TO DEG. FR. FLIMES									
ANCHOR WFIGHT						5950:00 18.									
FLIRE ANGLE-TYPE.						35,00 OFC 1 0=MOV 1=FT#									
AUX. ANCHOR TYPE						SARRE STOCKLESS ANCHOR									
AUX. ANCHOW WEIGHT						5950.00 [4.									
MAIN-AUR ANCHOR SEPARATION						45.0 FFFY									
DEPRESSORS . NO WT. EACH-TOTAL WT.						0 - 0.0 - 0.0 LP.									
#OOP I	NO LINE	DESCO	PTION			ANCHOR	TO GEF	T >[N. 9	TUDI INK CH	MEN TO	ALLY ANCH	INP TO 180	9		
						7.51N	STUDETA	K CHAIN	TO 340FT 2	IN. WIP	t bubl				
			NO T	E - INI	TIAL «H	ANK NER	7 7 7 F P O	FO TO PE	FLFCT MFAS	URFD WA	TFONEP **				
			•												
	1. DOAG DISTANCE S. ROTATION AND														
2. DECK TENSION A. SHANK ANGLE					In. CHAIN WEIGHT ON ROTTOM 14. WATER DEPTH										
	T. ANCH			MIRE P				A LEGAN		15. TO	TAL BOTT	OM MEIGHT	1		
	4. PACK	AGE OF	PT₩ A,	DECK H	OP[7, F	Uncl. 15	. ANCHO	D CHANK	TIP DEPTH						
1	,	3	4	4		7		9	10	11	12	13	14	15	
FFFT	KIPS	KIDS	FFET	DFG	DFG	ne c	FIPS	r F F T	1 AS	FFFT	FEFT	FFFT	FFFT	Į ne	
0.0	10.0	0.0	****	0.0	+7.5	6.2	18.9	244,9	*****		****	*****	13.0	2768A.	
2.0	24.0	0.0	****	0.0	-7.5	8.2	23.8	200.2	9715.7		••••	*****	13.4	21115.	
3.8	30.0	2.5	•••••	0.0	-5.^	7.4	29.A	191.4	8774.4	••••	****	****	13.0	20874.	
5.7	30.0	2.5	****	0.0	-4,5	7.3	29.A	192.4	AR76.4	•••••	•••••	*****	13.0	20724.	
7.8	37.0	3.8		0.0	0.0	7.1	36.7	177.3	A465.0		****	****	33.4	19944	
9,6	42.0	7.5	••••	0.0	7.7	6.4	41.7	(25.1	7956.6	••••	•••••	*****	13.0	19854.	
11.6	41.0	7,5		0.0	3.0	6.5	40.7	175.9	7997.A		••••	••••	13.0	19897.	
13.3	59,5	16.3	****	0.0	8.0	5.4	59.7	156.8	7030.9		•••••	****	13.4	14978.	
15.3	79.5	23.1	****	0.0	7.7	5.1	79.7	127.5	5571.2		•••••	••••	17.0	17471.	
17.2	101.0	31.3	•••••	0.0	7,5	4.7	100.7	103.4	4362.5		•••••	*****	13.0	16242.	
19.0	100.0	33.A	*****	0.0	7.6	4.4	99.7	115.5	4966.4	****	*****	•••••	13.0	TARKA.	
21.1	124.0	40.0		0.0	7.4	4.4	127.6	72.6	2418.3		*****	••••	13.0	14714.	
24.9	137.0	40.0	****	0.0	7.0	4.l	129.2	83.A	1379.4	*****	*****	****	13.0	15779.	
27.0	155.0	43.8	••••	0.0	6.5	3.9	134.7	82.7	3320.2 3005.0	*****	*****	*****	13.0	15224.	
-,,,	177.0	51.3		0.0	6.<	3.9	154.6	44.7	2095.9	•••••	•••••	••••	13.0	13995,	
Dista	NCE PAR	GF TRAV	ÆLLED	28.0											
	NCE ANC			27.0											
	-			• •											
Non	Anchor dept		•												
	urcio depi														



FI. SOUTHEAST OF BUOY 49

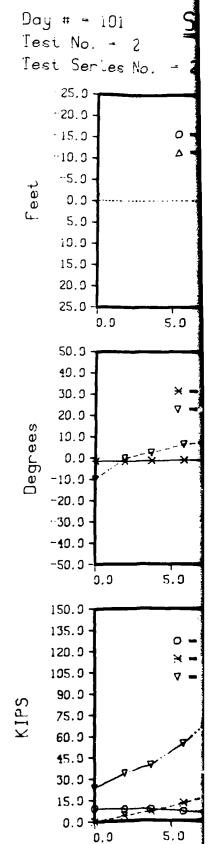


STOCKLESS ANCHOR TEST

DISTANCE MARGE TRAVELLED 24.0 DISTANCE ANCHOR TRAVELLED 23.1

Note Anchor depth at end of drag measured centerline of shank at anchor crown = 22 inches

HOTE - POSITIVE SHAWE ANGLE INDICATES SHAWE TIP RELOW CROWN



FI. SOUTHEAST OF BUOY 49 landem shanktoshackle 35 deg. fx. flukes depth 11-12 ft. mllw **5**.0 60.0 55.0 65.0 70.0 50.0 45.0 30.0 35.0 40.0 \$ 65.0 **5**.0 60.0 70.0 55.0 50.0 45.0 30.0 40.0 35.0 \$ 70.9 65.0 60.0 **5**.0 30.0 45.0 50.0 55.0 40.0 35.0 Anchor Drag Distance

135

30.9 15.9 0.9

0.0

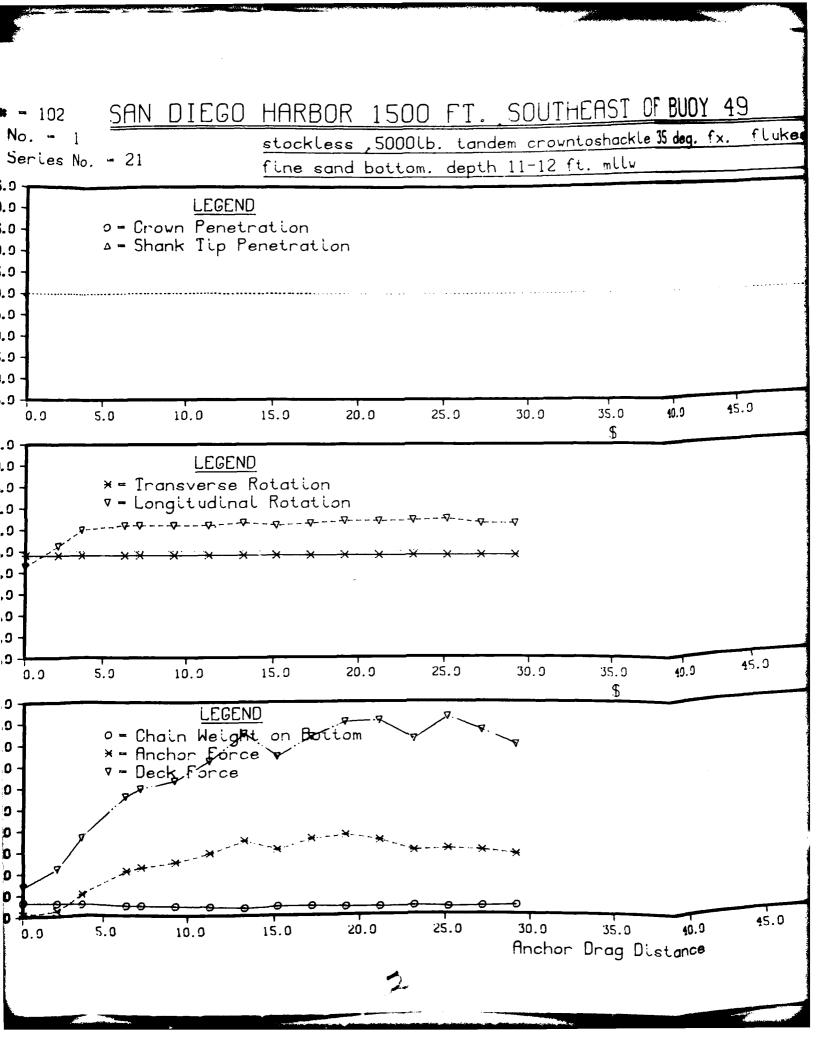
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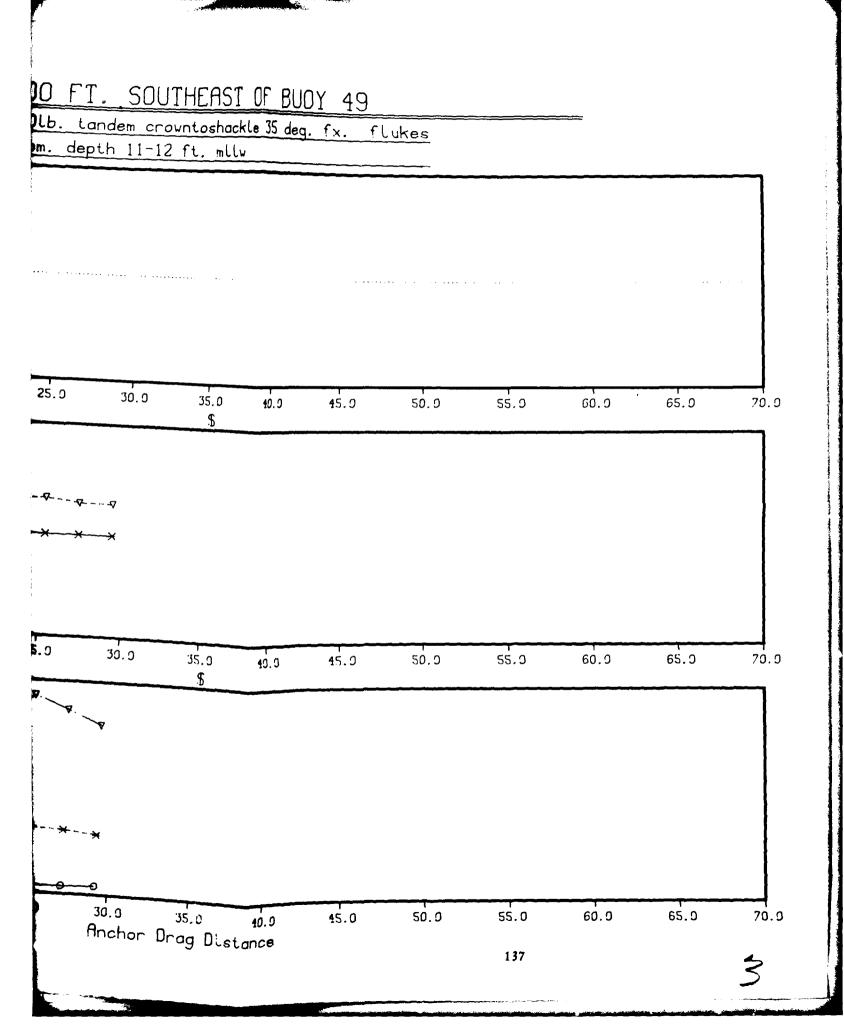
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TEST DATE
TEST NO.
TEST YOUR TEST NO.
TEST YOUR TEST NO.
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TEST YOUR TEST NO.
TEST YOUR TEST NO.
TEST YOUR TEST NO.
TEST YOUR TO THE CONTROL OF THE TEST OF GIVEN 49
TEST YOUR TYPE
TEST NO.
TEST YOUR TYPE
TEST NO.
TEST YOUR TEST NO.
THE CONTROL OF THE TEST OF GIVEN 49
TEST YOUR TEST OR ONLY THE TEST OF GIVEN A SECTION TO THE TEST OF GIVEN A SECTION TO THE TEST OF GIVEN T
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DISTANCE RARGE TRAVELLED 30.0 DISTANCE ANCHOR TRAVELLED 29.2

Note Anchor depth at end of drag measured — centerline of shank at anchor crown * 25 inches.

COUNT TO BE ON COUNTY CHANK TIP BE ON COUNTY CHANK TIP BE ON COUNTY COUN





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Day # = 102
 Test No. - 2
 Test Series No.
     25.0
    -20 0
    -15.0
    -10.0
     -5.0
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      0.0
 ā
      5.0
     10.0
     15.0
     20.0
     25.0
     50.0
      40.0
     30.0
     20.0
Degrees
     10.0
      0.0
    -10.3
    -20.0
    -30 0
    -40.0
    - 50.0
    150.0
    135.0
    120.0
    105.0
     90.0
     25.0
     60.0
     45.0
     30.0
     15.0
```

21

5.0

5.0

5.0

0.0

0.0

0.0

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STOCKLESS ANCHOR TEST
TEST DATE
TEST NO.
TEST SENTS
TEST ABEA
STABLEND TIMES
SEATION TYPE
AMCHON TYPE
AMCHON TYPE
AMCHON TYPE
ALIK, AMCHON TYPE
ALIK, AMCHON TYPE
ALIK, AMCHON TYPE
ALIK, AMCHON SPRADATION
DEPRESSORS, NO. - WT. FACH-TOTAL WT.
MODRING LINE DESCRIPTION
                                                                                                                                                                                                                     PI
SAN DIEGO MARROR ISON FT. SOLITHEAST OF RINGT 49
1007 - 1070
FIME SAMP BOTTOW, DEPTH 13-12 FT. MILLW
STOCKLESS, $50000 R. TANDEW CONWITOSHACKLE 35 OFG. FX. FLIMES
5950.00 LA.
SALON DEG. - 1 ORMOV 12FTY
SODOLR STOCKLESS AUCHOR
S950.00 IR.
45.0 FEET
0 - 0.0 - 0.0 R.
AMCHOR TO ASTT 21M. STUDIUM CHAIN TO AUX ANCHOR TO IRDET
2,51N STUDIUM CHAIN TO TANET 27M. WIRE GORF
                                                                                                                                                                                                                                                                                                                                                                                           13. ANCHOR FLIME TIP DEPTH
14. WATER DEPTH
15. TOTAL ROTTOM METCHT
                                                                                                                                                                                                                                        9. CHAIN LENGTH ON ROTTOM
IO. CHAIN WEIGHT ON ROTTOM
II. ANCHOR CPOWN OFFTH
IZ. ANCHOR SHANE TIP OFFTH
                                                                                                                            S. ROTATION ANGLE
A. SMANK ANGLE
7. WIDE ROPE ANGLE
8. DECK HORIT, EOD
                                                                                                                                                0FG .7 0.0 0.0 0.0 0.2 .2 .5 .5 .5 .5 .5 .5 .5
                                                                                                                                                                                                                          7
OFG
6.5
5.2
4.7
3.4
1.3
3.1
3.1
2.9
2.9
2.7
2.7
                                                                                                                                                                                                                                                       a

# PC

27.9

15.0

Cl.a

46.a

171.a

178.a

170.a

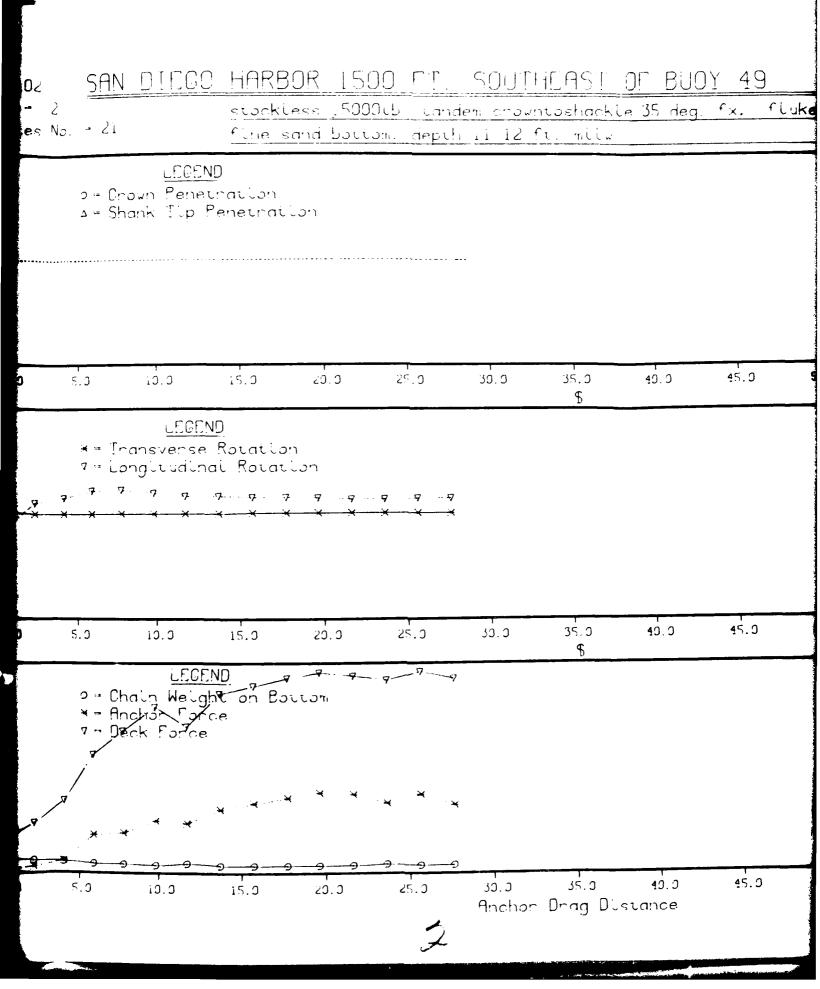
140.a

140.a

17.0

147.0

143.a
                                                                                                                                                                                                                                                                                                 9
FEET 716.5
203.4
1873.5
147.8
131.9
155.2
129.6
127.7
128.7
111.1
148.4
133.2
                                                                                                                                                                                                                                                                                                                                         10
194
9375.5
8377.5
A867.6
C788.7
A960.7
CA95.3
CA96.4
C740.5
A418.8
A418.8
A418.6
A418.6
                                                                                                              #IPS
27.0
36.0
52.0
RS.0
102.0
119.0
128.5
134.0
134.0
134.0
144.0
139.0
                                                                        RIPS
1.9
5.0
8.7
27.5
27.8
37.6
45.6
50.0
53.8
57.3
50.0
63.8
66.3
 STSTARCE MARGE TRAVELLED DISTANCE ANCHOR TRAVELLED
                      Anchor depth at end of drag measured — centerline of shank at anchor crown = 22 inches
                                         POSTTIVE GHANK
ANGLE INDICATES
GHANK TIP BELOW
PROMP
```



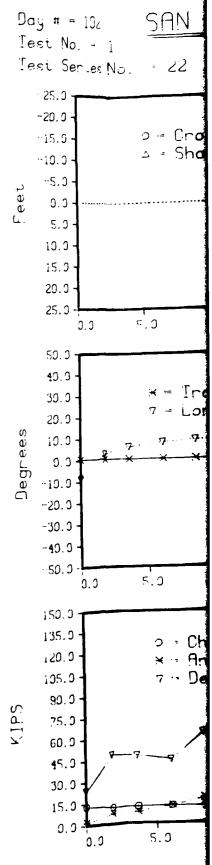
FT SOUTHEAST OF BUOY 49 vandem anowntoshackle 35 deg. fx. flukes depth ii 12 ft. milw 60.0 65.0 70.0 55.0 **2**5.0 30.0 35.0 50.0 40.0 45.0 \$ 65.0 60.0 70.0 **2**5.0 55.0 50.0 45.0 30.0 35.0 40.0 \$ 70.0 65.0 60.0 55.0 50.0 45.0 30.0 35.0 Anchor Drag Distance 139

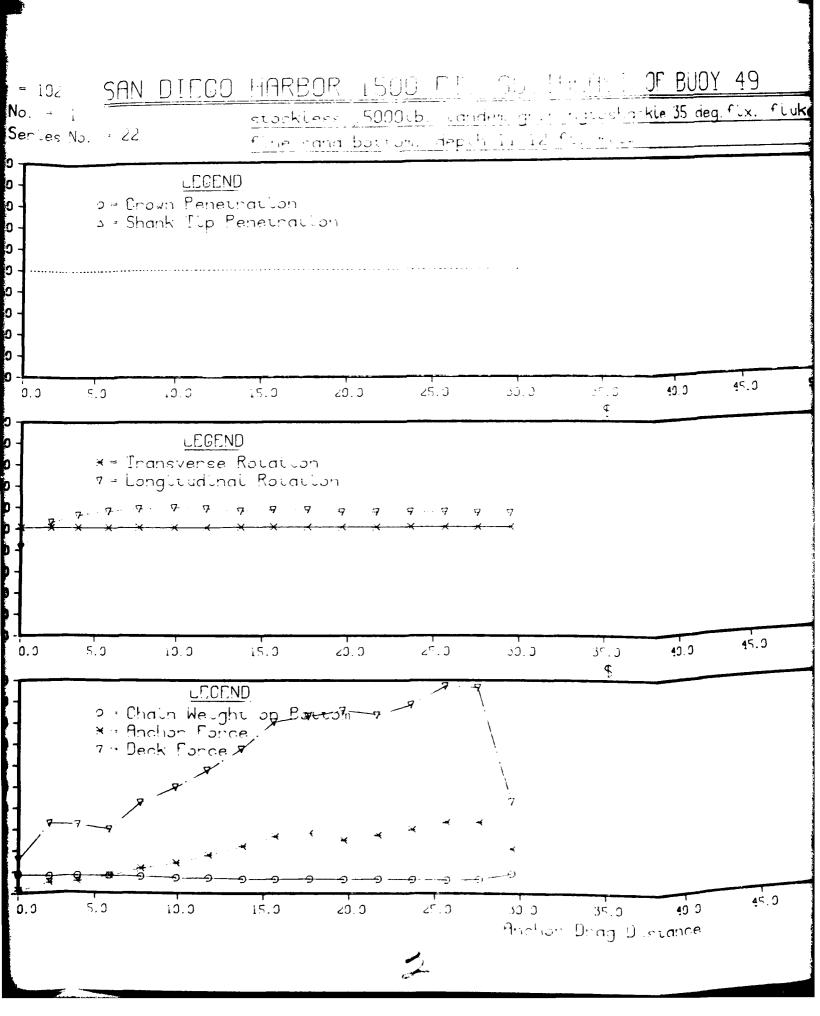
TOCKLESS ANCHOR TEST

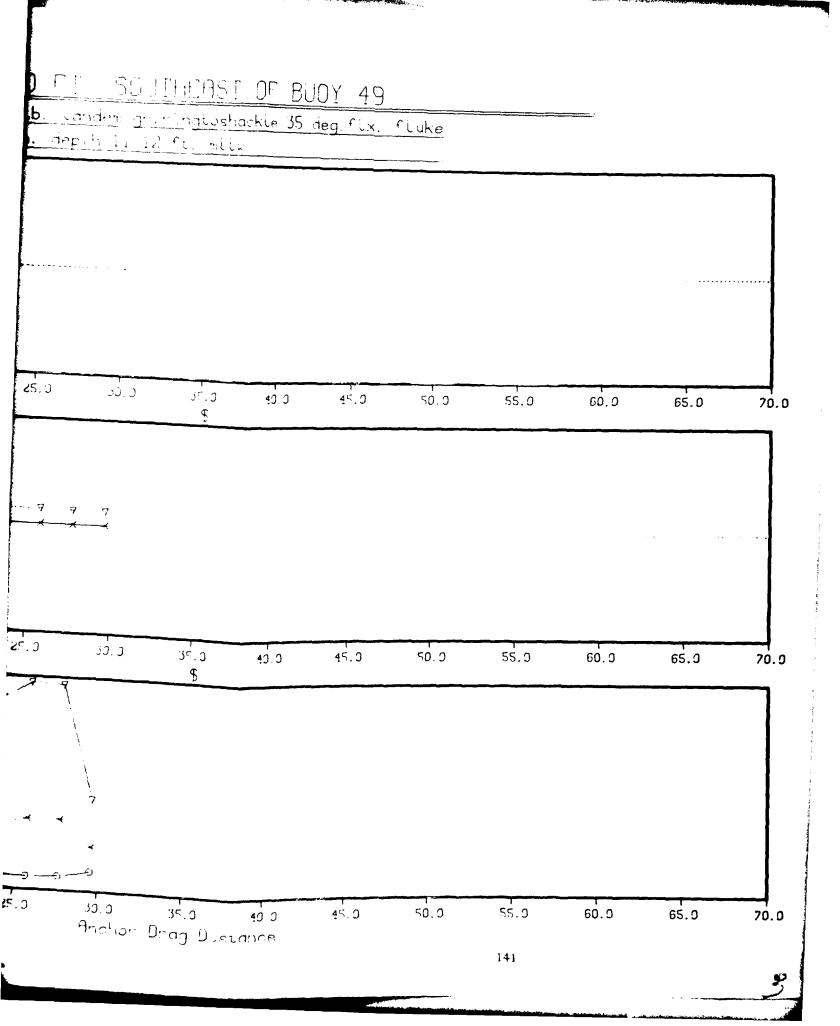
DISTANCE MARGE TRAVELLED 30.0 DISTANCE ANCHOR TRAVELLED 29.5

Note: Anchor depth at end of drag measured centerline of sharik at anchor crown = 15 inches.

NOTE - POSITIVE SMARK ANGLE INDICATES SMARK TIP RELOW CROWN







```
Day # - 106
  TEST DATE
TEST NO.
TEST SEDIES
THE S
                                                                                                                                                                                                                                                                                                                                                                                       106
]
24
                                                                                                                                                                                                                                                                                                                                                                                     74

CAN DIEGO MARROG AT RUDY 21

1177 - 1140

1-3 FT. WUD DYFOLDENSE SAND. DEPTH 35-38 FT. WILW

CTATO 3000 ft. 18-1W. STARILIFFOEXT. 31.5 DEG.WOY.FLIWES
3000.00 18.

31.50 DEG. - 0 0=WOY 18EFX
                                                                                                                                                                                                                                                                                                                                                                                       O.O LE.

O.O FFFT
O.O LE.

ANCHOP TO GOST 2 IN STUDY INK CHAIN TO IRRET 2,5 IN STUDY INK
CHAIN TO BARET 2 IN WIPF ORPE
                                               1. DRAG DISTANCE
2. DECK TENSION
3. ANCHOR TENSION
4. PACKAGE DEPTH
                                                                                                                                                                                                                        S. ROTATION ANGLE
A. SHANK ANGLE
T. WIPE BOPE ANGLE
9. DECK HORIT. FORCE
                                                                                                                                                                                                                                                                                                                                                                                                                       4. CHAIN ERIGHT ON ROTTON
11. ANCHOR CROWN DEPTH
12. ANCHOR CHANK TIP DEPTH
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            9

FFFT

251.2

212.4

212.4

197.3

197.3

185.3

117.4

165.0

173.1

200.7

200.7

200.7

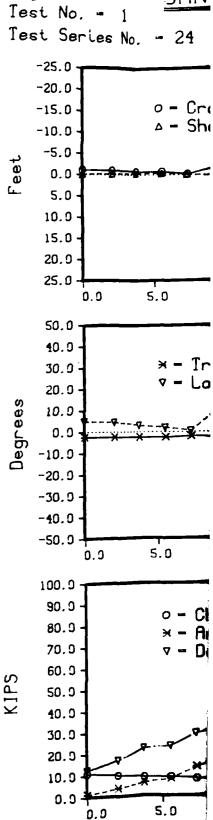
200.3

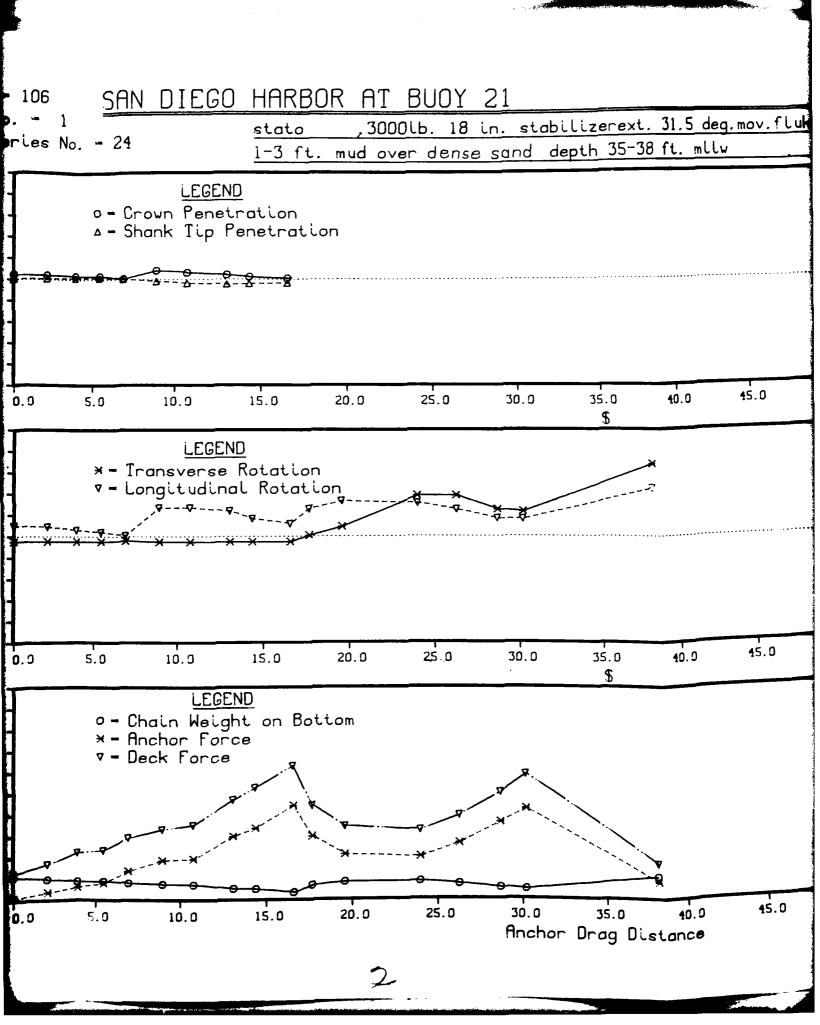
176.3

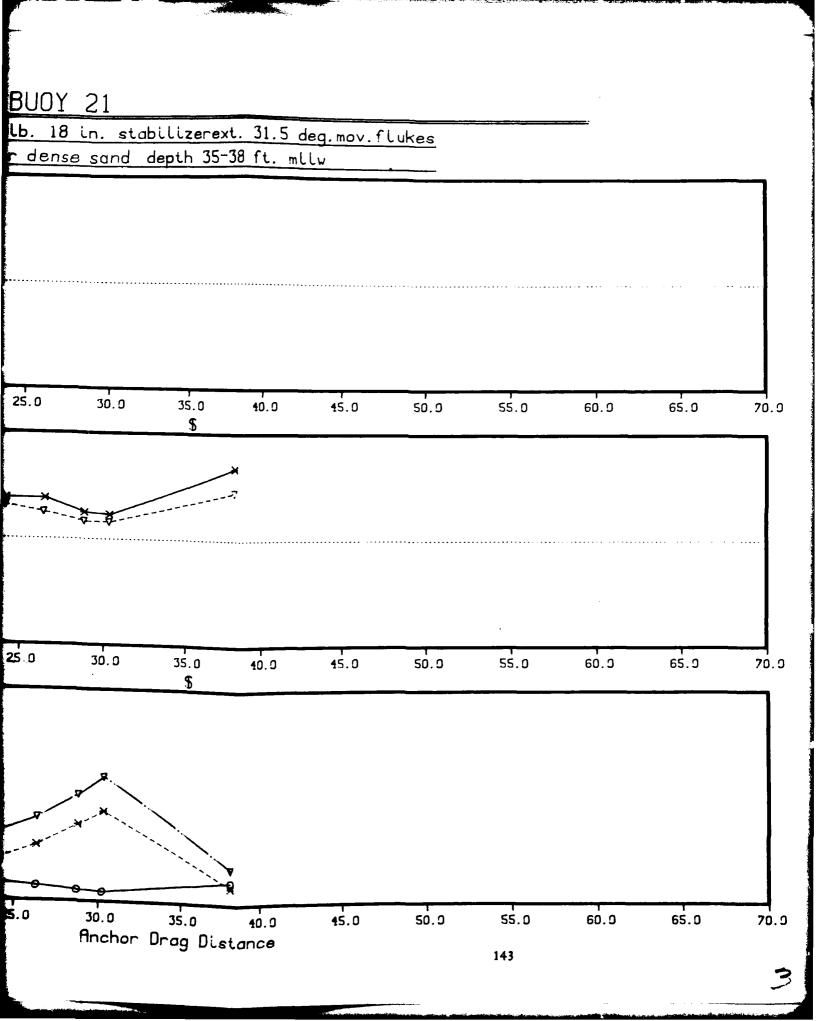
140.4

425.8

244.7
                                                                                                                            DISTANCE RARGE TRAVELLED DISTANCE ANCHOR TRAVELLED
      HOTE - DOSTITUE CHANK AND E INDICATES
```







```
STATO
 TEST DATE
TEST NO.
TEST SERIFS
TEST SERIFS
TEST SERIFS
START-END TIMES
SEART, ORD TYPE
ANCHOR TYPE
ANCHOR TYPE
AULI, ANCHOR TYPE
AULI, ANCHOR WEIGHT
MAIN-AUX ANCHOR SFRARATION
DEPRESSORS, NO.-BT.EACH-TOTAL WT.
HODBING LINE DESCRIPTION
                                                                                                                                                                   106
2
2
4
40 DIEGO MARROO AT 9UOY 21
1227 - 1236
1-3 FT. BUD OVEO DENSE SAND. DEPTH 35-38 FT. BLI W
5TATO .3000,0- TB TH. STABILIZEREXT. 31.5 DEG.MOV.FLUKES.
3000.00 LR.
31.50 DEG. - 0 0=MOV }=FJX
                                                                                                                                                                      0.00 FEFT
0.0 FEFT
0 - 0.0 - 0.0 LB,
0 - 0.1 - 0.0 LB,
4MCH0B TO GRET 2IN STUDLINK CHAIN TO IRRET 2.5IN STHIRLINK
CHAIN TO IRRET 2IN WIPE PAPE
                      1. NOAG DISTANCE
2. DECK TENSION
3. ANCHOR TENSION
4. PACYAGE DEPTH
                                                                                                4. ROTATION ANALE
A. SMANK ANGLE
7. WIRE POPE ANGLE
4. DECK HODIT. FORCE
                                                                                                                                                                                    9. CHAIN LENGTH ON POTTON
10. CHAIN WEIGHT ON ROTTON
11. ANCHOR CROWN DEPTH
12. ANCHOR SHAWE TIP DEPTH
                                                                                                                                                                                                                                                                                                    13. ANCHOR FLUKF TER DERTH
14. WATER DERTH
15. Total Bottom Weight
                                                                                                                                                                                                                                                                18
185
00000
9406.1
4733.5
5046.5
1808.0
1801.3
8601.3
                                                                                                                5
DFG
-1.0
-1.0
-1.0
-1.0
-1.0
3.5
3.5
                                                                                                                                                                                                                                 9
FEET
745.2
270.5
207.0
113.4
110.7
204.4
209.1
                                                                                                                                                                                                    #

FIPS

14.6

27.5

26.5

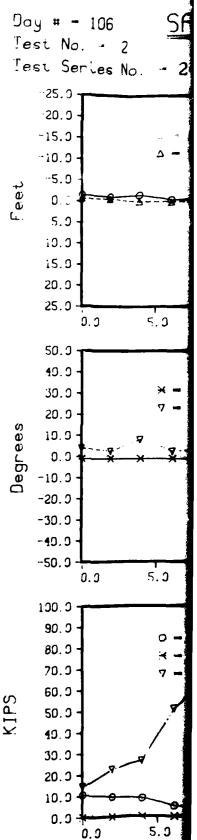
51.2

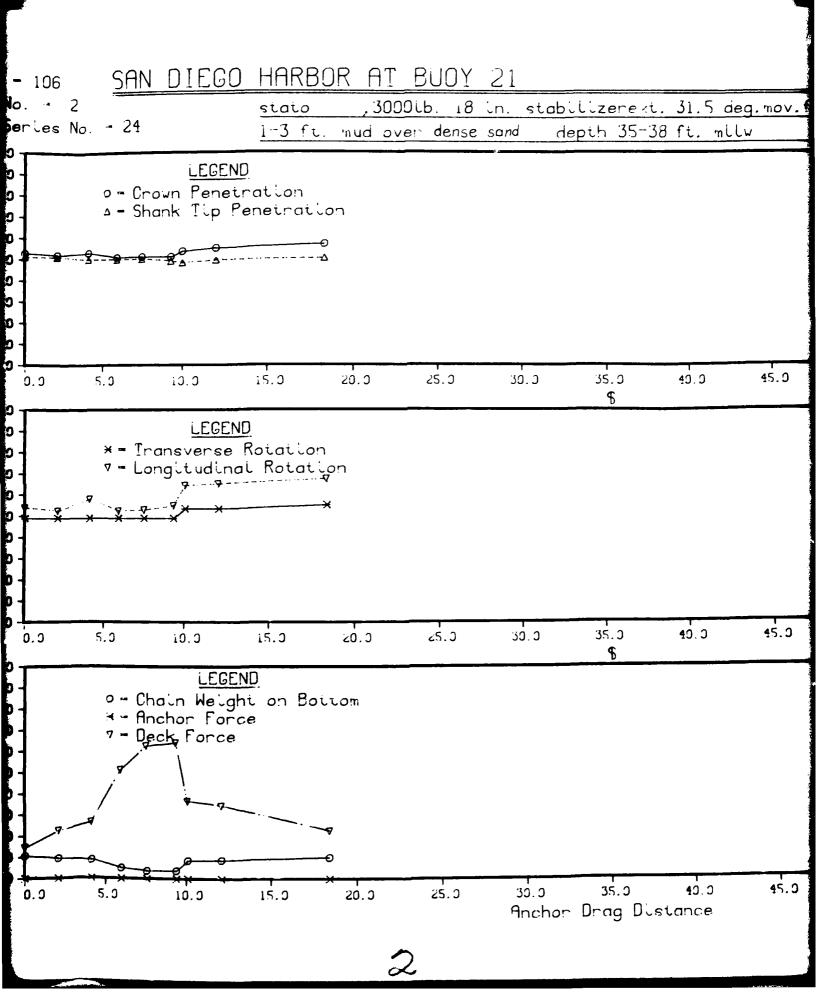
62.7

64.2

16.6

27.7
                                                                                                                                            A
DFG
4.6
7.5
7.6
7.6
14.6
15.7
                                                                                                                                                                                                                                                                                                                                         12
FFFT
40.4
40.4
40.9
41.0
41.4
41.8
41.8
                                                                                                                                                                                                                                                                                                                                                                                                           7
K1PS
15.0
27.0
57.0
61.5
64.0
37.0
21.0
                                                                                                                                                                                                                                                                                                         ) | FEFT | 19.6 | 19.4 | 40.5 | 40.4 | 19.1 | 18.4 | 17.5
                                                                                    FEET
40.1
40.2
40.4
40.7
41.0
40.3
39.8
                                                                                                                                                                         NEG
13.2
11.7
11.4
10.0
9.3
9.0
8.5
8.6
9.9
DISTANCE RANGE TRAVELLED
BISTANCE ANCHOR TRAVELLED
                      - POSTYTUE SHINE
SHARE TIP BELOW
CROWN
```



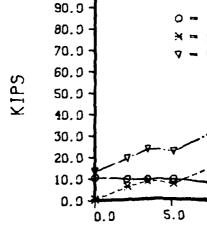


stabilizerext. 31.5 deg.mov.flukes depth 35-38 ft. mllv 35.0 . o 45.0 55.0 60.0 35.0 65.0 50.0 70.0 40.0 35.0 45.0 30.0 50.0 40.0 55.0 60.0 70.9 . o 65.0 8 35.0 33.0 45.0 50.0 55.0 60.0 65.0 70.0 40.0 . ၁ Anchor Drag Distance 145

-20.0 -15.0 -10.0 -5.0 0.0 5.0 10.0 15.0 20.0 25.0 0.0 5.0

50.0

100.0



STATO ANCHOR TEST

TEST DATE

TEST MO.

TEST SEDIES

TEST SEDIE

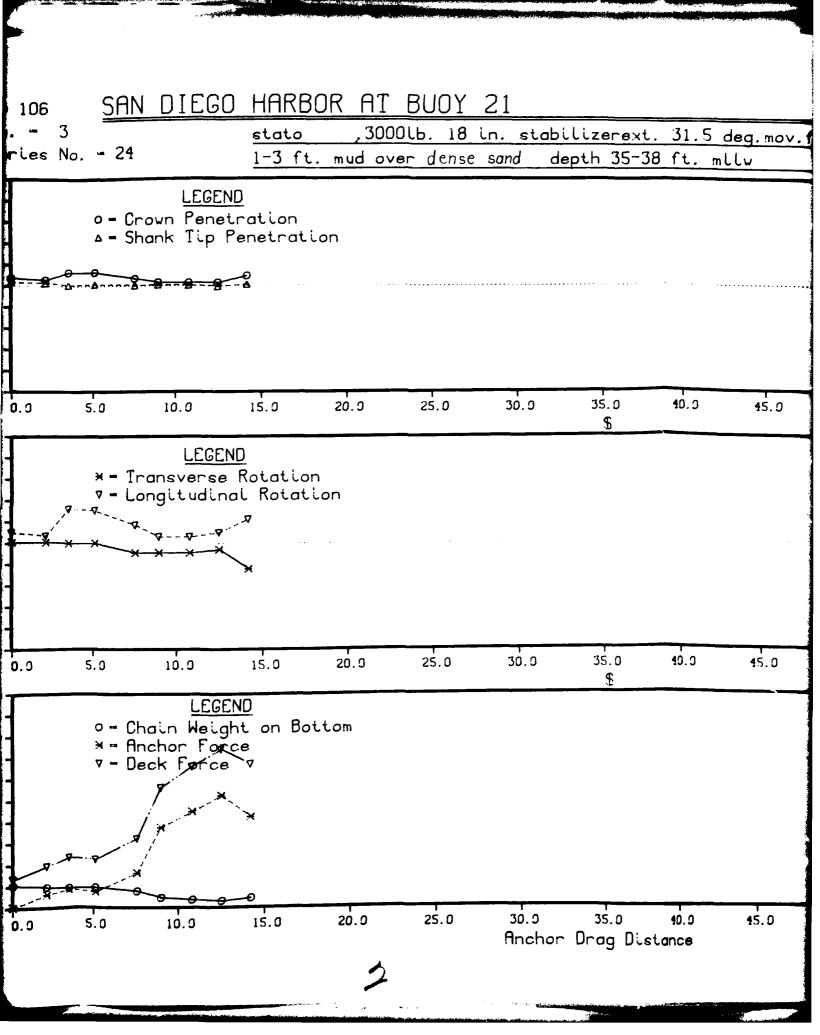
106
34
can D[FGO HADROD AT RIDY 2]
1330 - 1330
1-3 ff. win Dyep DENSE SAND. DEPTH 35-38 Ff. will w
ctato sandia. Ia in. Starli [FFOFKT. 3].c DEG., MOV., FLINFC
3000.00 1-2.
31.50 DEG. - 0 0=MOV [FF]X
0.00 FF.
0.01 FF.
0.02 FF.
0.03 FF.
0.04 FF.
0.05 FF.
0.06 FF.
0.07 FF.
0.08 FF.
0.08 FF.
0.08 FF.
0.08 FF.
0.08 FF.
0.09 FF.
0

DISTANCE MARGE TRAVELLED 14.0 DISTANCE ANCHOR TRAVELLED 14.2

HOTE - DOSTTIVE CHAME SNG F THRECATES CHAME TID RELOW CROWN

4

ologie filmani alia 1949 (1941) (1941)



21 18 in. stabilizerext. 31.5 deg.mov.flukes depth 35-38 ft. mllw dense sand 25.0 30.0 35.0 55.0 60.0 65.0 40.0 45.0 50.0 70.0 \$ 50.0 55.0 60.0 **25**.0 30.0 35.0 65.0 40.0 45.0 70.0 70.0 25.0 30.0 55.0 60.0 65.0 45.0 50.0 35.0 40.0 Anchor Drag Distance 147

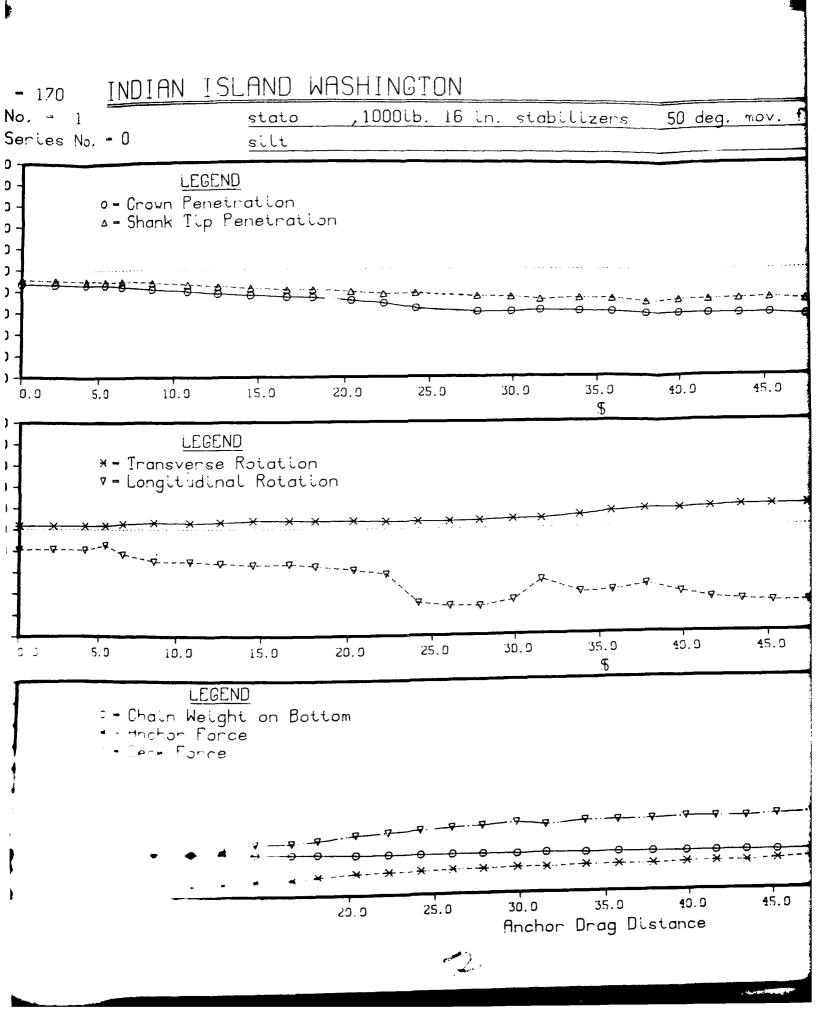
```
Day # - 170
Test No. - 1
Test Series No.
   -25.0
   -20.0
   -15.0
   -10.0
    -5.0
     ٥,٥
     5.0
    10.9
    15.0
    20.0
    25.0
         0.0
                   5.0
    50.0
    40.0
    30.9
    20.0
   10.0
    0.0
  -10.0
  -20.0
  -30.0
  -40.0
  -50.0
                   5.0
         0.0
  100.0
   90.0
   80.9
   70.9
   60.0
   50.0
   40.0
   30.0
   20.0
   10.9
    0.0
                   5.0
         0.0
```

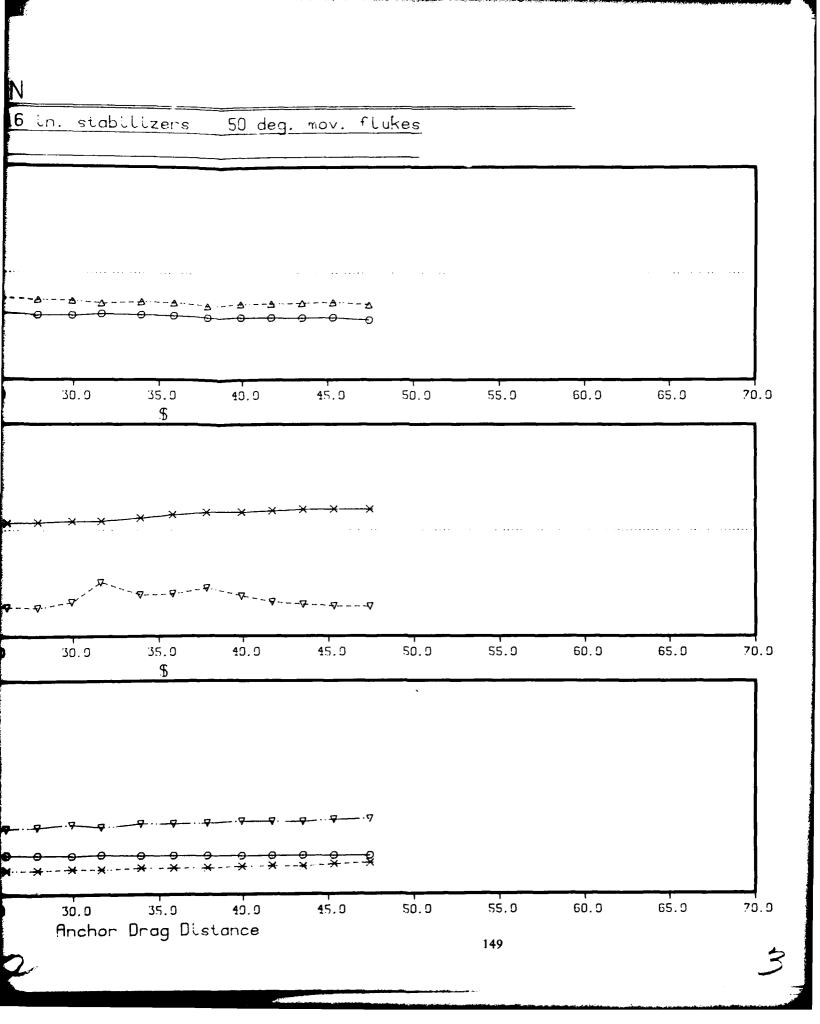
```
| 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170
```

STATO

ARCHOD TEST

MUTE ~ POSITIVE SMANK ANGLE INDICATES SMANK TIP BELOW CROWN





```
Day # - 172
  Test No. - 7
 Test Series No.
    -25.0
    -20.0
    -15.0
    -10.0
     -5.9
      0,0
      5.0
     10.9
     15.0
     20.0
     25.0
                     5.0
           0.0
     50.0
     40.0
     30.0
     20.0
Degrees
     10.0
      0.0
    -10.0
    -20.9
    -30.0
    -40.0
    -50,0
                     5.0
           0.0
    100.0
     90.0
     80.9
     70.0
     60.0
     50.9
     40.0
     30.0
     20.0
```

10.0 0.0

0.0

5.0

0

```
TEST DATE
TEST NO.
TEST NAM
TEST AREA
START-END TIMES
SEAFLOR TYPE
ANCHOR TYPE
ANCHOR TYPE
ANCHOR TYPE,
AUL. ANCHOR TYPE
AUL. ANCHOR TYPE
AUL. ANCHOR TYPE
ORDERSORS, NO.—MT. EACH—TOTAL MT.
POURING LIME DESCRIPTION
                                                                                                                                                                                        0
INCIAN ISLAND WASHINGTON
1255 - 1320
SILT
STOCKLESS 9000LBS.W.STAB
11370 LB.
48.00 DEG. - 0 0-MOV
                                                                                                                                                                                                  0.00 LB.
C.O FEET
- 0.0 - 0.0 LB.
FT. 2 IA. CMAIN, 360 FT, 2.5 IN. CHAIN, 400 FT. 1 5/8 IN.
RC ROPE, 346 FT. • 2 IN. INRC ROPE
                                                                                                           5. ROTATION ANGLE
6. SHANK ANGLE
7. BIRE ROPE ANGLE
8. DECK MORIZ. FORCE 12. ANCHOR SCHAMK TIP DEPTH
                       1. DRAG DISTANCE
2. DECK TENSION
3. ANCHOR TENSION
4. PACKAGE DEPTH
                                                                                                                                                                                                                                                                                       10
LBS
198C0-0
18800-7
18791-5
18613-1
18205-1
17603-9
17031-7
16684-8
15935-2
19470-8
14732-4
14013-6
14792-8
14013-6
14341-6
13431-6
13311-5
12985-0
                                                                                                                             9

427.7

407.9

407.6

404.4

404.1

395.9

372.5

365.6

348.7

425.3

341.6

322.7

327.9

312.3

313.6

2312.7

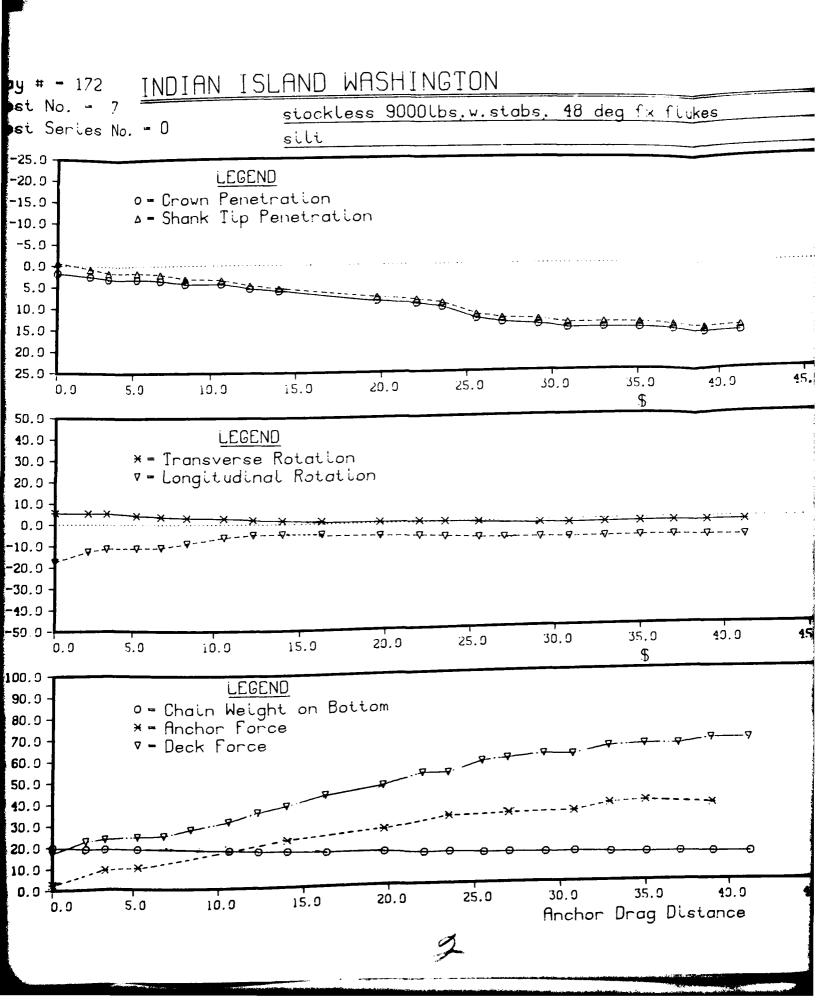
308.2

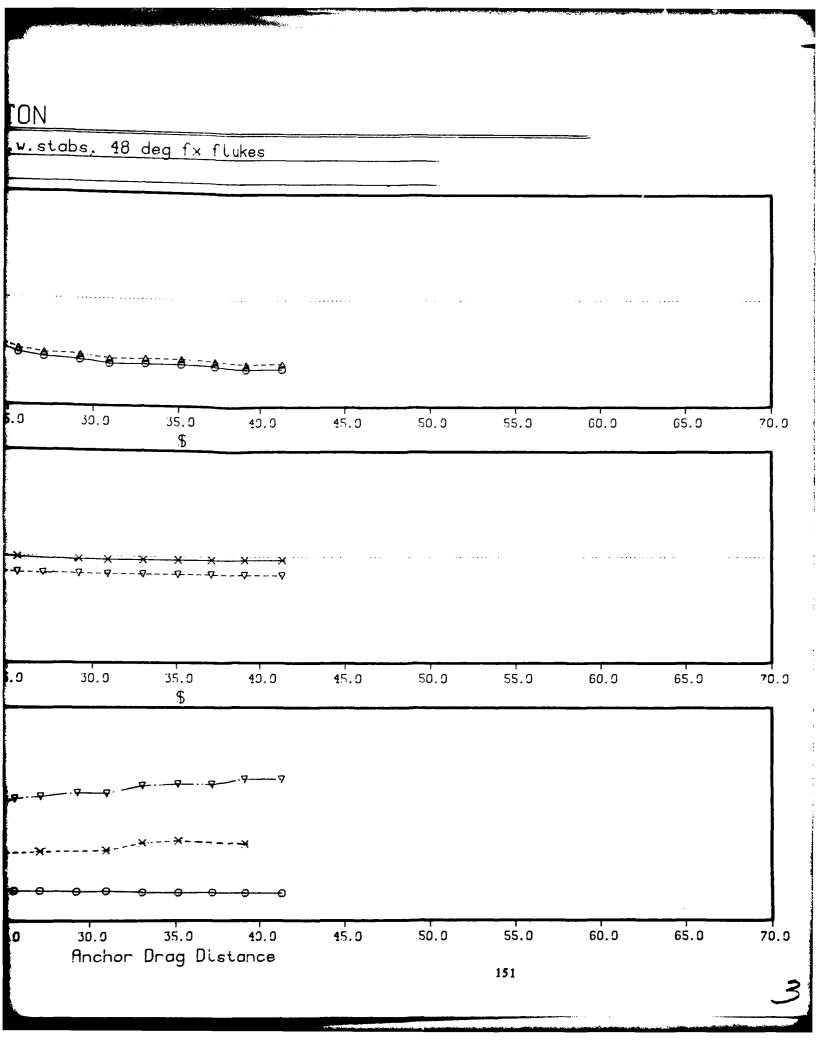
298.3

291.8

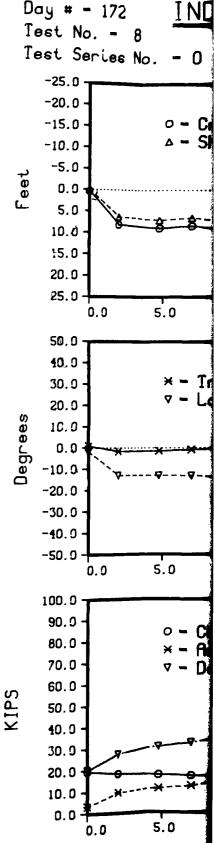
289.4
                                                                                                                                                                                                                                                                                                                                                                                                                                                        KÍPS
2.5
                                                                                                                                                       0EG
-17-4
-12-0
-11-20
-11-20
-8-8
-6-9
-4-7
-5-9
-7-6-9
-7-6-9
-7-8-1
-8-3
-8-3
-8-6
                              KIPS
18.0
24.3
25.2
25.7
32.2
36.3
36.3
36.3
49.0
25.6
47.8
53.1
53.1
53.3
60.7
64.9
67.3
                                                                                              DEG
15-8
14-7
14-1
13-8
12-8
11-7
11-4
11-0
10-3
10-3
10-1
10-1
                                                                                                                                                                                                                           KIPS
17.3
23.5
24.9
28.5
35.3
35.3
35.3
45.9
52.1
35.5
57.5
60.8
643.9
66.3
66.3
                                                                9.L
10.1
                                                                22.0
                                                                26.8
                                                                32.6
                                                               33.1
36.6
37.6
                                                                35.9
DISTANCE MARGE TRAVELLED DISTANCE ANCHOR TRAVELLED
                                                                                                                              44.0
```

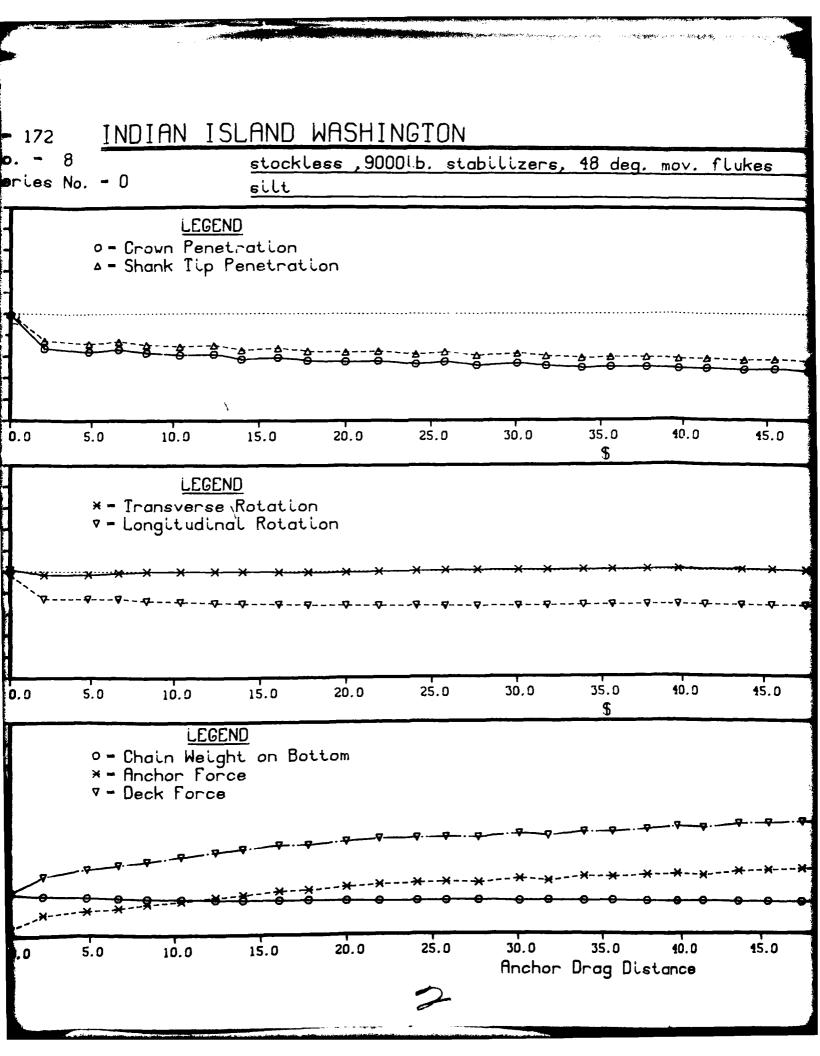
NOTE - POSITIVE SHANK ANGLE INDICATES SHANK TIP BELOW CROWN STECKLESS ANCHOR TEST





Day # - 172 STOCKLESS ANCHOR TEST -25.0 TEST DATE TEST NO. TEST RUN TEST RUN TEST AREA START-END TIPES SEAFLOOR TYPE ANCHOR TYPE ANCHOR TYPE ALCHOR TYPE AUX. ANCHOR TYPE, AUX. ANCHOR TYPE AUX. ANCHOR SEJARATION DEPRESSORS-NO.-WI-EACH-TOTAL MT. PEORING LIME DESCRIPTION -20.0 C INCIAN ISLAND WASHINGTON 1430 - 1447 SILT STOCKLESS .9000LB. STABILIZERS, 48 DEG. POV. FLUKES . 11370 LB. 48.00 DEG. - 0 0-ROY 1-FIX -15.0-10.0 0.00 LB. C.O FEET O - 0.0 - 0.0 LB. 90 FT. 2 IN. CHAIN, 300 FT. 2.5 IN. IMBC ROPE, 346 FT. • 2 IN. IMRC ROPE -5.0 0.0 5.0 5. ROTATION ANGLE 9. CHAIN LENGTH ON BOTTON 6. SMANK ANGLE 10. CHAIN WEIGHT ON BOTTON 7. WIRE ROPE ANGLE 11. ANCHOR CROBN DEPTN 8. DECK MORIZ. FORCE 12. ANCHOR SMARK TIP DEPTH 1. DRAG DISTANCE 2. DECK TENSION 3. ANCHOR TENSION 4. PACKAGE DEPTH 10.0 7 0EG 12.4 12.6 12.6 12.6 11.9 11.5 11.4 11.3 11.3 11.3 11.3 11.1 11.0 10.9 10.6 10.7 10.6 9 FEE1 421.9 399.7 385.0 379.2 377.1 361.8 364.5 355.5 346.9 345.7 348.1 339.0 345.4 339.0 345.4 339.0 345.4 339.0 3339.1 337.4 230.7 10 LBS 19509.2 18394.5 17657.7 17364.2 17103.5 16496.1 16405.1 16405.1 16427.6 19551.3 19688.1 19551.3 19688.1 19571.7 15370.7 15370.7 15370.7 15370.7 15370.7 15470.2 17493.7 15.0 9 6 066 CEC -1.7 -13.0 -1.4 -13.0 -7 -13.0 0.0 -14.2 0.0 -14.8 0.0 -15.1 -3 -15.6 -4 -16.4 -3 -16.6 -4 -16.4 -4 -16.5 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 -4 -16.6 8 K20-7 31-9 31-9 31-9 40-2 43-9 45-3 47-9 45-6 45-6 45-6 45-6 45-6 45-6 45-7 47-7 47-7 47-7 47-9 45-8 11 FEET 71-2 99-0 99-7 99-2 100-0 100-5 100-3 101-5 101-6 102-0 101-9 102-6 102-9 102-4 103-9 103-8 103-8 103-8 103-8 103-8 103-8 103-8 103-8 103-8 12 FEET 90.9 97.8 97.8 97.3 98.1 98.5 98.2 99.6 100.3 100.1 101.2 101.0 101.5 101.5 101.5 101.5 4 91-0 97-7 98-4 97-7 99-1 98-9 100-3 100-3 100-3 101-3 101-8 101-8 101-8 101-8 101-8 101-8 101-8 102-1 102-1 102-2 102-2 102-2 13 FEET 75-4 102-3 103-0 102-5 103-7 103-7 103-6 104-6 104-9 105-1 105-9 105-9 105-9 106-0 106-3 106-4 106-8 107-2 107-2 KIPS 20.9 21.8 33.6 33.6 33.6 33.6 43.1 43.8 46.6 46.6 46.6 46.6 46.6 46.6 52.8 52.8 53.0 Kips 3.3 9.6 11.4 12.6 14.7 15.9 17.7 10.7 20.5 21.0 22.5 24.0 24.5 24.0 25.8 26.5 27.3 29.6 30.3 30.3 20.0 25.0 50.0 40.0 30.0 20.0 10.0 0.0 -10.0 MOTE - POSITIVE SHANK ANGLE INDICATES SHANK TIP BELOW CROWN -20.0-30.0-40.0 -50.0 100.0 90.0 80.0 70.0 60.0





STON .b. stabilizers, 48 deg. mov. flukes **3**5.**0** 30.0 45.0 40.0 50.0 55.0 60.0 65.0 25.0 70.0 \$ **25**.0 30.0 35.0 45.0 50.0 55.0 60.0 65.0 10.0 70.0 \$ 30.0 35.0 55.0 50.0 60.0 45.0 65.0 70.0 Anchor Drag Distance 153

```
INDI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       Day # - 172
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                                                                                                                                                                                                                                                                                                                                    STOCKLESS ANCHOR TEST
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   -25.0
      TEST DATE
TEST NO.
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TEST AREA
STANT-END TIMES
SEAFLOOR TYPE
ANCHOR TYPE
ANCHOR TYPE
AUV. ANCHOR TYPE
AUV. ANCHOR TYPE
AUV. ANCHOR TYPE
AUV. ANCHOR SEPARATION
DEPRESSORS.NO.-MT.EACH-TOTAL WT.
POORING LINE DESCRIPTION
                                                                                                                                                                                                                                                                                                   172
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   -20.0
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1638 - 1657
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                                                                                                                                                                                                                                                                                                   STECKLESS .5000LB. STABILIZERS. 48 DEG. FX. FLUKES
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             Sha
                                                                                                                                                                                                                                                                                                 5950.00 LB.
48.00 CEG. - 1 0-MOV 1-FIX
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   -10.0
                                                                                                                                                                                                                                                                                                   0.00 LB.

C.O FEET

O - 0.0 ~ 0.0 LB.

90 FT. 2 IN. CHAIN. 360 FT. 2.5 IN. CHAIN. 400 FT. 1 5/8 IN.

LWRC ROPE. 346 FT. + 2 IN. IMRC ROPE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              -5.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      0.0
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                                                                                                                                                                       S. ROTATION ANGLE 9. CHAIN LENGTH ON BOTTON 13. ANCHOR FLUKE TIP DEPTH
6. SHARK ANGLE 10. CHAIN WEIGHT ON BOTTON 14. WATER DEPTH
7. WAR ROPE ANGLE 11. ANCHOR CROWN DEPTH 15. TOTAL BOTTON WEIGHT
8. DECK HORIZ. FORCE 12. ANCHOR SHANK TIP DEPTH
                                          1. DRAG DISTANCE
2. DECK TENSION
3. AACHOR TENSION
4. PACKAGE DEPTH
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              10.0
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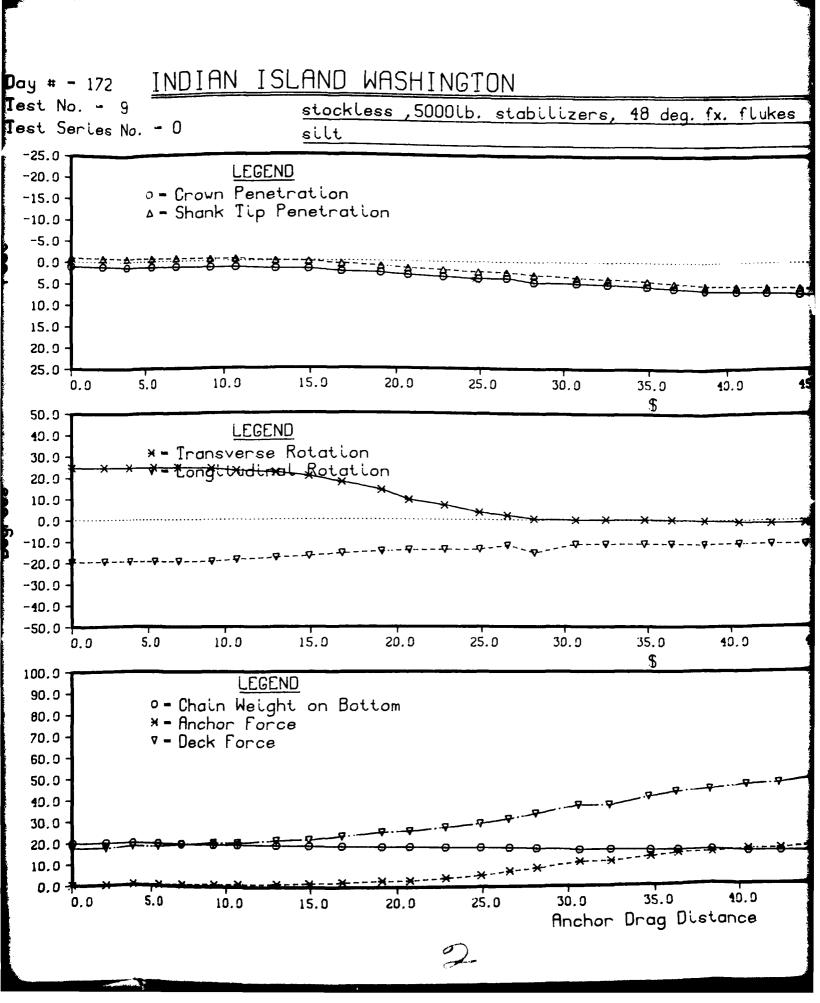
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22793.1
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21946.2
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CISTANCE BARGE TRAVELLED DISTANCE ANCHOR TRAVELLED
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    -40.0
      NOTE - POSITIVE SHANK
ANGLE INDICATES
SHANK TIP BELOW
CROWN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    -50.0
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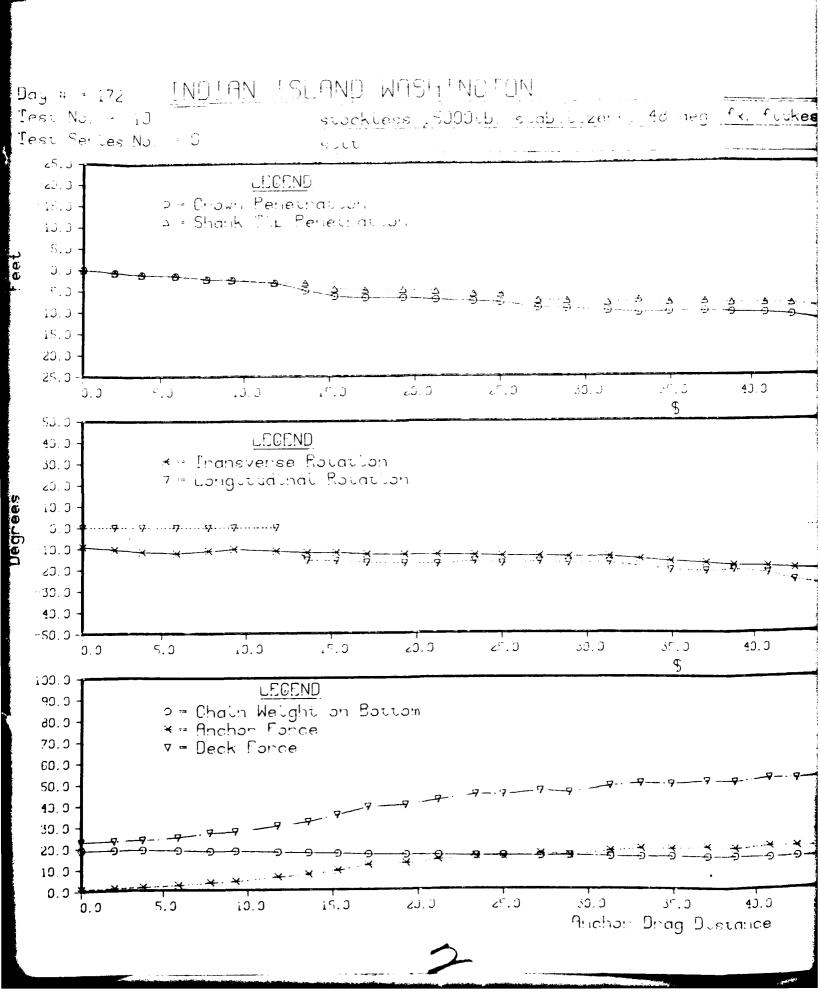
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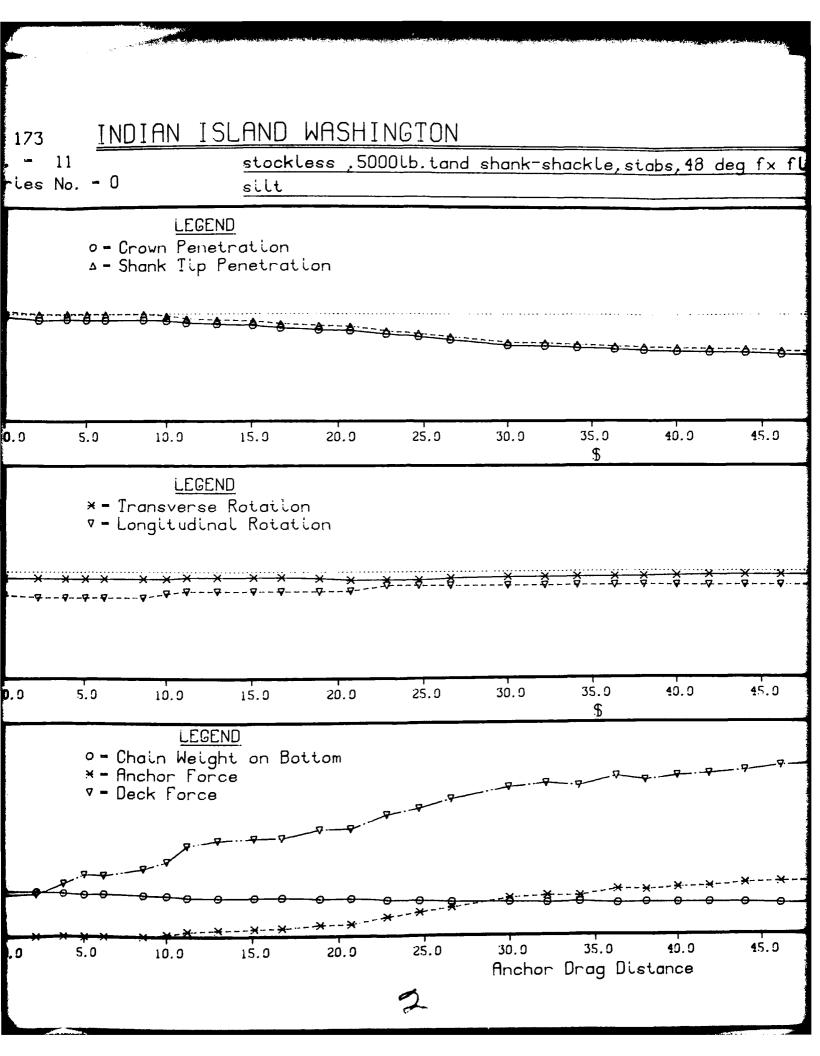
stabilizeri, 40 deg. <u>fx. fuukes</u> ر. ای . J 45.0 :3.0 4J. J 65.0 55.0 60.0 50.0 70.9 65.0 Já. 3 35.3 55.0 60.0 45.0 70.0 40.0 50.0 44.0 აე.ე 50.0 60.0 65.0 55.0 Anchor Drag Dustance 157

Day # - 173 Test No. Test Series No. STOCKLESS ANCHOR TEST -25.0 TEST BATE
TEST BAG.
TEST RUM
TEST AREA
START-END TIMES
SEAFLORD TYPE
ANCHOR TYPE
ANCHOR TYPE
ANCHOR TYPE
AUX. ANCHOR TYPE
AUX. ANCHOR TYPE
AUX. ANCHOR TYPE
AUX. ANCHOR TYPE
TAIR-AUX ANCHOR SEPARATION
DEPRESSORS, BO.-BT.EACH-TOTAL BT.
ROGRING LINE DESCRIPTION -20.0 -15.00 --10.0 5950.00 LB.
135.0 FEET
0 - 0.0 LB.
0 - 0.0 LB.
135FT. 21N. CHAIN ATTD TO INDRO ANCHOR SHAMK.340FT. 2.51N
CHAIN. 400 FT. 1 5/8 IN. IBRC ROPE. 344 FT. 2 IN. IMRC ROPE -5.0 0.0 5.0 1. DRAG DISTANCE
2. DECH TENSION
3. ANCHOR TENSION
4. PACKAGE DEPTH 5. ROTATION ANGLE 6. SHANK ANGLE 7. WIRE ROPE ANGLE 8. DECK HORIZ. FORCE 9. CHAIN LENGTH ON SOTTOR 10. CHAIN WEIGHT ON BOTTOR 11. ANCHOR CROBN DEPTH 12. ANCHOR SMANK TIP DEPTH 10.0 15.0 9 FEET 473.4 467.5 442.6 442.6 448.3 436.1 410.4 410.9 376.1 366.6 359.2 376.1 359.2 359.3 359.3 359.3 339.4 339.4 339.4 339.4 339.4 15 185.3166.5 32666.5 32666.5 31262.2 31262.2 31262.2 31262.2 31262.2 30263.1 29360.1 29360.1 29360.1 29360.1 29360.1 29360.1 29360.1 28612.8 28265.4 2721.1 27546.2 27546.2 27645.0 26465.0 26465.0 26465.0 26467.2 26469.1 LAS 21266-5 20968-5 20225-7 197222 20068-7 19722-2 20068-7 1973-6 18105-1 17973-6 18131-1 17973-6 16185-4 17973-6 15912-0 15948-6 15912-0 15908-2 15908-2 15908-2 15908-2 14908-2 14908-2 14908-2 14908-2 14908-2 14908-2 14908-2 FEET 97.1 97.4 97.7 97.7 98.1 98.1 99.4 100.0 101.7 102.3 103.0 104.4 104.8 105.1 105.2 105.5 106.5 106.5 106.7 FEFT 101.2 101.2 101.2 101.2 101.4 101.9 102.2 102.2 103.2 103.5 104.7 105.6 106.2 106.2 106.2 106.2 106.2 106.2 106.2 106.3 106.7 107.0 109.2 109.2 109.3 109.2 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 110.5 OEG -11.00 -12.00 -12.00 -12.00 -10.10 -9.00 -9.00 -9.00 -6.45 -6.55 -6.55 -6.56 -6.66 -6.66 -6.66 -6.66 KIPS
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83.0 FEET 98.4 99.0 99.1 99.1 100.4 101.0 101.4 103.7 105.0 105.1 105.5 106.6 310.7 20.0 25.0 0.0 5.0 50.0 40.0 30.0 20.0 10.9 Degre 0.0 -10.0-20.0DISTANCE BARGE TRAVELLED -30.0 BISTANCE ANCHOR TRAVELLED -40.0NOTE - POSITIVE SHANK ANGLE INDICATES SHANK TIP BELOW CROWN -50.0 0.0 5.0 100.0 90.0 80.0 70.9 60.0 50.9 40.0 30.9 20.0 10.9 0.0

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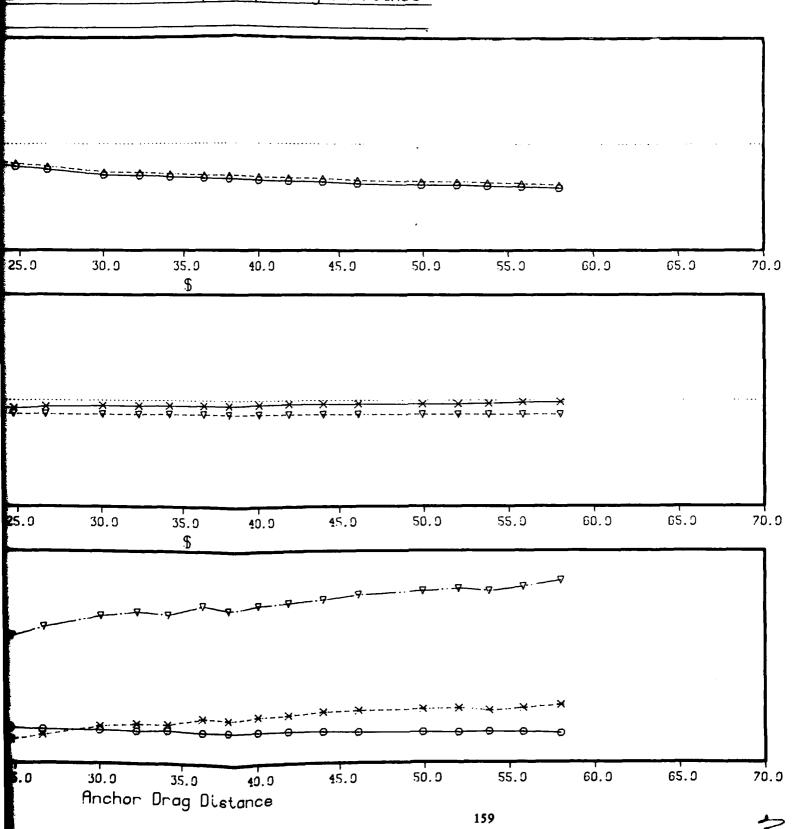
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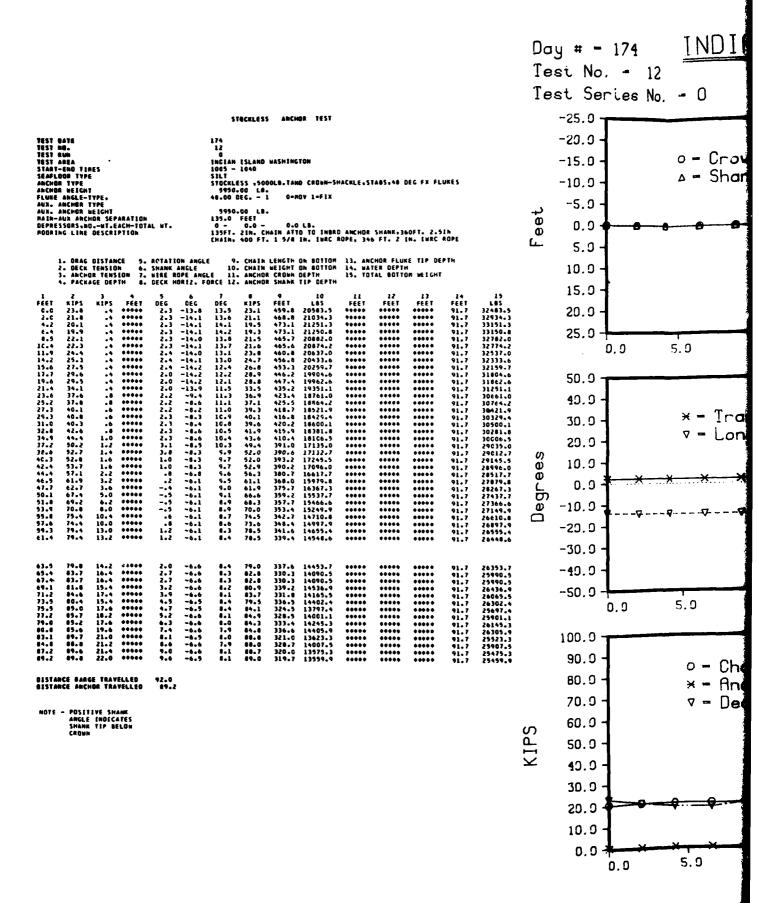
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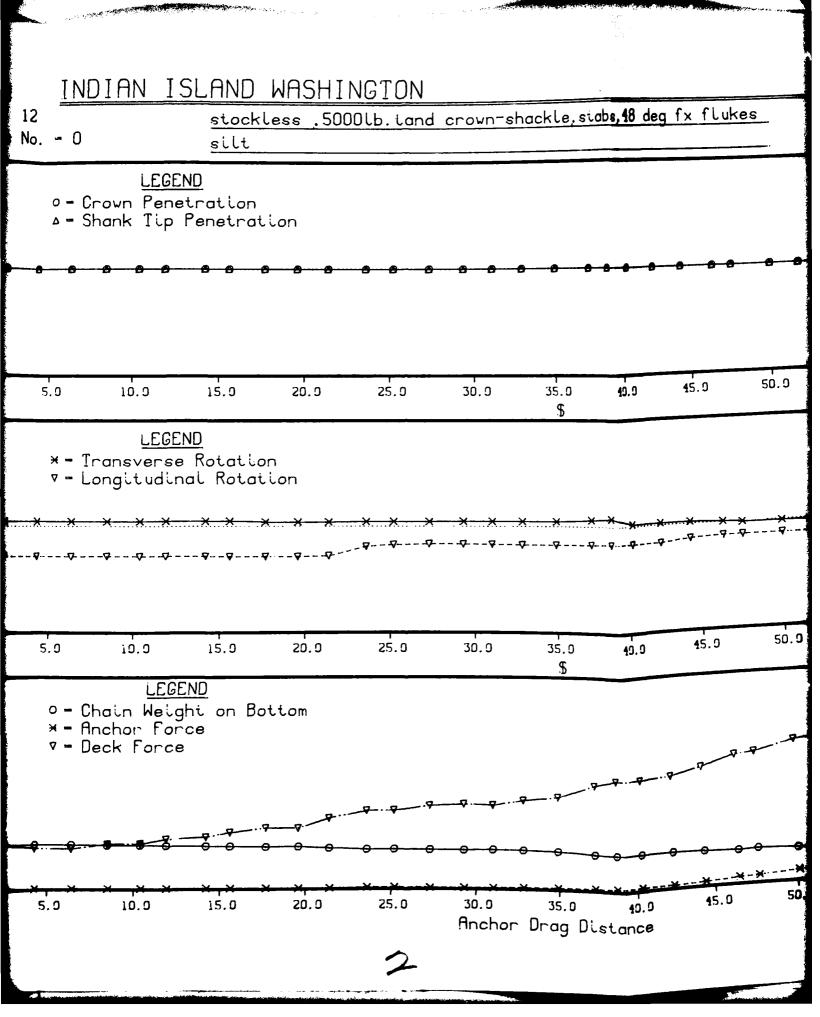


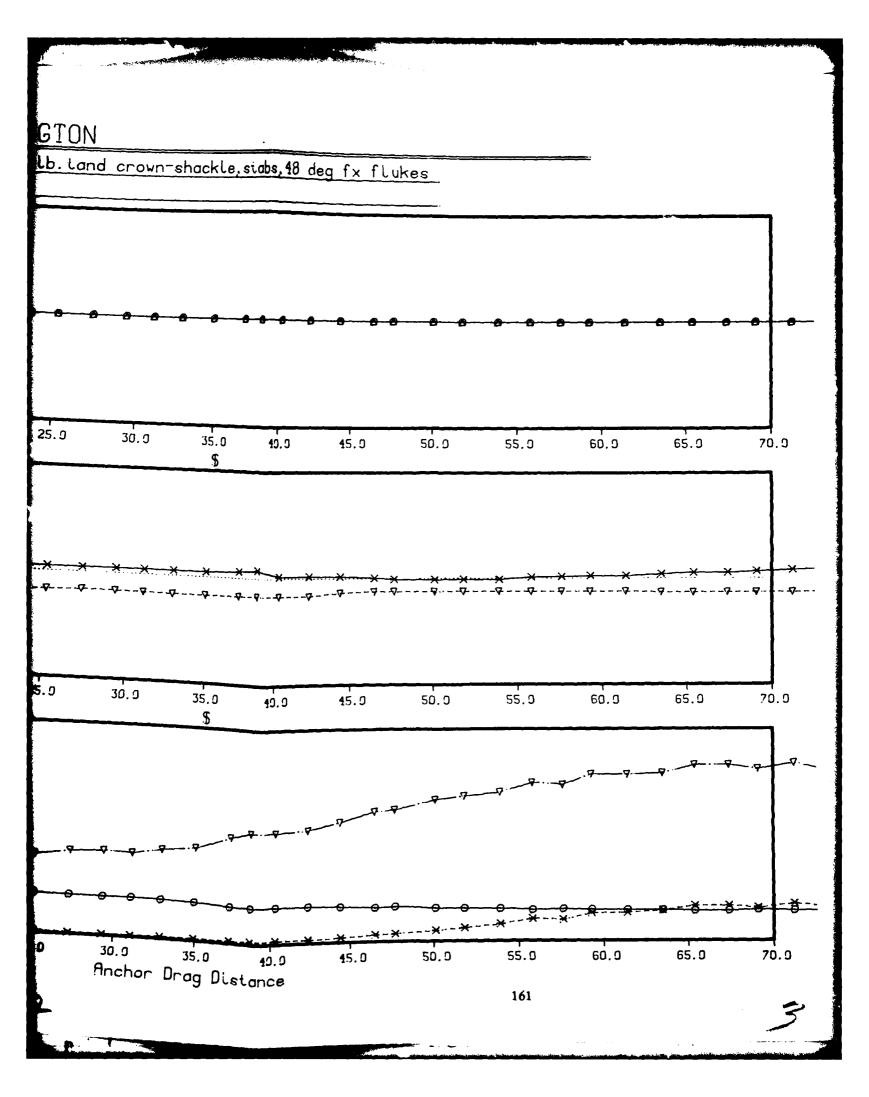
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b. tand shank-shackle, stabs, 48 deg fx flukes

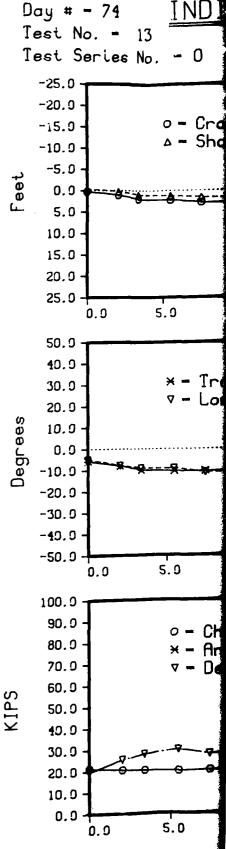


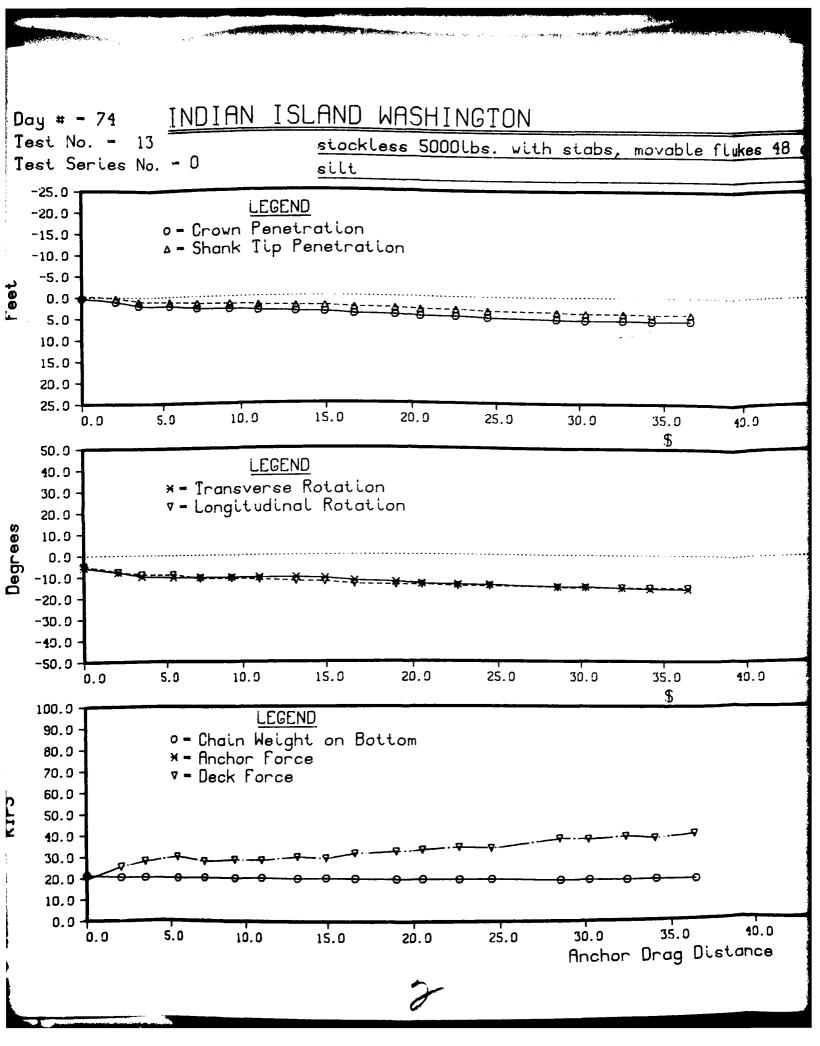




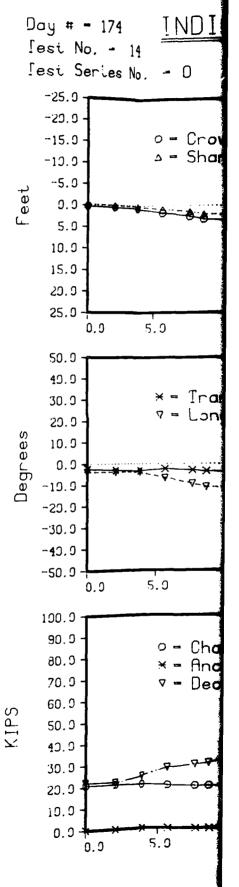


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TEST DATE
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TEST RUN
TEST REA
START-ENG TIMES
SEAFLOOR TYPE
ANCHOR TYPE
ANCHOR TYPE
AUX. ARCHOR TYPE,
AUX. ARCHOR TYPE
AUX. ARCHOR TYPE
AUX. ARCHOR SEPARATION
DEPRESSORS.ANG.-MI-EACH-TOTAL MT.
PUORING LIME GESCRIPTION
                                                                                                                  1. DRAG DISTANCE
2. DECK TENSION
3. ANCHOR TENSION
4. PACKAGE DEPTH
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         5. ROTATION ANGLE
6. SHANK ANGLE
7. LIRE ROPE ANGLE
8. DECK HORIZ. FORCE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           13. ANCHOR FLUKE TIP DEPTH
14. WATER DEPTH
15. TOTAL BOTTOM WEIGHT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         9. CHAIR LENGTH ON BOTTOR
10. CHAIR WEIGHT ON BOTTOR
11. ANCHOR CROWN DEPTH
12. ANCHOR SHAHR TIP DEPTH
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                15
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FEET 90.5
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DISTANCE BARGE TRAVELLED DISTANCE ANCHOR TRAVELLED
                                                                                                                                                                 POSITIVE SHANK
ANGLE INDICATES
SHANK TIP BELOW
CROWN
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| 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DISTANCE | 1. ORAC DIS



INDIAN ISLAND WASHINGTON stockless 5000lbs. with stabs, movable flukes 48 deg. **-** 0 sili LEGEND o - Crown Penetration △ = Shank Tip Penetration 5.0 50.0 45.0 20.0 10.0 15.0 25.0 30.0 35.0 40.0 \$ LEGEND * - Transverse Rotation ▼ = Longitudinal Rotation - V --- 9 -- - Q --- Q -.0 50.0 15.0 20.0 25.0 30.0 45.0 40.0 10.0 35.0 LEGEND o = Chain Weight on Bottom x = Anchor Force V - Deck force 45.0 50.0 15.0 20.0 25.0 35.0 40.0 10.0 Anchor Drag Distance

Cra

Sha

Lor Degrees -10.0 -20.0 -30.0-40.0-50.0 5.0 0.0

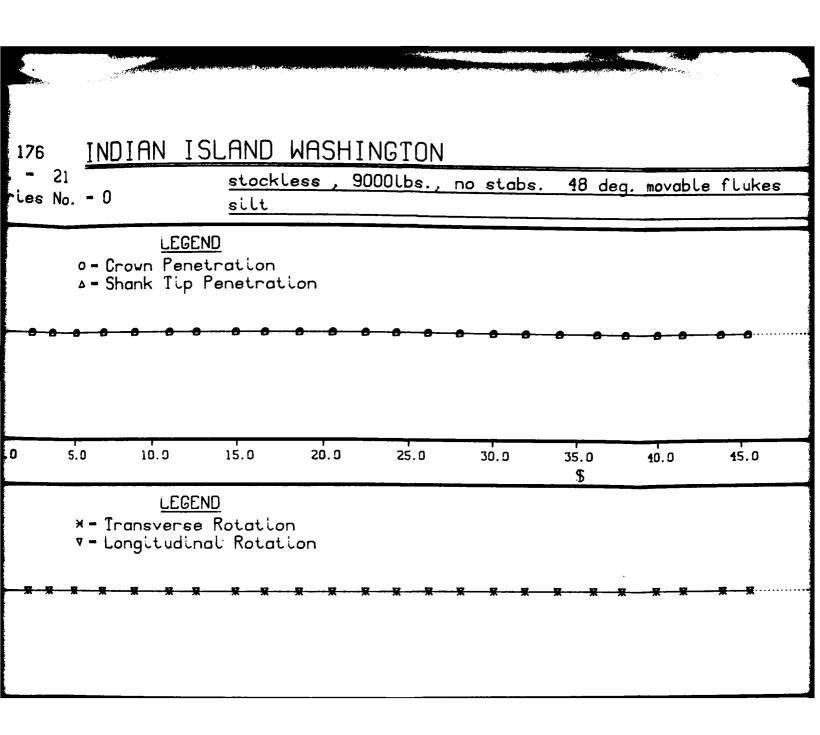
100.0 90.0 80.0 70.0 De 60.0 50.0 40.0 30.0 20.0 10.0 0.0 5.0

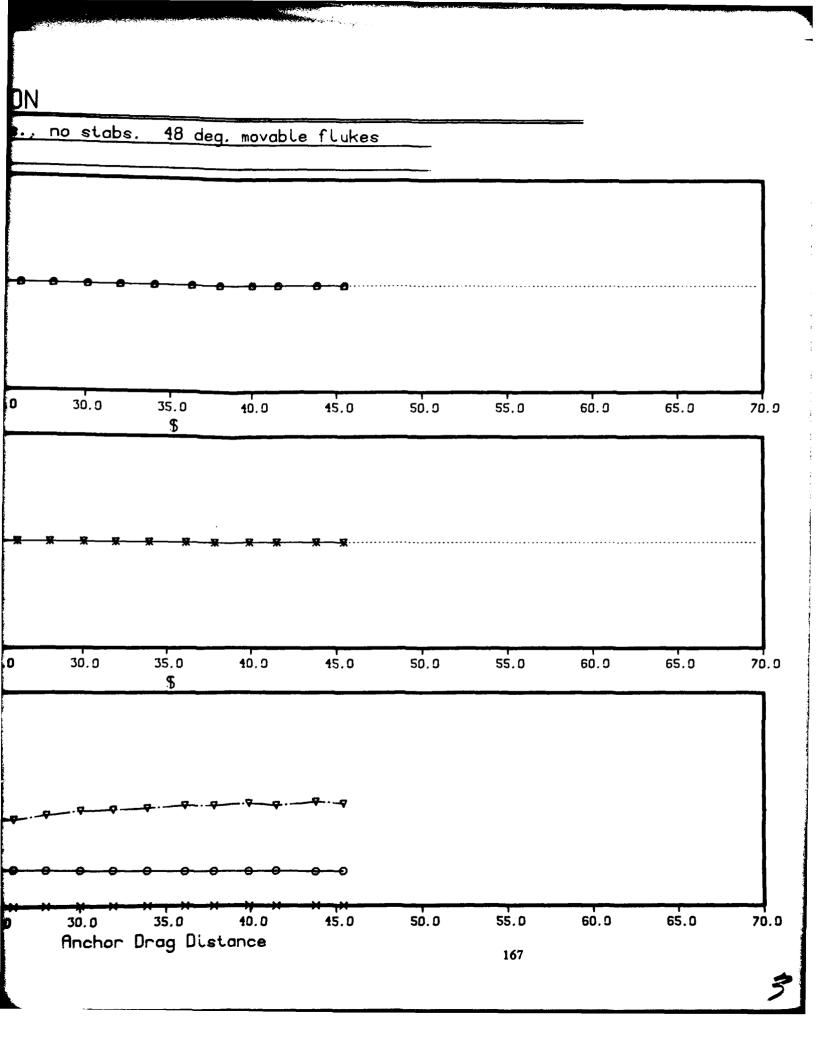
0.0

STOCKLESS ANCHOR TEST

TEST DATE
TEST NO.
TE 0
INCIAN ISLAND WASHINGTON
810 - 900
SILT
STOCKLESS , 9000LBS., NO STABS., 48 DEG. ROVABLE FLUKES
10500 LB.
48.00 DEG. - 0 0-ROV 1-FIX 0.00 LB.
C.O FEET
0 - 0.0 - 0.0 LB.
135 FT. 2 In. CHAIN.300 FT. 2.5 IN. CHAIN.400 FT. 1 5/8 IN.
1MBC ROPE, 346 FT. * 2 IN. IMBC ROPE 1. DRAG DISTANCE
2. DECK TENSION
3. ANCHOR TENSION
4. PACKAGE DEPTM
6. SHAMK ANGLE
10. CHAIN MEIGHT ON BOTTON
11. ANCHOR TENSION
6. SHAMK ANGLE
11. ANCHOR CROBN DEPTM
15. TOTAL BOTTON MEIGHT
15. TOTAL BOTTON MEIGHT 9 FEET 443.9 437.0 429.5 426.3 417.9 417.6 410.3 413.6 409.6 398.6 398.6 399.6 399.6 379.6 379.7 385.6 379.7 375.2 375.2 377.2 377.2 377.2 377.2 377.2 5 DEG 10 LBS 19787-5 19271-6 1906-0 19904-4 18482-9 18104-4 18267-6 17784-5 17784-5 17785-7 17920-7 17190-6 1865-3 1858-3 18527-3 18527-3 18534-9 18534-9 18534-9 18534-9 18534-9 2 3

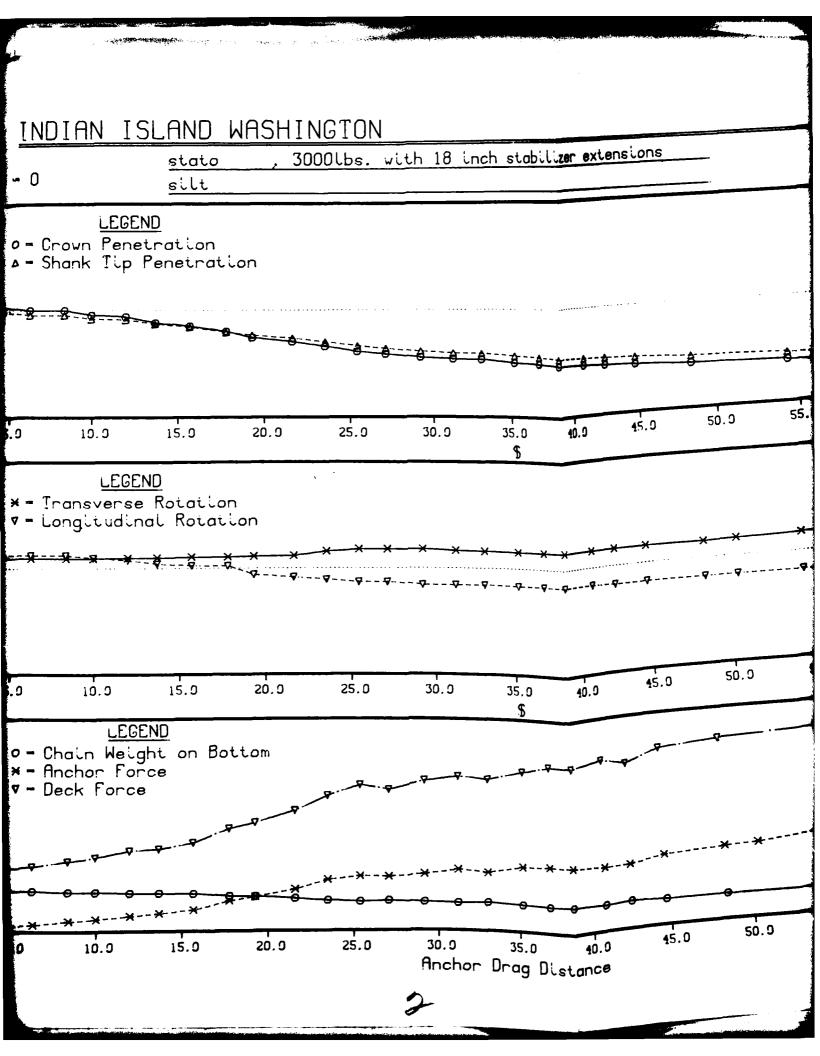
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STATE TEST DATE
TEST NO.
TEST NUN
TEST ARA
START-EAD TIPES
SEAFLOOR TYPE
ANCHOR TYPE
ANCHOR TYPE
AULT. ANCHOR TYPE,
AULT. ANCHOR TYPE
AULT. ANCHOR TYPE
CAULT. ANCHOR TYPE
AULT. ANC INDIAN ISLAND WASHINGTON 1030 - 1100 SILT STATO , 3000LBS. WIF 3500.QQ LB. , 3000LBS. HITH IS INCH STABILIZER EXTENSIONS 3500.00 LB. 0.00 LB. U.GG LB. C.O FEET O - 0.O - 0.O LB. 139 FT. 2 IN. CHAIN-300 FT. 2-5 IN. CHAIN-400 FT. 1 5/8 IN. LURC ROPE, 346 FT. • 2 IN. LURC ROPE S. ROTATION ANGLE
A. SMANK ANGLE
10. CHAIN MEIGHT ON BOITON
7. SIRE ROPE ANGLE
11. ANGHOR CROBN DEPIN
12. ANGHOR SMANK TIP DEPIN 13. ANCMOR FLUKE TIP DEPTH 14. WATER DEPTH 15. TOTAL BOTTOM WEIGHT 1. ORAG DISTANCE 2. DECK TENSION 3. ANCHOR TENSION 4. PACKAGE DEPTH 15 LBS 22479.8 23142.3 22580.3 22170.3 22014.4 21926.2 21490.9 21053.3 20007.4 19759.4 8 KIPS 28.7 28.0 39.9 33.9 35.0 38.1 38.1 35.0 748.3 56.7 68.6 68.6 65.7 72.9 77.8 80.6 87.7 80.6 83.2 83.4 10 LBS 19479.8 19670.3 19358.3 19060.3 18514.4 18020.2 17990.9 14260.2 14260.2 13199.0 13199.0 13199.0 12798.8 12798.8 12798.8 12798.8 12798.8 12798.1 12798.1 12798.1 12798.1 12798.1 7-ET 7 80.8 81.0 81.1 81.0 81.9 83.0 83.4 85.6 9 85.6 9 85.6 9 85.6 9 92.2 2 93.0 95.0 2 95.0 2 95.0 2 97.0 1 97.0 1 97.0 1 97.0 1 97.0 1 97.0 1 97.0 1 75.7 85.7 85.7 85.8 86.7 87.7 88.0 89.3 90.0 91.3 92.5 93.4 94.4 95.4 96.0 97.3 98.1 98.8 99.2 99.3 100.2 98.8 DEG 13.1 13.1 13.1 12.9 12.7 12.3 12.1 FEET 437.8 441.0 455.4 429.6 429.6 407.8 407.8 378.5 373.6 321.4 337.6 310.7 317.5 303.0 298.6 305.4 288.0 293.6 KIPS 29-5 29-5 31-7 35-1 31-7 35-9 49-2 57-1 64-9 67-6 77-6 77-6 81-8 78-9 81-8 11.6 11.3 10.9 10.8 10.3 10.2 10.1 10.1 10.1 9.9 9.7 9.7 9.7 9.7 9.7 9.7 9.7 18785.8 17766.2 17143.8 17596.3 16952.6 16946.6 16218.6 15998.9 16251.7 15751.6 16343.1 15469.3 40.6 84.4 87.4 15153.4 15402.6 15188.7 DISTANCE BARGE TRAVELLED DISTANCE ANCHOR TRAVELLED 60.0 58.2

POSITIVE SHANK ANGLE INDICATES SHANK TIP BELOW CROWN



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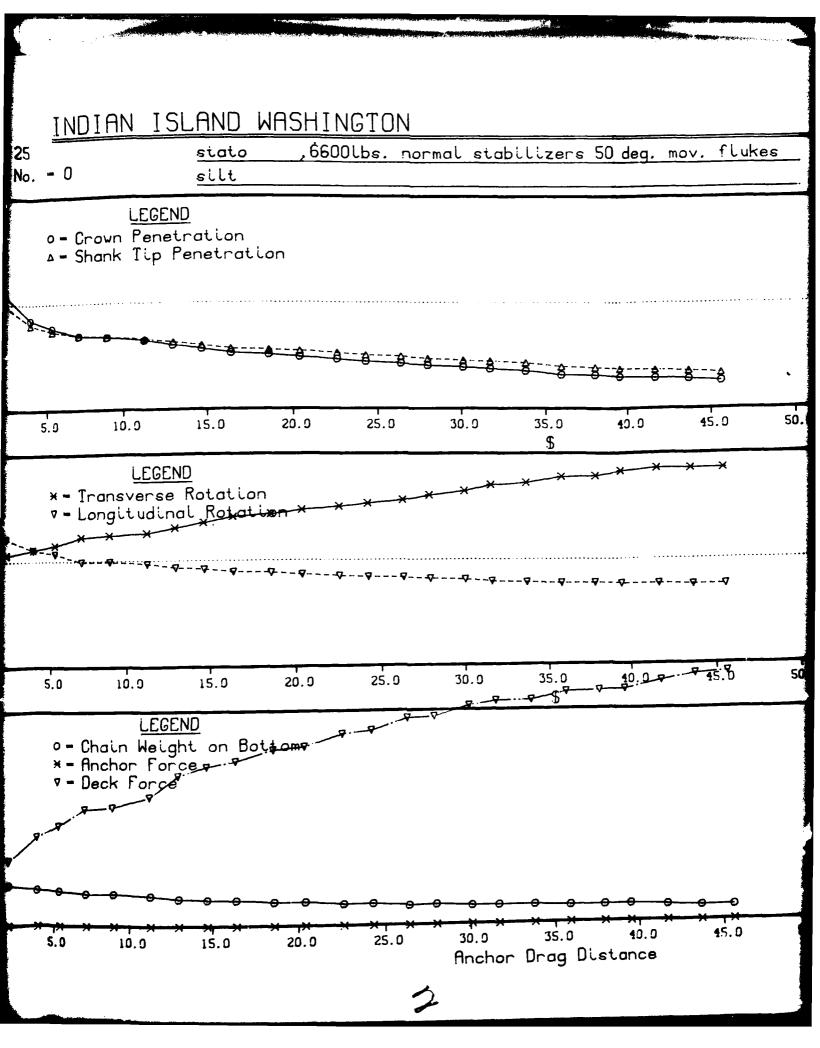
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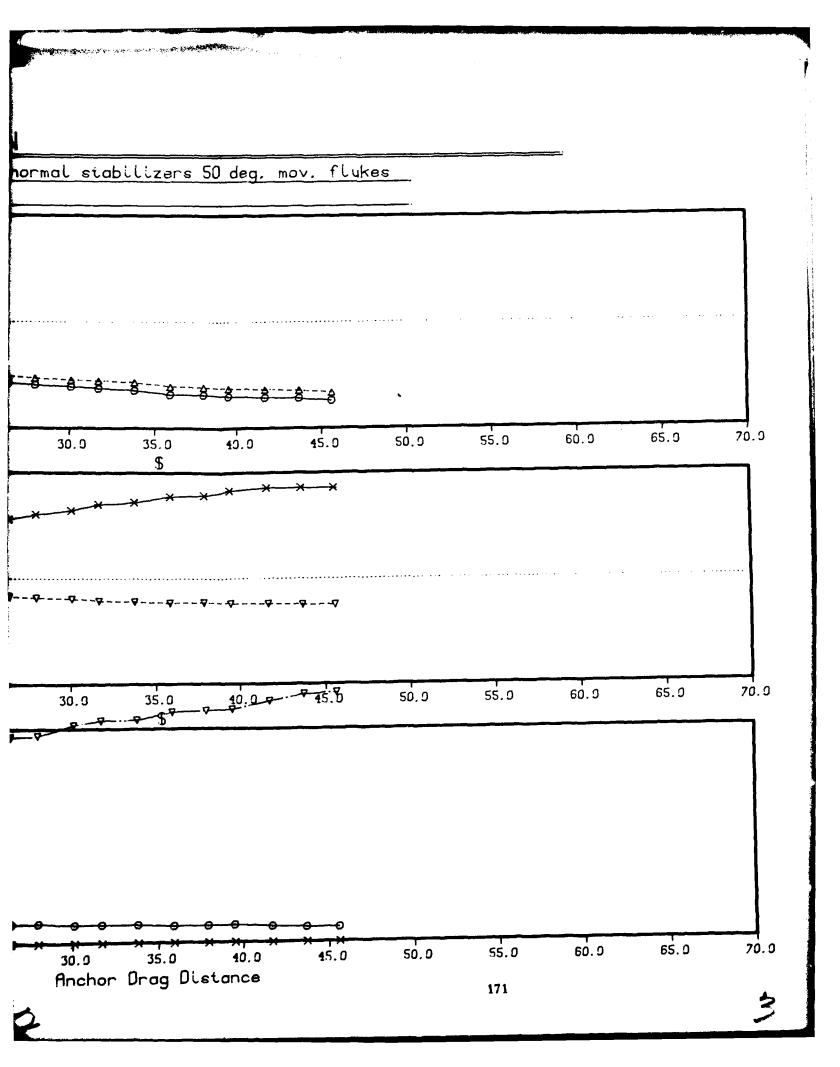
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